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CELESTIAL NAVIGATION

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PREFACE

To carry out any activities at sea one needs to know how to fix positions, set a course and measure the distance. In the area of fisheries, navigational knowledge is obviously essential. For instance, when a fishing boat is preparing to leave a port for a fishing ground, the planned sea route (Course) must be drawn on the charts, and the course in degrees and distance in nautical miles calculated. The departure and arrival time at the fishing ground must be decided.

After leaving the port, position fixes are taken during coasting. Eventually, terrestrial objects to fix positions by will not be visible, then positions must be fixed by means of observing celestial objects and the use of electronic navigational aids, in order to reach the fishing ground and to navigate safely and economically.

When the ship arrives at the fishing ground, she will move in pursuit of fish schools and position must be checked on the fishing ground chart in order to continue effective fishing activities. On the other hand, when one sets-up a stationary trapnet, a place to set it must be carefully selected and the position and depth of water measured beforehand. This is so that one can design the net, its size and construction, according to the depth of water and place it will be set. Also when one sets-up a conservation or prohibited fishing area, fish shelter or artificial reef, one has to determine the correct and exact position by latitudes and longitudes on a chart and set seamarkers in the water.

To carry out the aforementioned activities at sea, there are many devices and instruments which can be used to fix position e.g. sextant, divider, protractor, triangle ruler, magnetic compass, gyrocompass, chronometer, radar, echosounder, satellite navigator, loran receiver, decca receiver, omega receiver, doppler-speed log, sonar, direction finder, xy-plotter, course recorder, theodolite distance meter, etc. These devices

and instruments will help you fix position but, first you have to know: what latitudes and longitudes are; how to express ship's course and distance to be travelled; what difference of latitudes and longitudes are; what lines of position given by terrestrial objects are; the celestial bodies; how to observe and measure the distance and altitude of landmarks; how to measure the altitude of heavenly bodies; how to operate electronic instruments; what index error, chronometer error, variation, deviation and compass error are; how to check and select marine charts for navigation; how to make your own charts of fishing grounds and topography of sea-bed.

Without navigational knowledge, no one would understand the positioning of fishing gear in the water or information given by a meteorological agency concerning marine weather. Such knowledge is important to fishing boats in ensuring that their activities at sea are effective and safe. Navigational knowledge is also important in understanding the international laws of the sea such as: "CONVENTION ON THE TERRITORIAL SEA AND CONTIGUOUS ZONE" and "CONVENTION ON THE HIGH SEAS" and thus preventing troubles with other countries.

Trainees learning NAVIGATION at the SEAFDEC Training Department will receive instruction and practical experience, including shipboard training. During the course, it is recommended that you practice by yourself both in the dormitory and on board the training ships. Only practice makes perfect!

Thank you.

(Masato Oishi)
Training Department

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CELESTIAL NAVIGATION

To fix a ship's position by using some knowledge of astronomy is called celestial navigation

Navigators who intend to fix their position on the oceans by celestial navigation must acquire a basic knowledge of astronomy, starting from the basic definition.

1. Basic definitions

1. The celestial sphere

When we look at the sky on a dark night (the moon cannot be seen only stars are twinkling and planets shining), the heavenly bodies look equidistant from us (from the earth), and that they are located on the inner surface of a giant sphere whose center is the earth, and its radius is infinite. This is called the celestial sphere, and this is also an imaginary sphere with infinite radius (Fig. 1, 5)

2. The celestial axis

Is the axis which extends from the minor axis of the earth to the celestial sphere (Fig. 1)

3. The celestial poles

The celestial poles are the points where the minor axis of the earth extends to the celestial sphere and intersects with it (Fig. 1, 5)

4. The celestial equator or the equinoctial

Is the intersection where the plane of the earth's equator is extended to the celestial sphere (Fig. 1, 5)

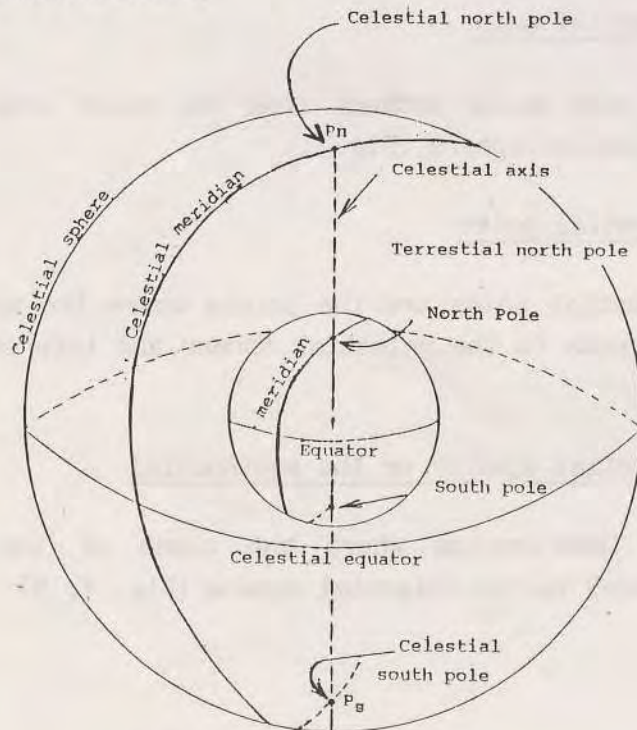
5. The celestial meridians

Are the intersections where the planes of the earth's meridians are extended to the celestial sphere (Fig. 1, 5). These meridians are arcs of great circles through the celestial poles (Fig. 1, 5)

6. The zenith and the nadir

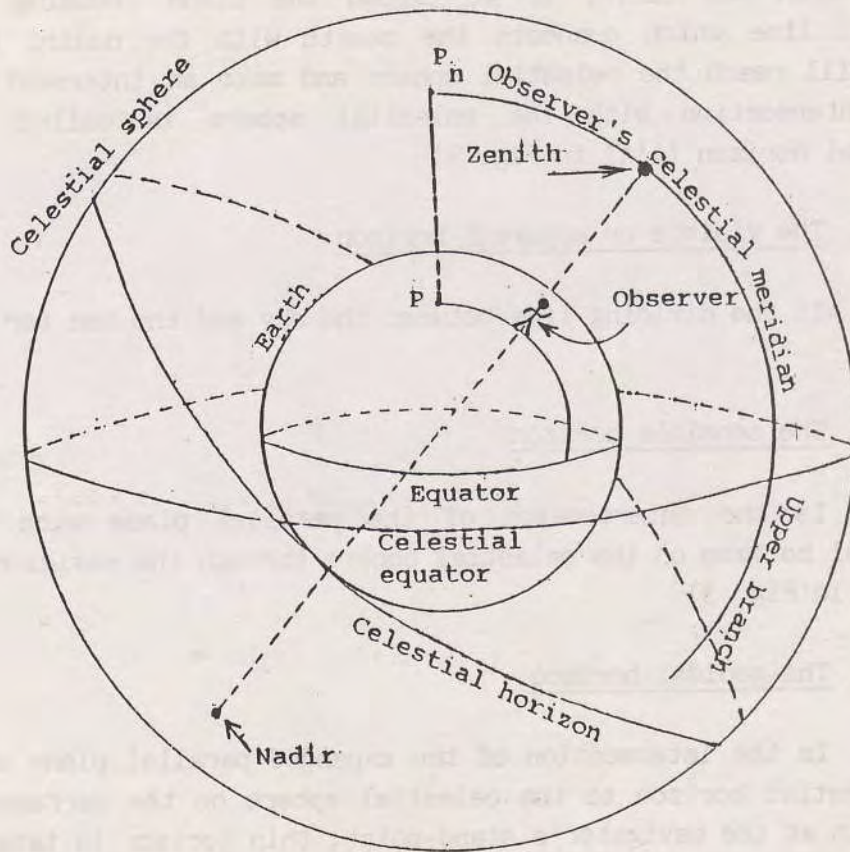
If we extend the straight line connecting the center of the earth with the navigator (observer of a heavenly body), this line will reach the celestial sphere and make a point of intersection on it. This point is called the zenith. Then we extend this straight line to the opposite side of the navigator, this line also reaches the celestial sphere and makes a point of intersection; this point is called the nadir. Therefore, the zenith is your imaginary location on the celestial sphere (Fig. 2, 5).

Note: We suppose that the celestial sphere and the earth have a common center.



Celestial Sphere

Fig. 1



Celestial Sphere & an Observer

Fig. 2

The arc of a celestial meridian connecting with celestial poles and the zenith is called the upper branch, and the lower branch is another arc of a celestial meridian connecting the poles and the nadir (Fig. 2, 5).

Usually a celestial meridian means its upper branch. A celestial meridian takes the name, e.g. 101° east, of its terrestrial counterpart.

7. The celestial horizon

At the center of the celestial sphere which has a common center with the earth, if we expand the plane crossing the straight line which connects the zenith with the nadir, this plane will reach the celestial sphere and make an intersection. This intersection with the celestial sphere is called the celestial horizon (A'A' in Fig. 3)

8. The visible or apparent horizon

Is the dividing line between the sky and the sea (or the earth)

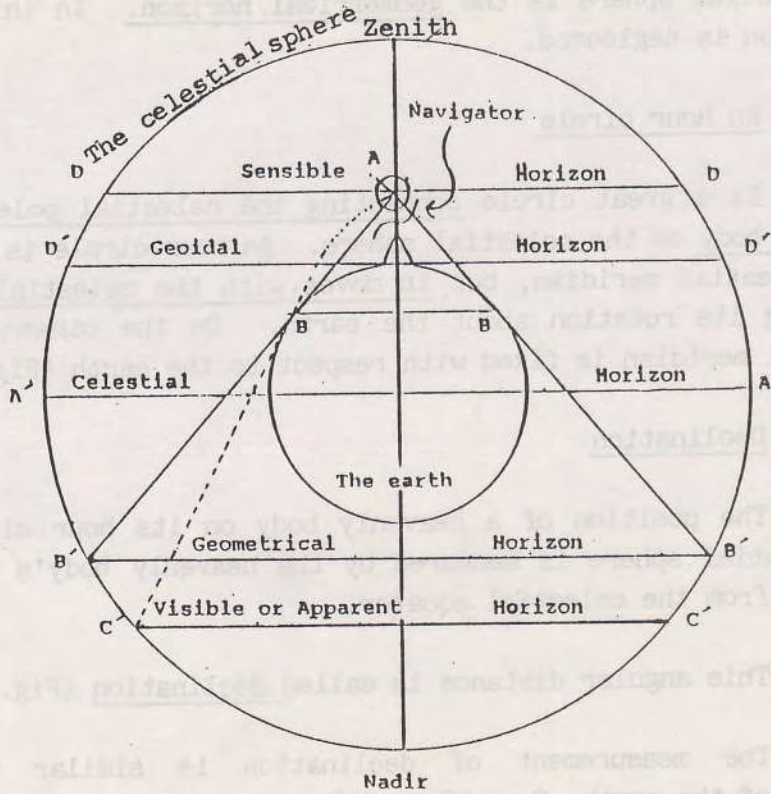
9. The sensible horizon

Is the intersection of the parallel plane with the celestial horizon on the celestial sphere through the navigator's eye (DD in Fig. 3)

10. The geoidal horizon

Is the intersection of the expanded parallel plane with the celestial horizon to the celestial sphere on the surface of the earth at the navigator's stand-point, this horizon is tangent to the surface of the earth at the navigator's stand-point (D'D' in Fig. 3)

(The radius of the earth is negligible in comparison with the radius of the celestial sphere).



Celestial Sphere & Horizon

Fig. 3

11. The geometrical horizon

In Figure 3, the position of navigator's eye is A (the vertex of a cone ABB), and the straight line ABB' is tangent to the surface of the earth at the circle BB. The intersect B' on the celestial sphere is the geometrical horizon. In this case, refraction is neglected.

12. An hour circle

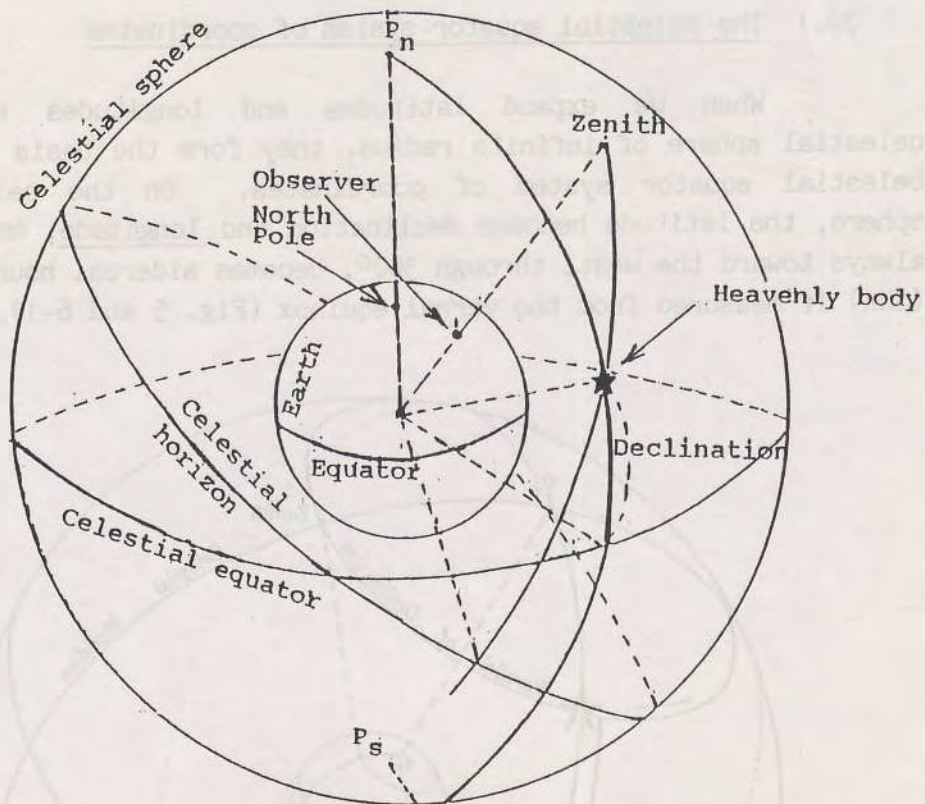
Is a great circle connecting the celestial poles and a heavenly body on the celestial sphere. An hour circle is similar to a celestial meridian, but it moves with the celestial sphere following its rotation about the earth. On the other hand, a celestial meridian is fixed with respect to the earth (Fig. 5).

13. Declination

The position of a heavenly body on its hour circle on the celestial sphere is measured by the heavenly body's angular distance from the celestial equator.

This angular distance is called declination (Fig. 4, 5).

The measurement of declination is similar to the latitude of the earth, from 0° to 90° , and should be named N or S (dec. 8° N, dec. 15° S, Capella 25/12/1979 dec. $45^{\circ} - 58'6$ N, Spica 25/12/1979 dec. $11^{\circ} - 03'3$ S)

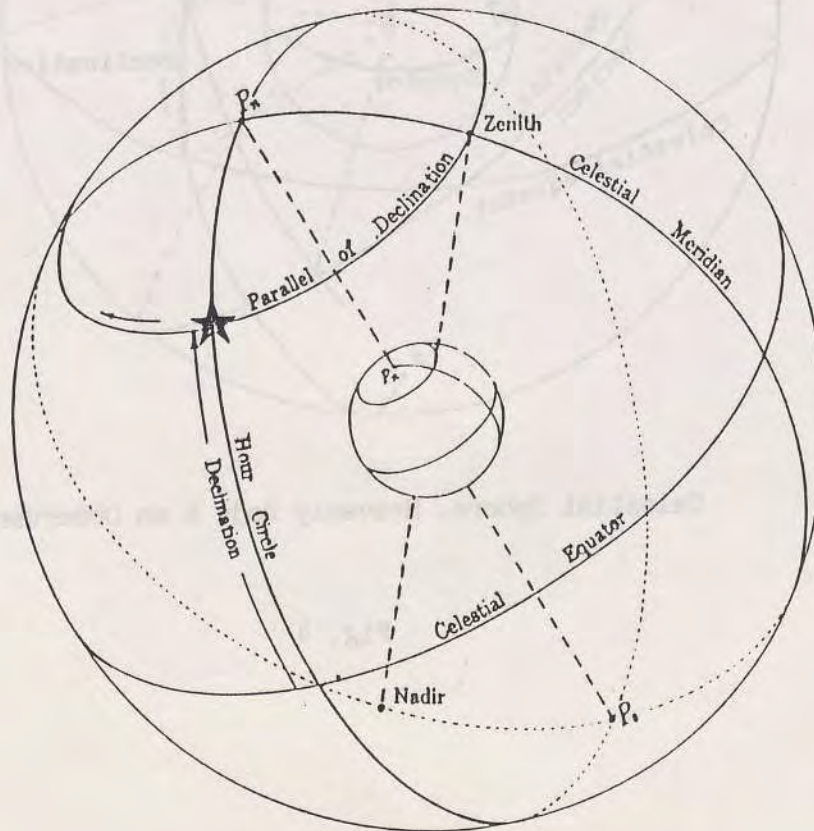


Celestial Sphere, Heavenly Body & an Observer

Fig. 4

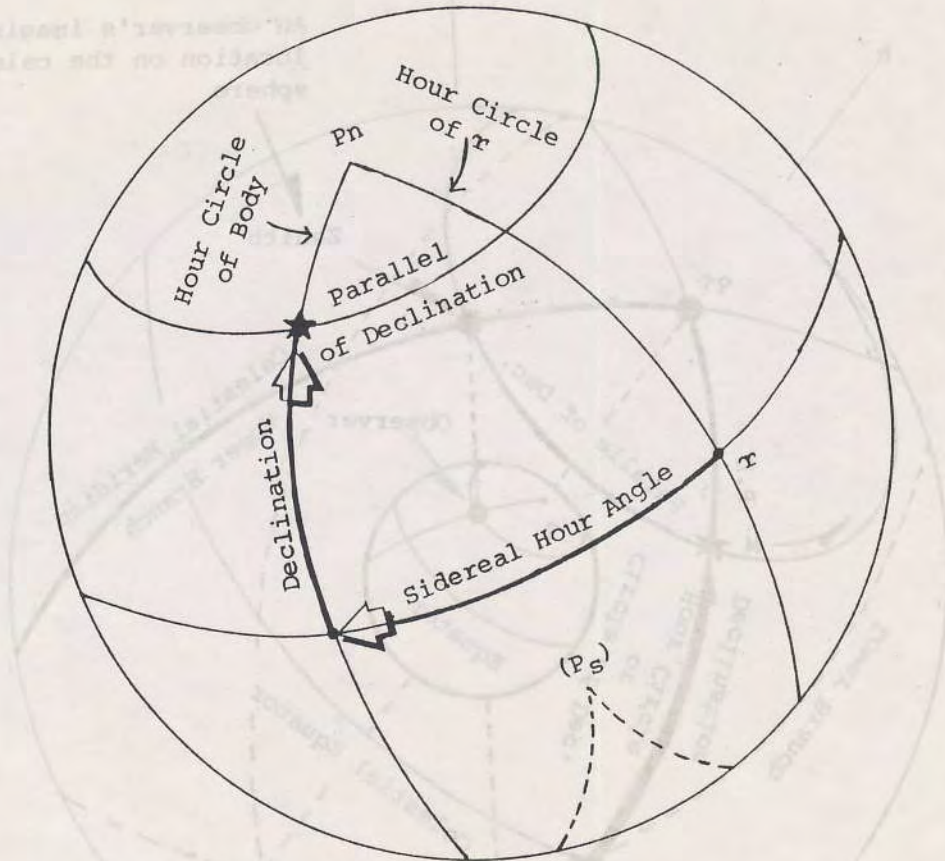
20.1 The celestial equator system of coordinates

When we expand latitudes and longitudes to the celestial sphere of infinite radius, they form the basis of the celestial equator system of coordinates. On the celestial sphere, the latitude becomes declination and longitude, measured always toward the west, through 360° , becomes sidereal hour angle (SHA) if measured from the vernal equinox (Fig. 5 and 6-1).



Celestial Equator System
(Bowditch)

Fig. 5



Sidereal Hour Angle & Declination

Fig. 6-1

T Vernal equinox See Page ...

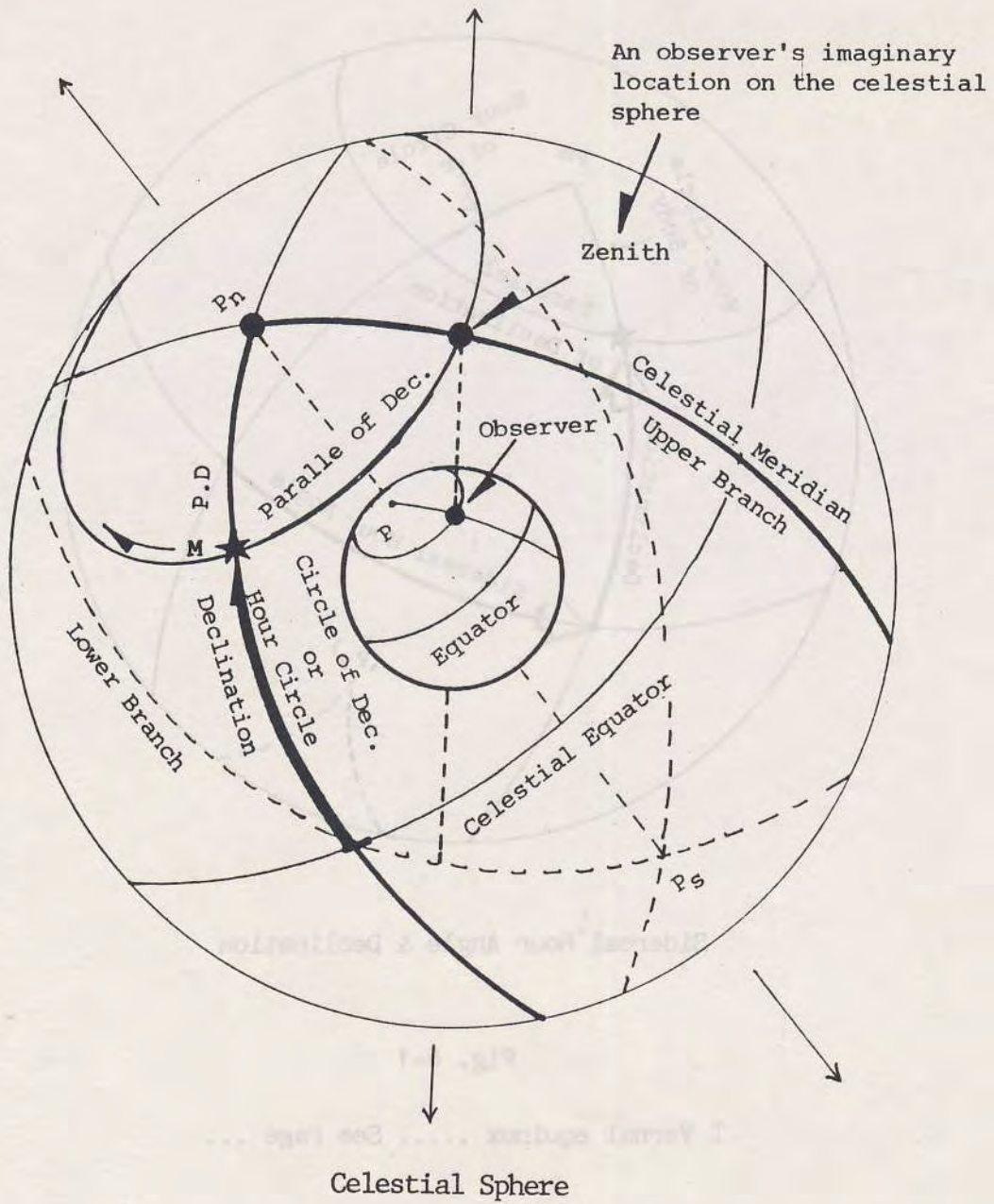


Fig. 6-2

14. The circle of declination

Is a celestial meridian which connects the celestial poles with a celestial body (Fig. 6-2)

15. Polar distance (P.D.)

Is the angular distance from a celestial pole to the heavenly body on the celestial meridian of the heavenly body (P_nM in Figure 6-2)

When the name of observer's latitude is the same as the name of declination,

$$\text{Polar distance} = 90^\circ - \text{declination}$$

When the name of observer's latitude is different from the name of declination,

$$\text{Polar distance} = 90^\circ + \text{declination}$$

16. Local hour angle (L.H.A.) and Greenwich hour angle (G.H.A.)

L.H.A. is the angular distance between the observer's celestial meridian and the heavenly body's celestial meridian (the circle of declination) at the celestial pole (Fig. 9)

Local hour angle is customarily measured from the observer's celestial meridian to the heavenly body's meridian westerly through 360° .

In this case if we use the greenwich meridian as the reference, instead of the local meridian, this hour angle is called Greenwich hour angle (G.H.A.)

17. A parallel of declination

Is a circle which is parallel to the celestial equator, it connects all points of equal declination.

18. Diurnal [dɪ'ɪə:rnəl] circle

The path of a celestial body during its daily apparent revolution around the earth is called its diurnal circle. This is not exactly a circle because of changes of its declination.

19. The ecliptic [ɪkliptɪk]

Is the orbit of the sun's annual motion and considered a great circle of the celestial sphere, inclined at an angle of about $23^{\circ} 27'$ to the celestial equator. This angle is called the obliquity [ɒblikwəti] of the ecliptic (Fig. 6)

20. The vernal equinox and the autumnal equinox

The ecliptic and the celestial equator intersect and make two equinoxes because both of them are great circles and are non-parallel (Fig. 6)

One equinox that the sun passes through the celestial equator from south to north is called the vernal equinox (symbol γ ; [u:psəlan]). The other equinox that the sun passes through the celestial equator from north to south is called the Autumnal equinox (symbol ω [aʊm'egə]) (Fig. 6)

21. The summer solstice and the winter solstice

The furthest points on the ecliptic from the celestial equator are called the solstices. The summer solstice is located northward from the celestial equator, and the winter solstice is located southward from the celestial equator (Fig. 6).

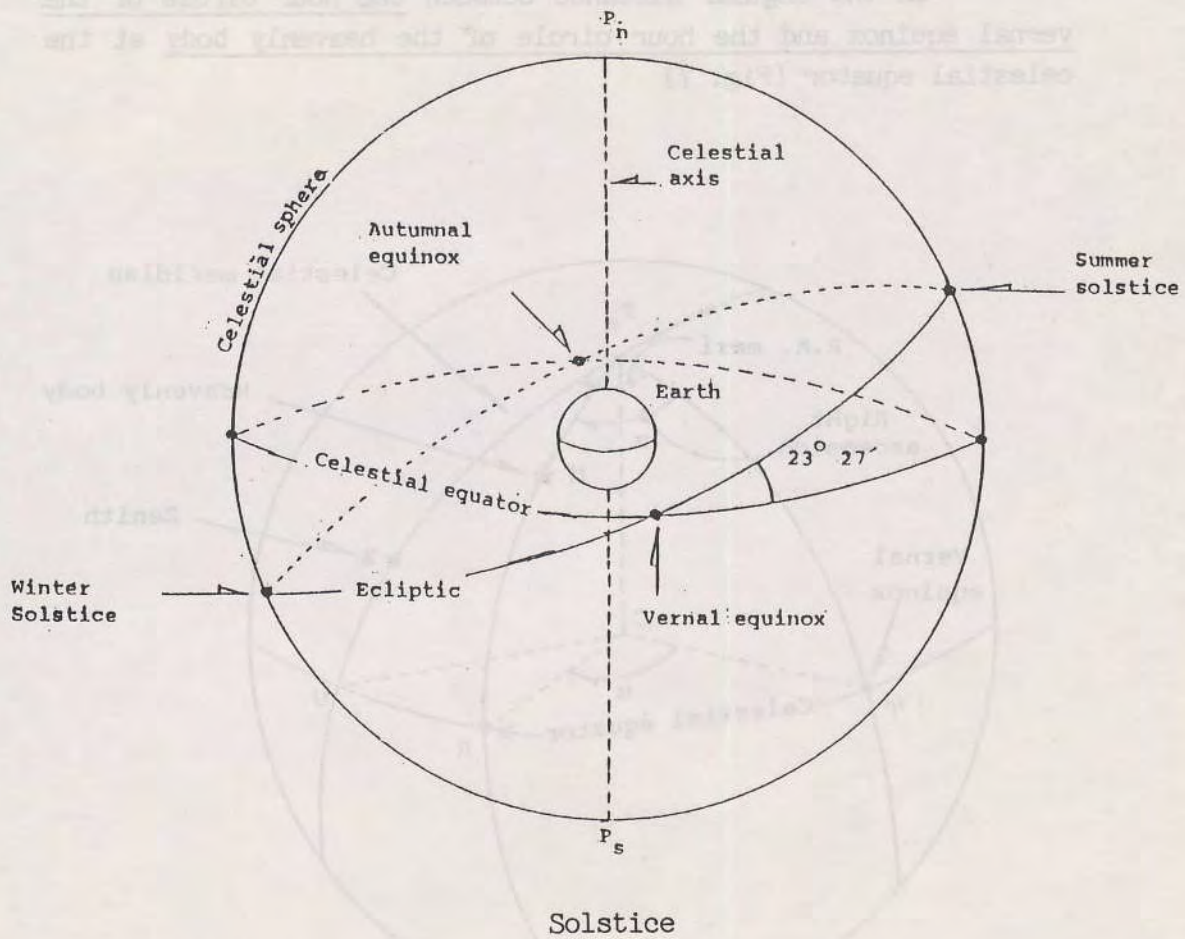
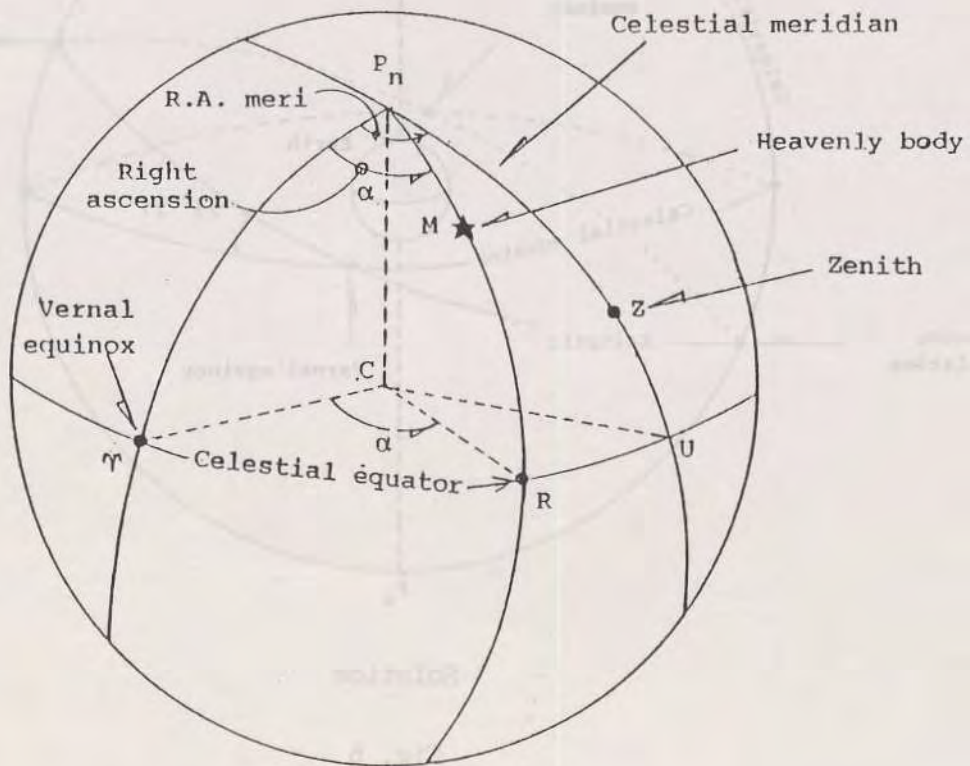


Fig. 6

22. The right ascension (R.A.)

Is the angular distance between the hour circle of the vernal equinox and the hour circle of the heavenly body at the celestial equator (Fig. 7)



Right Ascension

Fig. 7

In Figure 7, the right ascension of M (heavenly body) is $\widehat{\gamma R}$ at the celestial equator, and $\angle \gamma P_n M$ at the P_n

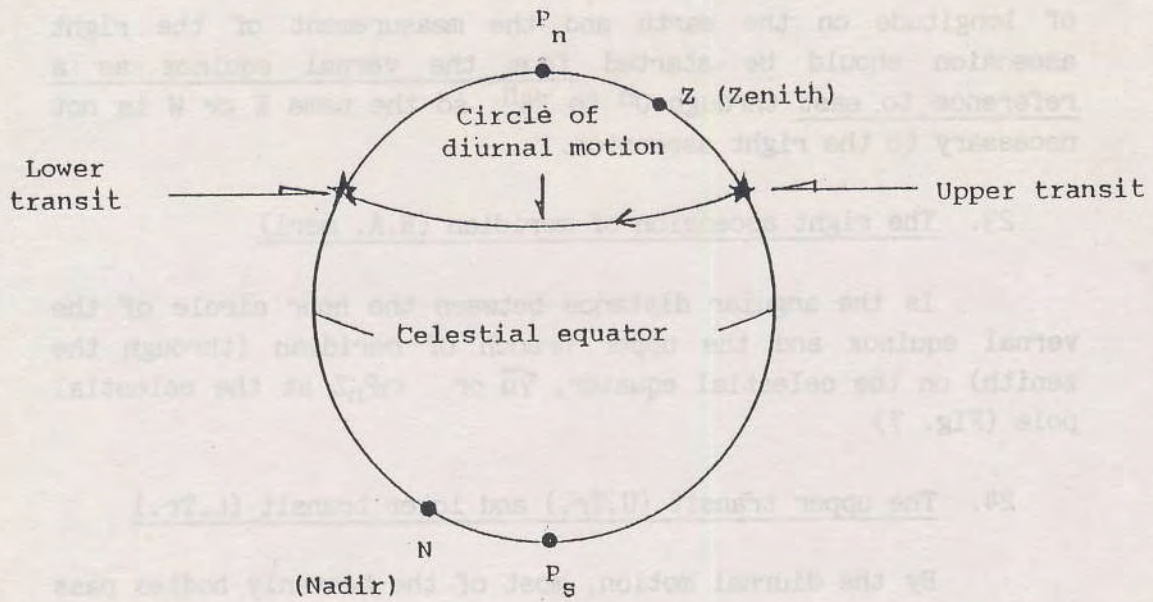
The concept of the right angle is similar to the concept of longitude on the earth and the measurement of the right ascension should be started from the vernal equinox as a reference to east through 0^h to 24^h , so the name E or W is not necessary to the right ascension.

23. The right ascension of meridian (R.A. meri)

Is the angular distance between the hour circle of the vernal equinox and the upper branch of meridian (through the zenith) on the celestial equator, \widehat{u} or $\angle P_n Z$ at the celestial pole (Fig. 7)

24. The upper transit (U.Tr.) and lower transit (L.Tr.)

By the diurnal motion, most of the heavenly bodies pass through upper branch of meridian and lower branch of meridian once a day. This passing through the branches is called transit. When a heavenly body passes through the upper branch of meridian, it is called the upper transit, and a heavenly body passing through the lower branch of meridian, it is called the lower transit (Fig. 8)



Transit

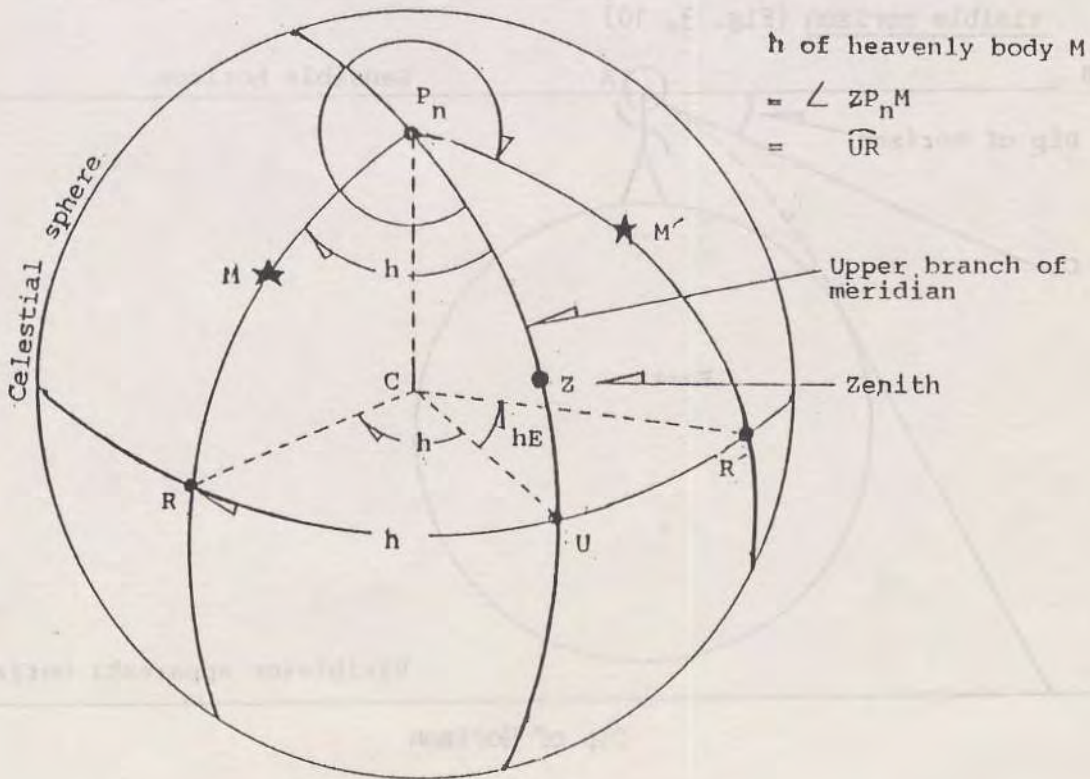
Fig. 8

Navigators call it the meridian passage (meri pass) instead of the upper transit, and call the then altitude of the heavenly body the meridian altitude (meri. alt.)

25. The hour angle (acronym = H.A., abbreviation = h)

Is the angle between the upper branch of the meridian and the hour circle of a heavenly body at the celestial pole, or is the angular distance between the upper branch of the meridian and hour circle of a heavenly body on the celestial equator (Fig. 9)

The hour angle should be measured from the upper branch of the meridian as reference to west side through 0^h to 24^h or through 0° to 360° (Fig. 9)



Hour Angle

Fig. 9

When a heavenly body passes over the lower branch of meridian (M' in Figure 9), the hour angle of M' should be measured from the upper branch of meridian as a reference to east. In case, this hour angle is called = E'ly H.A., easterly hour angle (acronym abbreviation hE)

$$\text{Then } hE = 24^h - h^h \text{ or } hE = 360^\circ - h^\circ$$

The six o'clock hour circle means $h = 6^h$ or 18^h

26. The dip of horizon (abbreviation = Dip.)

Is the dip angle between the sensible horizon and the visible horizon (Fig. 3, 10)

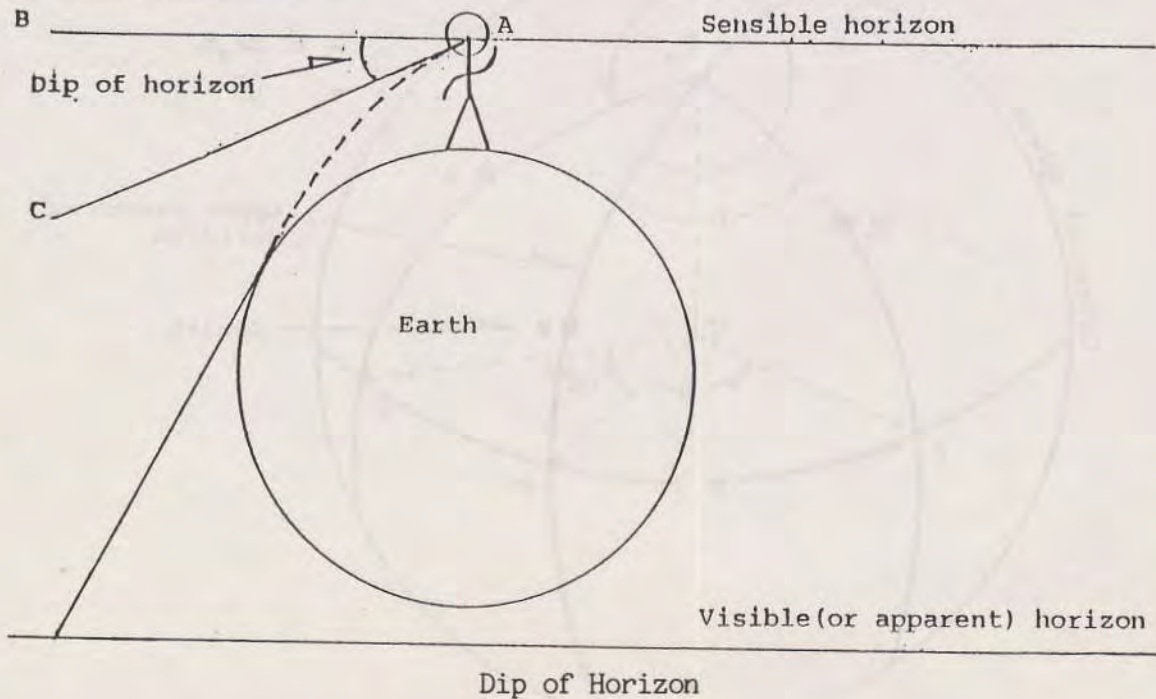


Fig. 10

In Figure 10, dip is $\angle BAC$, between the sensible horizon and a straight line which is tangent to the curving ray of light at the observer's eye (A) from the visible horizon.

27. The vertical circle

Is the great circle passing through the zenith and the nadir (Fig. 11)

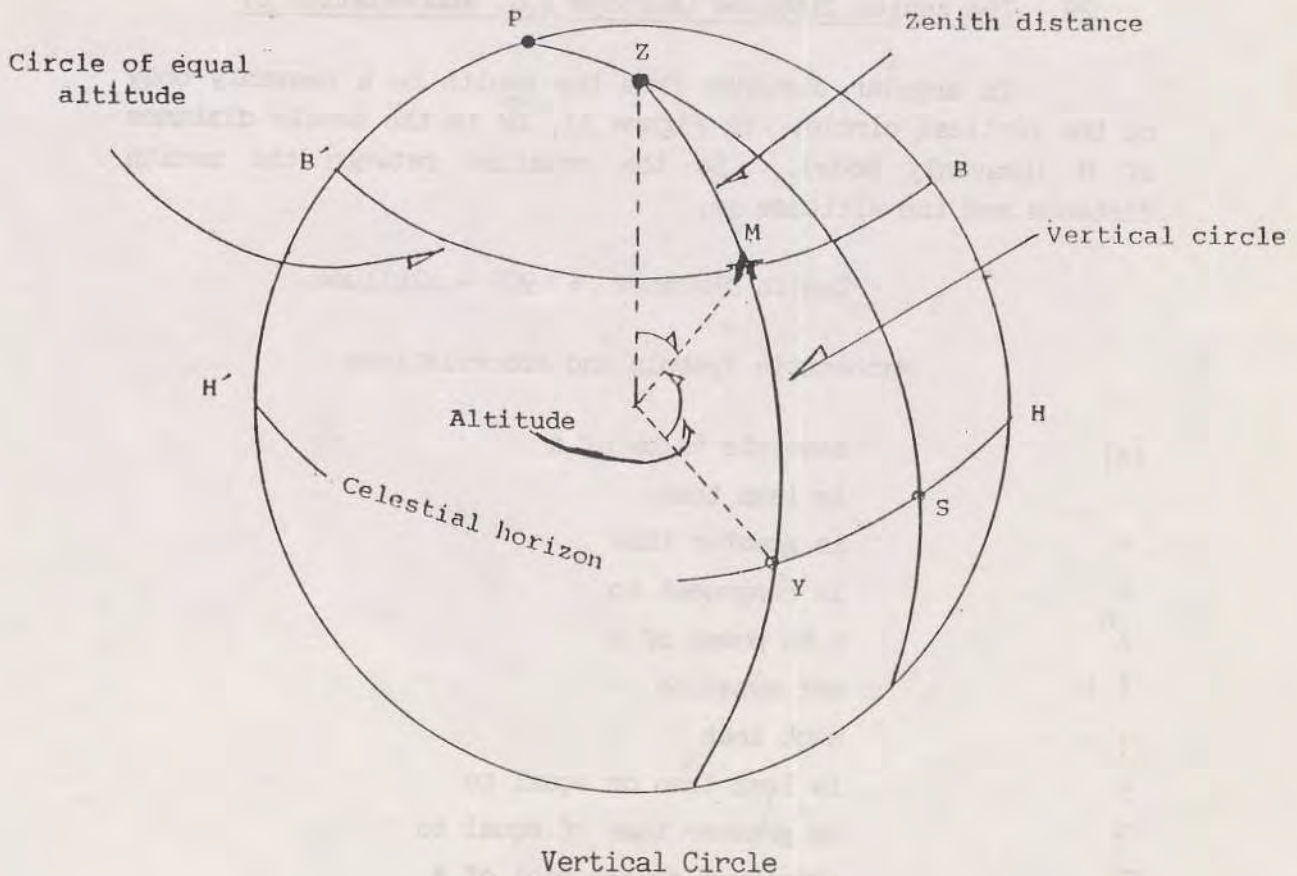


Fig. 11

The vertical circle is sometimes called the circle of altitude or the azimuth circle

In Figure 11, \widehat{PZS} is the celestial meridian, and the small circle including a heavenly body which is parallel to the celestial horizon is called the circle of equal altitude, $\widehat{BMB'}$ in Figure 11.

28. The altitude (of M) (abbreviation alt, or a)

Is the angular distance from horizon to the heavenly body on the vertical circle. In Figure 11, \widehat{YM} is the altitude of M (heavenly body).

29. The zenith distance (acronym Z.D. abbreviation Z)

Is angular distance from the zenith to a heavenly body on the vertical circle. In Figure 11, \widehat{ZM} is the zenith distance of M (heavenly body). So the relation between the zenith distance and the altitude is,

$$\text{Zenith distance} = 90^\circ - \text{altitude}$$

Mathematic Symbols and Abbreviations

$ a $	absolute value of a
$<$	is less than
$>$	is greater than
\cong	is congruent to
x^n	n th power of x
$\{ \}$	set notation
$:$	such that
\leq	is less than or equal to
\geq	is greater than or equal to
\sqrt{a}	principal square root of a
$\sqrt[n]{a}$	principal n th root of a
$\pm a$	a or the opposite of a
\vec{AB}	Vector from A to B
AB	distance between A and B
$f(x)$	value of function f for a given x
\overline{AB}	line segment AB
A^{-1}	multiplicative inverse of matrix A

$\log_b x$	logarithm of x, base b,
$\log x$	common logarithm of x
$\sum_{n=1}^6 A_n$	summation notation (sigma)
<	angle
sin	sine
cos	cosine
tan	tangent
csc	cosecant
sec	secant
cot	cotangent
ABC	triangle ABC
$\sin^2 \theta$	square of sin
+	plus (addition)
-	minus (subtraction)
\pm	plus or minus
~	difference
•	multiplied by
x	times (multiplication)
÷	divided by (division)
∴	therefore
∵	because
=	equals
≠	not equal to
≈	nearly equal to
∫	integral sign
∞	infinity
....	repeating decimal

On positions



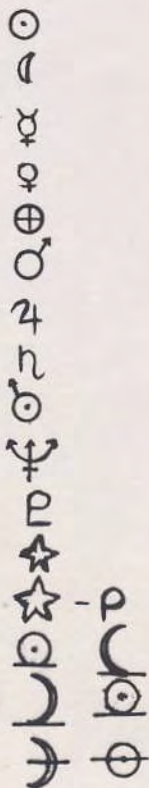
dead reckoning position

fix

estimated position

symbol used for one set of fixes when simultaneously fixing by two means, e.g. visual and radar sometimes used for radionavigation fix

On celestial bodies



Sun

Moon

Mercury

Venus

Earth

Mars

Jupiter

Saturn

Uranus

Neptune

Pluto

Star

Star-planet altitude Correction (altitude)

Lower limb

Center

upper limb



new moon
 crescent moon
 first quarter
 gibbous moon
 full moon
 gibbous moon
 last quarter
 crescent moon

On signs of zodiac



Aries (vernal equinox)
 Taurus
 Gemini
 Cancer (summer solstice)
 Leo
 Virgo
 Libra (autumnal equinox)
 Scorpius
 Sagittarius
 Capricornus (winter solstice)
 Aquaries
 Pisces

On years and degrees

y	Years
m	Months
d	Days
h	Hours
.m	Minutes of time
s	Seconds of time
°	Degrees
'	minutes of arc
"	seconds of arc

Greek Alphabet

A α a	alpha
B β B	Beta
Γ γ	Gamma
Δ δ	Delta
E ε	Epsilon
Z ζ	Zeta
H η	Eta
Θ θ	Theta
I ι	Iota
K κ	Kappa
Λ λ	Lambda
M μ	Mu
N ν	Nu
Ξ ξ	Xi
Ο ο	Omicron
Π π	Pi
P ρ	Rho
Σ σ	Sigma
T τ	Tau
Υ υ	Upsilon
Φ φ	Phi
X χ	Chi
Ψ ψ	Psi
Ω ω	Omega

30. The prime vertical

The prime vertical is a vertical circle which is perpendicular to the celestial meridian. This is a great connecting the zenith, the east point and the west point on the celestial horizon (Fig. 12)

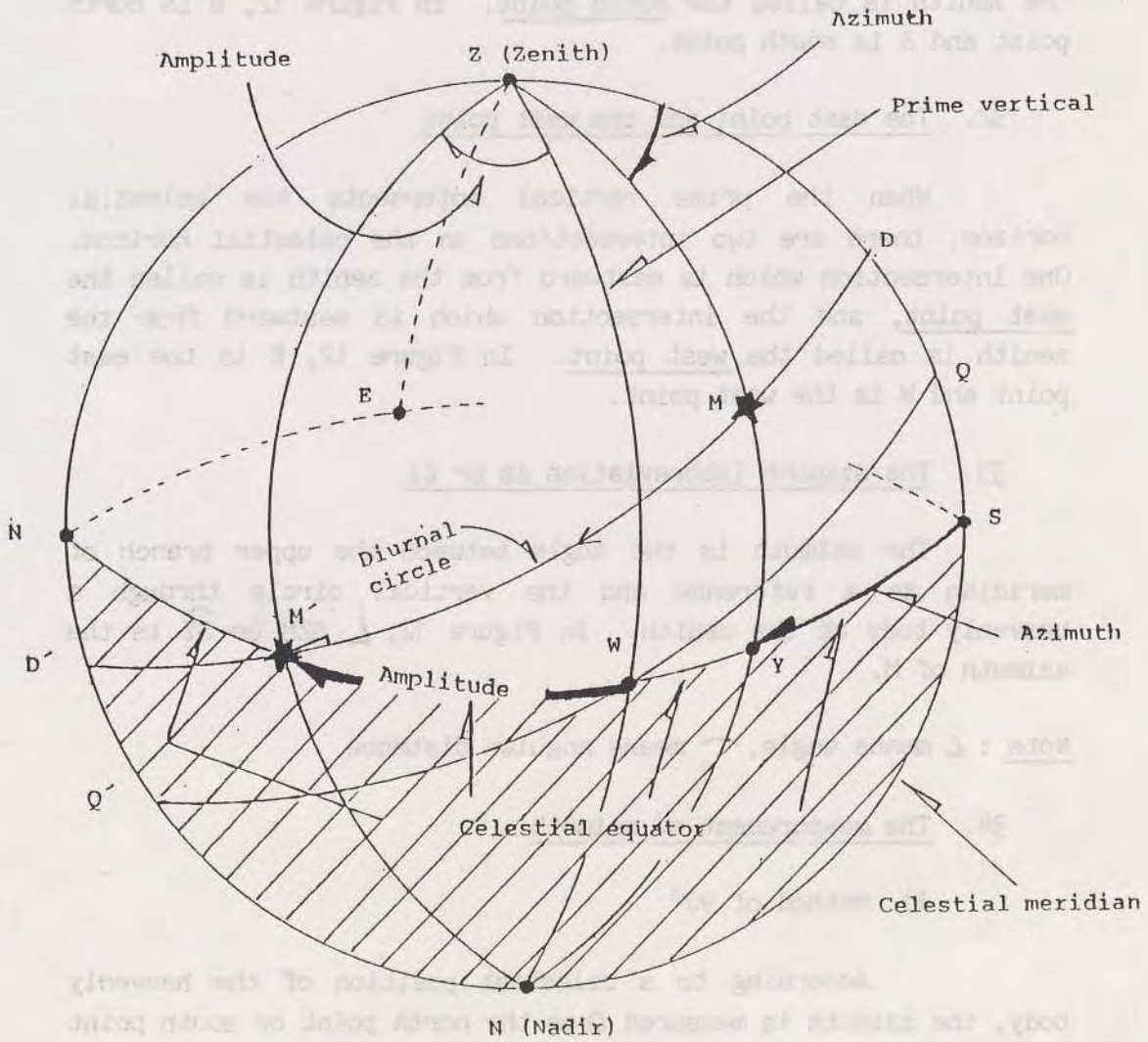


Fig. 12

31. The north point and the south point

When the celestial meridian intersects the celestial horizon, there are two intersections on the celestial horizon. Then one intersection which is northward from the zenith is called the north point, and the other intersection southward from the zenith is called the south point. In Figure 12, N is north point and S is south point.

32. The east point and the west point

When the prime vertical intersects the celestial horizon, there are two intersections on the celestial horizon. One intersection which is eastward from the zenith is called the east point, and the intersection which is westward from the zenith is called the west point. In Figure 12, E is the east point and W is the west point.

33. The azimuth (abbreviation Az or Z)

The azimuth is the angle between the upper branch of meridian as a reference and the vertical circle through a heavenly body at the zenith. In Figure 12, \angle SZM or \widehat{SY} is the azimuth of M.

Note : \angle means angle, $\widehat{\quad}$ means angular distance

34. The measurement of azimuth

1) Method of 90°

According to a celestial position of the heavenly body, the azimuth is measured from the north point or south point to the east point or the west point, starting from 0° to 90° . The value of the azimuth should be given the prefix N or S, and the suffix E or W.

2) Method of 180°

According to the observer's position, the azimuth is measured from the north point or the south point to the east point or the west point, starting from 0° to 180° . The value of the azimuth should be given the prefix N or S and the suffix E or W.

3) Method of 360° (clockwise)

The azimuth is measured from the north point as a reference to the eastward, starting from 0° to 360° . The prefix and the suffix are not necessary for the value of the azimuth.

35. Amplitude (abbreviation = Amp.)

Amplitude is the angle between the east point or the west point and the intersection where the diurnal circle intersects the celestial horizon. In Figure 12, $\angle WZM'$ or $\widehat{WM'}$ is the amplitude of M'

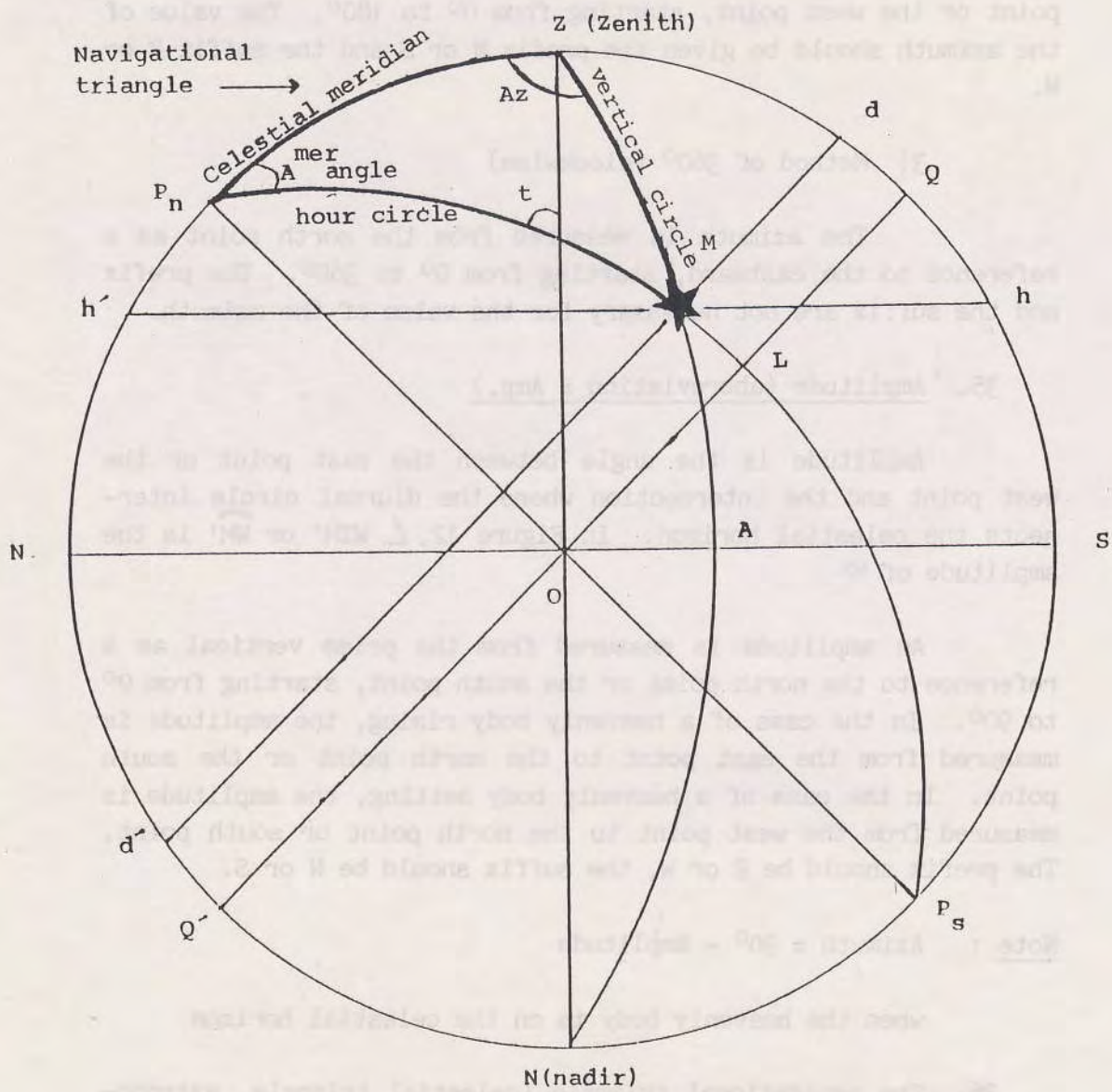
An amplitude is measured from the prime vertical as a reference to the north point or the south point, starting from 0° to 90° . In the case of a heavenly body rising, the amplitude is measured from the east point to the north point or the south point. In the case of a heavenly body setting, the amplitude is measured from the west point to the north point or south point. The prefix should be E or W, the suffix should be N or S.

Note : Azimuth = 90° - Amplitude

when the heavenly body is on the celestial horizon

36. The navigational triangle (celestial triangle, astronomical triangle, position triangle)

The navigation triangle is a spherical triangle which is formed by arcs of the observer's celestial meridian (a great circle connecting the zenith with a celestial pole), a vertical circle (a great circle connecting the zenith and a heavenly body) and an hour circle (a great circle connecting a celestial pole and a heavenly body) (Fig. 13).



The navigation triangle

Fig. 13

The navigation triangle is a spherical triangle which is formed by arcs of the celestial sphere. It is bounded by arcs of the celestial meridian (a great circle connecting the zenith with a celestial pole), a vertical circle (a great circle connecting the zenith with a heavenly body), and an hour circle (a great circle connecting a celestial pole and a heavenly body) (Fig. 13).

In Figure 13

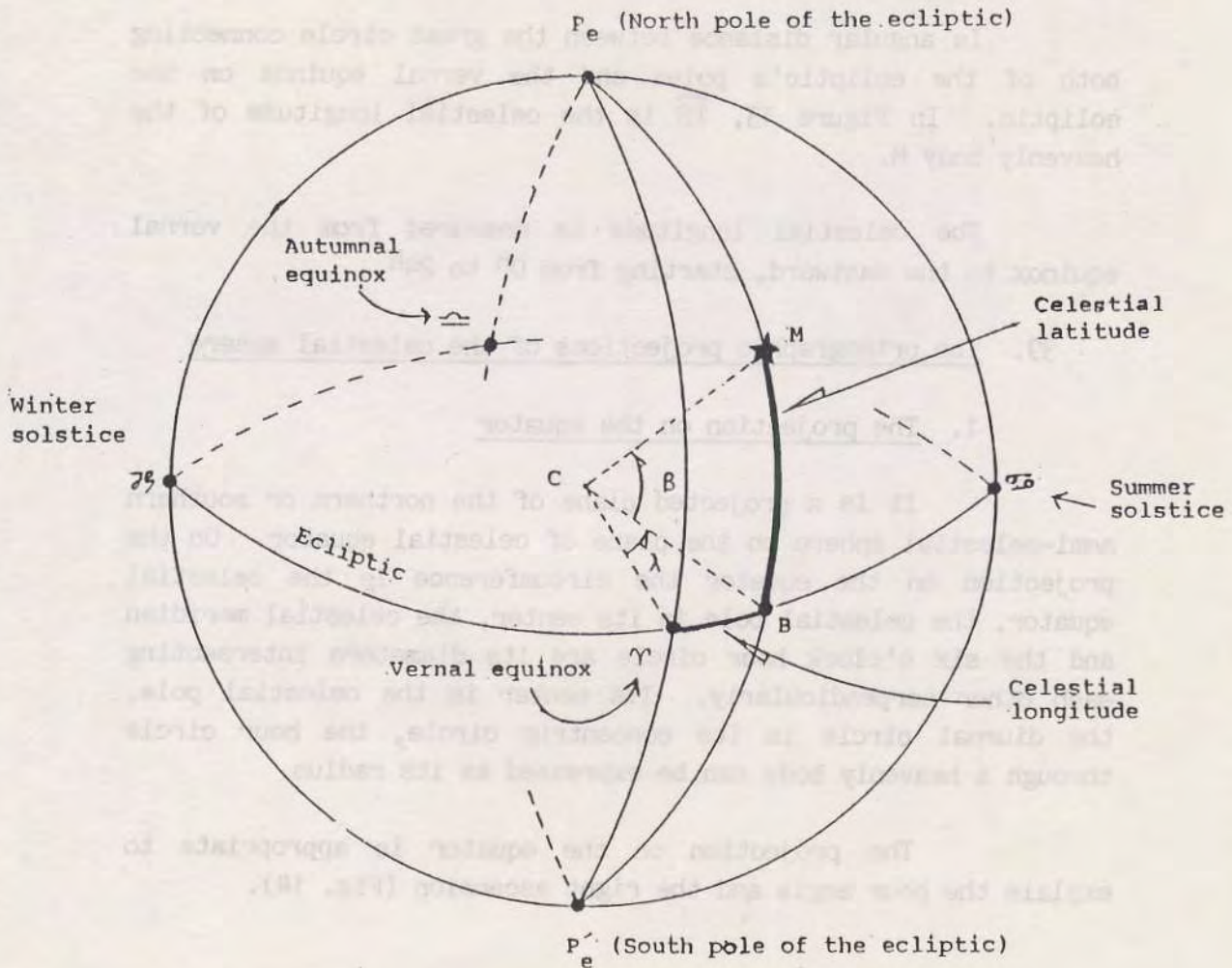
1. The earth is at the center, O.
2. The heavenly body is at M.
3. $\overline{dd'}$ is the parallel of declination of the heavenly body M.
4. $\overline{hh'}$ is the altitude circle of the heavenly body M.
5. \widehat{QZ} of the the celestial meridian is the latitude of the observer'.
6. $\widehat{P_nZ}$, one side of the triangle, is the colatitude.
7. \widehat{AM} of the vertical circle is the altitude of the heavenly body.
8. \widehat{ZM} , one side of the triangle, is the zenith distance or coaltitude.
9. \widehat{LM} of the hour circle is the declination of the heavenly body M.
10. $\widehat{P_nM}$, one side of the triangle, is the polar distance or codeclination.
11. The angle at P_n ($\widehat{ZP_nM}$), having the hour circle and the celestial meridian as sides, is the meridian angle.
12. The angle at the Z ($\widehat{P_nZM}$), having the vertical circle and that arc of the celestial meridian which includes the elevated pole as sides, is the azimuth angle.
13. The angle at M ($\widehat{ZMP_n}$), having the hour circle and the vertical circle as sides, is the parallactic angle (x), which is not generally used by the navigator.

The navigational triangle is utilized for solution of problems by navigators as follows:

1. Given latitude, declination, and the meridian angle, to find altitude and azimuth angle. This is used in the reduction of a celestial observation, to establish a line of position.
2. Given latitude, altitude, and azimuth angle to find declination and meridian angle. This is used to identify an unknown celestial body.
3. Given meridian angle, declination, and altitude, to find azimuth angle. This is used to find azimuth when the latitude is known.
4. Given the latitude of two places on the earth and the difference of longitude between them; to find the initial great-circle course and the great-circle distance.

37. The celestial latitude and the celestial longitude

The celestial latitude (abbreviation = Cel. Lat. symbol β) is angular distance from the ecliptic to the heavenly body on the great circle connection the poles of the ecliptic and the heavenly body (Fig. 13)



Celestial latitude & longitude

Fig. 13a

In Figure 13, \widehat{BM} is the celestial latitude of the heavenly body M . The celestial latitude is measured from the ecliptic to the northward or southward, starting from 0° to 90° and it has the suffix N or S .

38. The celestial longitude (abbreviation = Cel.Long. symbol = λ)

Is angular distance between the great circle connecting both of the ecliptic's poles and the vernal equinox on the ecliptic. In Figure 13, \widehat{TB} is the celestial longitude of the heavenly body M.

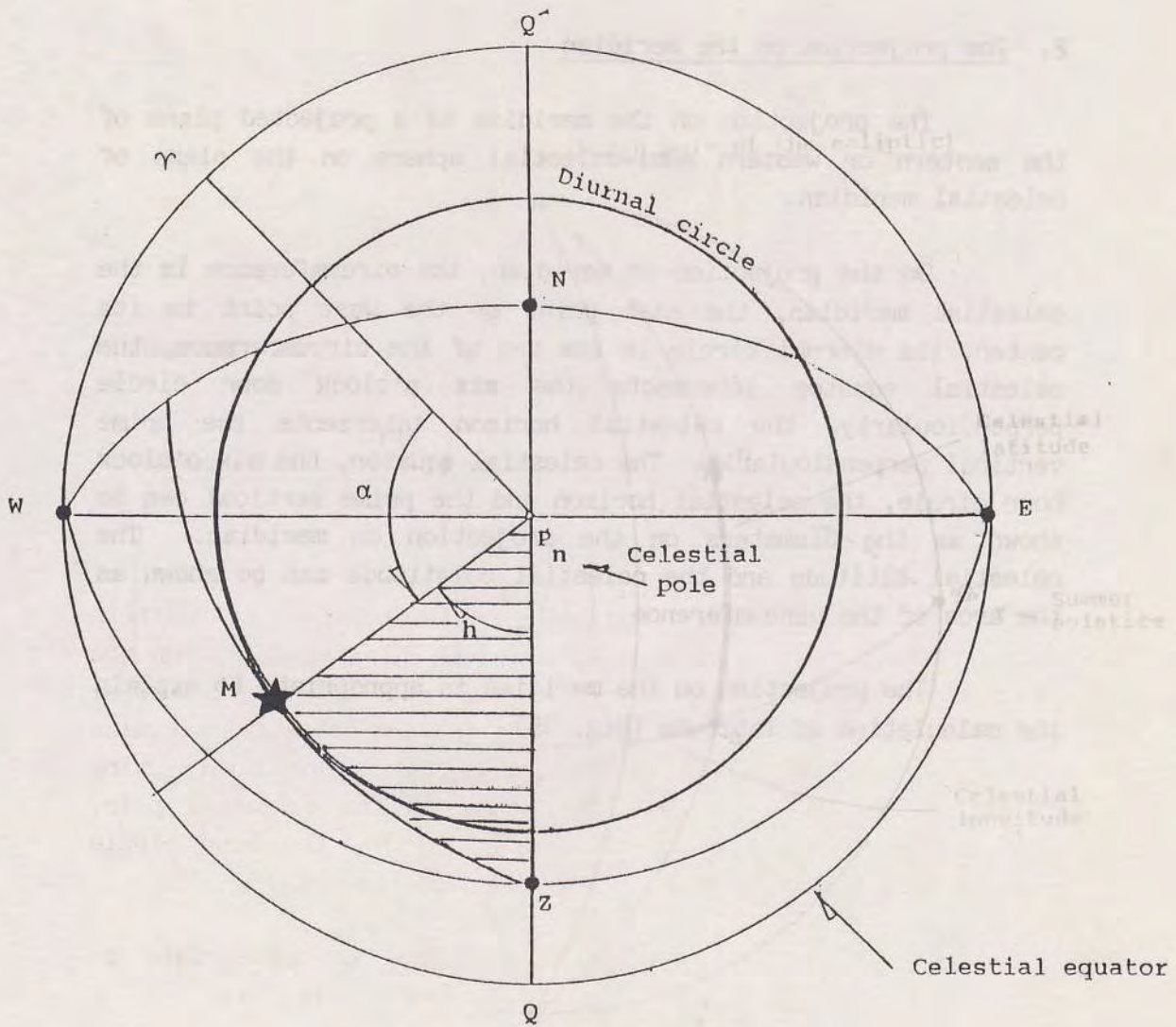
The celestial longitude is measured from the vernal equinox to the eastward, starting from 0^h to 24^h .

39. The orthographic projections of the celestial sphere

1. The projection on the equator

It is a projected plane of the northern or southern semi-celestial sphere on the plane of celestial equator. On the projection on the equator the circumference is the celestial equator, the celestial pole is its center, the celestial meridian and the six o'clock hour circle are its diameters intersecting each other perpendicularly. Its center is the celestial pole, the diurnal circle is its concentric circle, the hour circle through a heavenly body can be expressed as its radius.

The projection on the equator is appropriate to explain the hour angle and the right ascension (Fig. 14).



Projection on the equator

Fig. 14

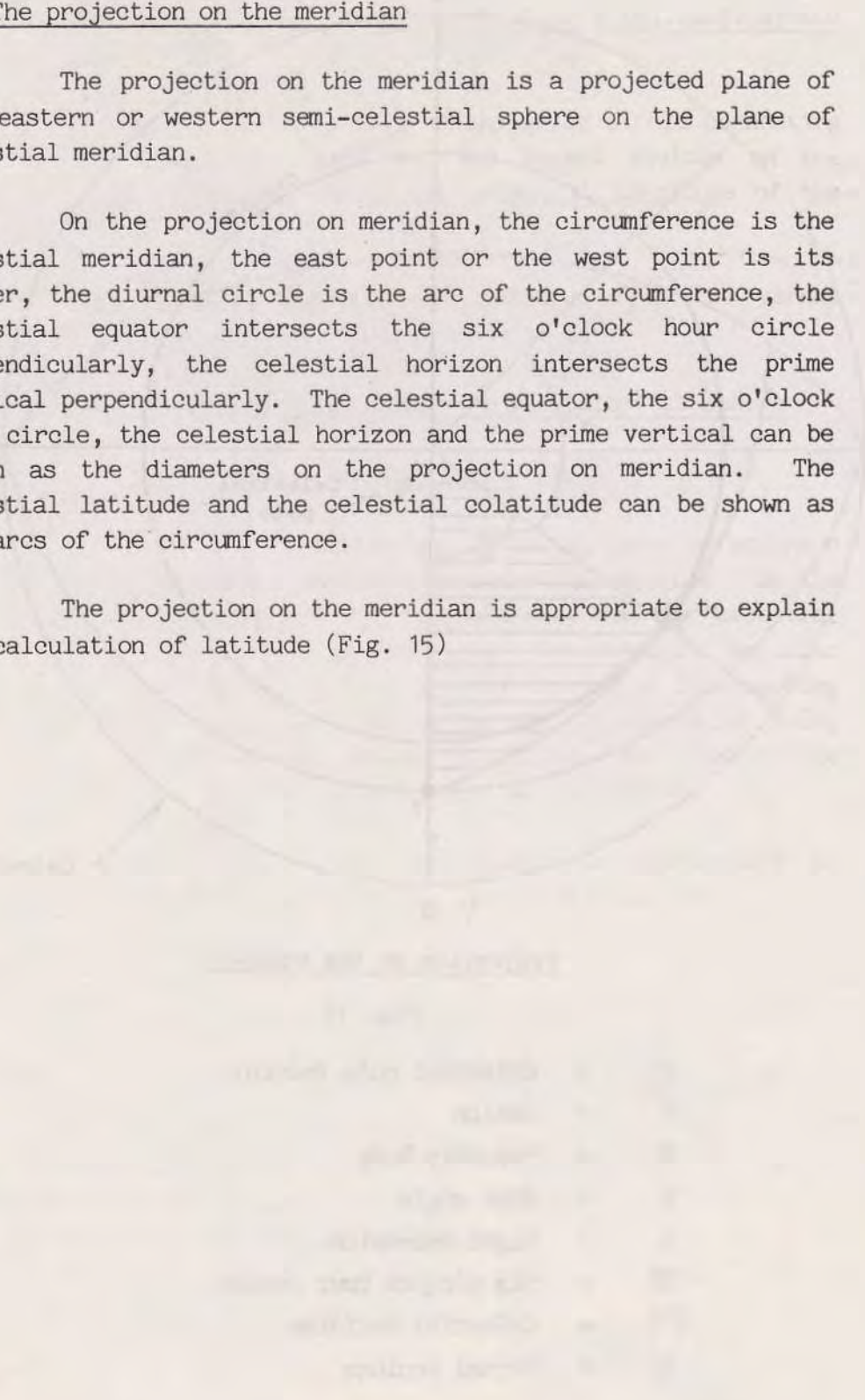
- P_n = Celestial pole (north)
- Z = Zenith
- M = Heavenly body
- h = Hour angle
- α = Right ascension
- \overline{WE} = Six o'clock hour circle
- $\overline{Q'Q}$ = Celestial meridian
- T = Vernal equinox

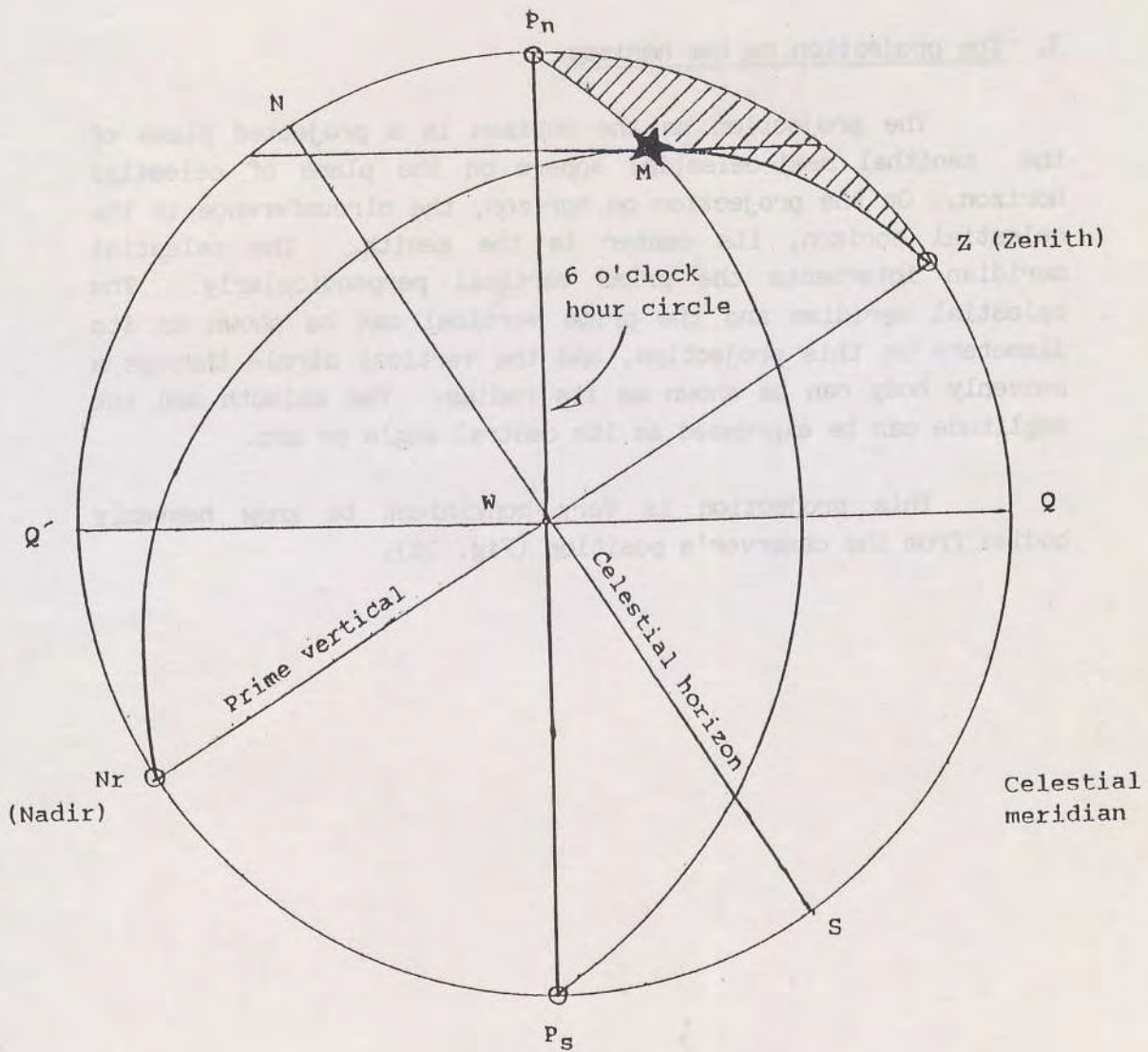
2. The projection on the meridian

The projection on the meridian is a projected plane of the eastern or western semi-celestial sphere on the plane of celestial meridian.

On the projection on meridian, the circumference is the celestial meridian, the east point or the west point is its center, the diurnal circle is the arc of the circumference, the celestial equator intersects the six o'clock hour circle perpendicularly, the celestial horizon intersects the prime vertical perpendicularly. The celestial equator, the six o'clock hour circle, the celestial horizon and the prime vertical can be shown as the diameters on the projection on meridian. The celestial latitude and the celestial colatitude can be shown as the arcs of the circumference.

The projection on the meridian is appropriate to explain the calculation of latitude (Fig. 15)





Projection on meridian

Fig. 15

- W = West point
- $\overset{\frown}{P_n Q' P_s Q}$ = Celestial meridian
- \overline{NS} = Celestial horizon
- $\overline{Z Nr}$ = Prime vertical
- M = Heavenly body

3. The projection on the horizon

The projection on the horizon is a projected plane of the zenithal semi-celestial sphere on the plane of celestial horizon. On the projection on horizon, the circumference is the celestial horizon, its center is the zenith. The celestial meridian intersects the prime vertical perpendicularly. The celestial meridian and the prime vertical can be shown as its diameters on this projection, and the vertical circle through a heavenly body can be shown as its radius. The azimuth and the amplitude can be expressed as its central angle or arc.

This projection is very convenient to know heavenly bodies from the observer's position (Fig. 16).

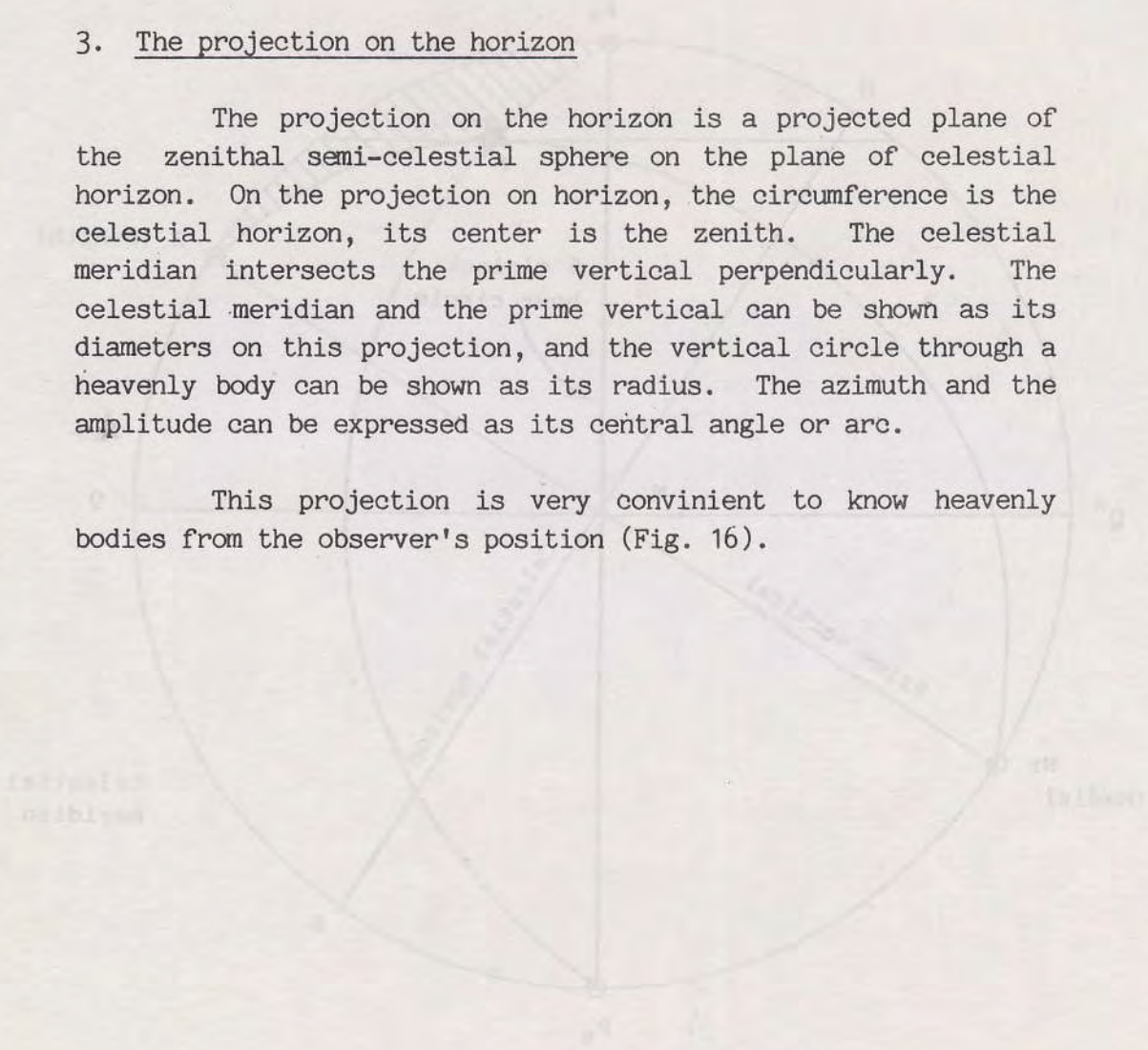
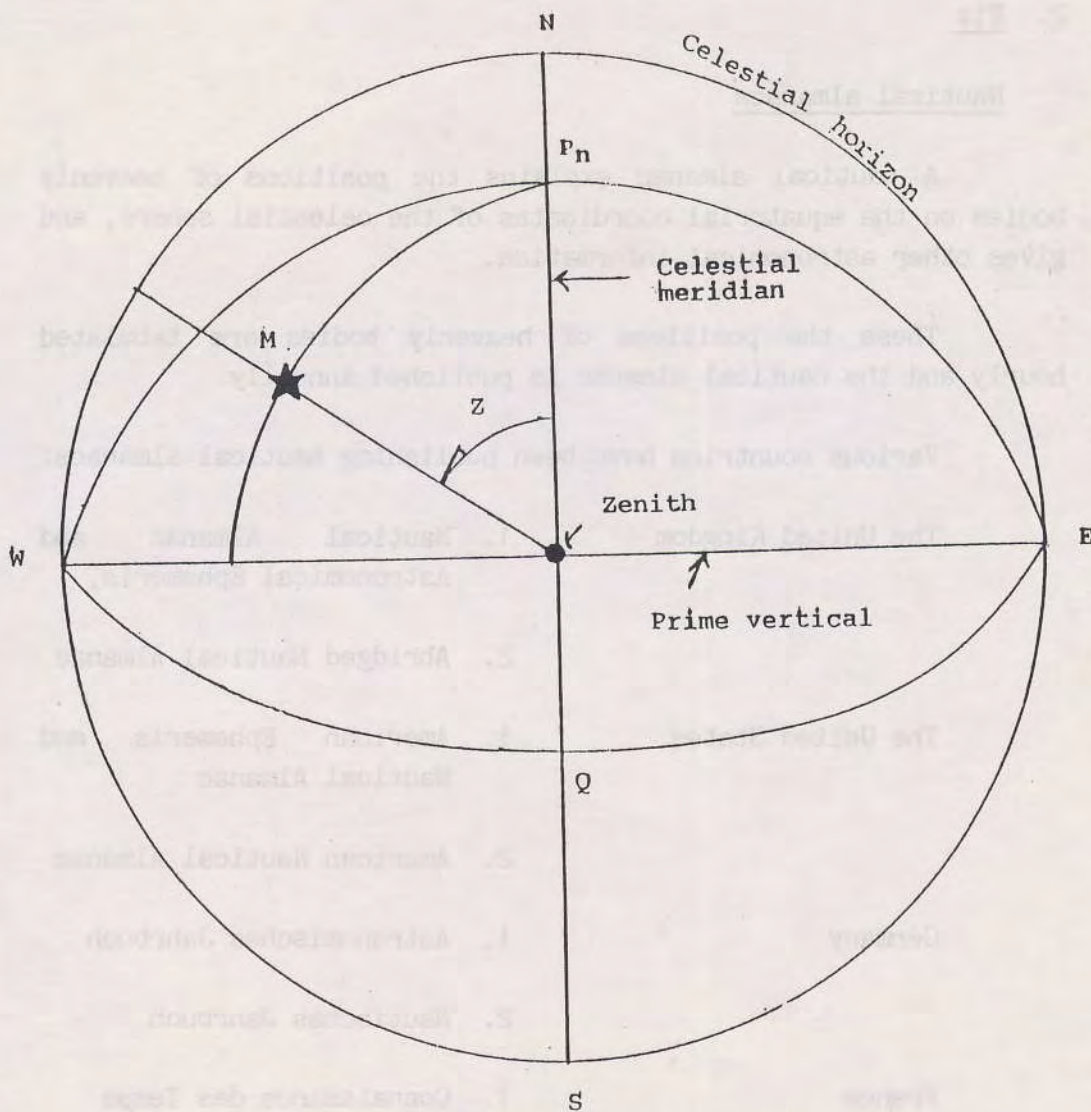


Fig. 16
Projection of the zenithal semi-celestial sphere on the plane of the celestial horizon.



Heavenly Body & an Observer

Fig. 16

- z = Azimuth
- \overline{WE} = Prime vertical
- \overline{NS} = Celestial meridian
- M = Heavenly body

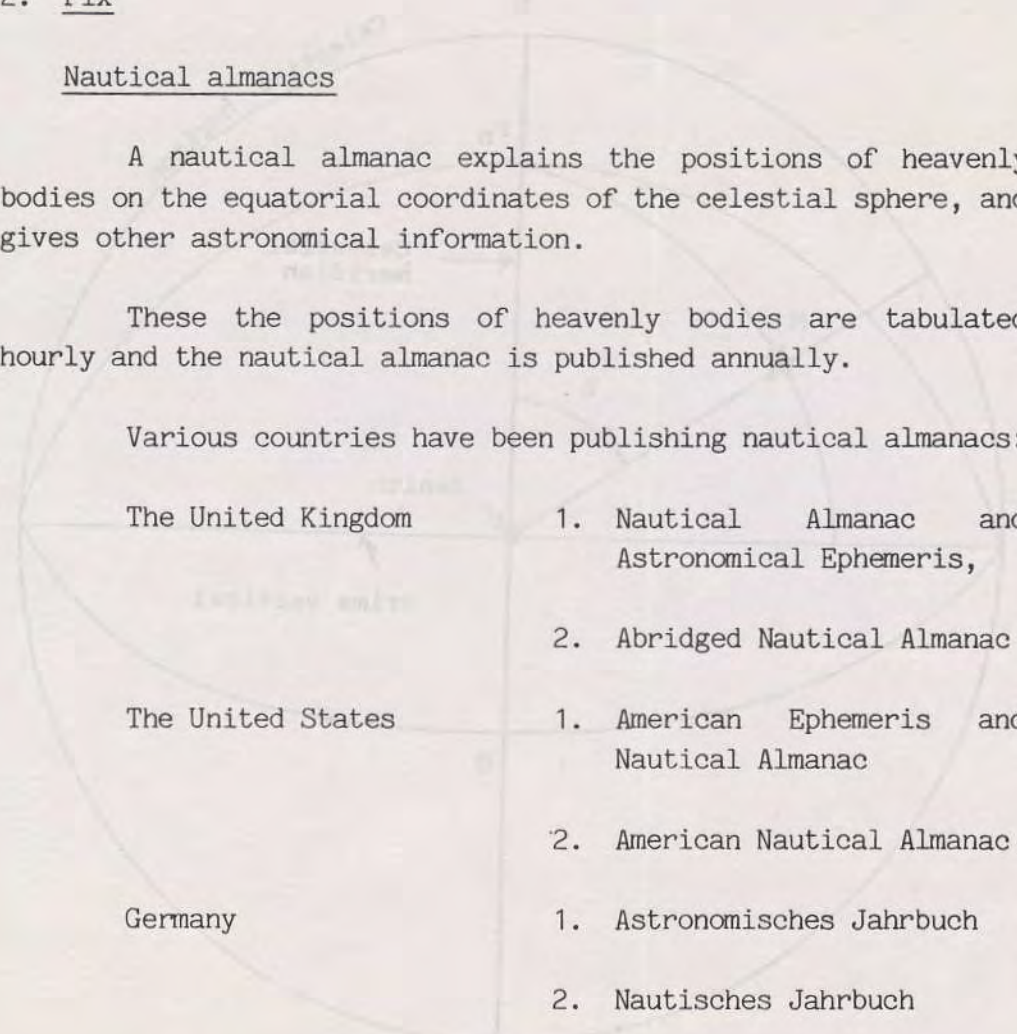
2. Fix

Nautical almanacs

A nautical almanac explains the positions of heavenly bodies on the equatorial coordinates of the celestial sphere, and gives other astronomical information.

These the positions of heavenly bodies are tabulated hourly and the nautical almanac is published annually.

Various countries have been publishing nautical almanacs:



The United Kingdom	1. Nautical Almanac and Astronomical Ephemeris, 2. Abridged Nautical Almanac
The United States	1. American Ephemeris and Nautical Almanac 2. American Nautical Almanac
Germany	1. Astronomisches Jahrbuch 2. Nautisches Jahrbuch
France	1. Connaissance des Temps 2. Ephemerides Nautiques
Japan	1. Nautical Almanac 2. Abridged Nautical Almanac

In these almanacs, the astronomical information is tabulated to a practical degree of accuracy, such as 0'.1 of arc and 1^s of time at hourly intervals.

The major part of the nautical almanac consists of the value of greenwich hour angle and declination, GHA of Aries and both GHA and the declination of Venus, Mars, Jupiter, and Saturn, also SHA and the declination of stars. The GHA and declination of the sun and moon, and the horizontal parallax of the moon, are tabulated.

For the sun and the moon, the time of transit is given for each day. For the moon, both upper and lower transits and the age and the phase are given in the table. Altitude corrections of sextant and dip table are also given.

Before calculating greenwich hour angle, declination, etc. by making use of a nautical almanac, please study how to use a programmable calculator CASIO fx-4000 P on page 43.

Altitude corrections

The altitude of a heavenly body is the angular distance from the horizon to the heavenly body on the vertical circle or the altitude is an included angle between the center of the heavenly body and the plane of the celestial horizon at the center of the earth. But as a matter of fact, it is impossible for us to measure this altitude (the true altitude) or the included angle. Usually, navigators measure altitude by marine sextant, and the altitude is the angular distance from the apparent horizon to the heavenly body.

This altitude obtained with the sextant is called Sextant Altitude (Sex. alt.) and corrected altitude by index error is called Observed Altitude (Obs. alt. or A_o). Then the observed altitude is the included angle between the lower limb or the upper limb (in the case of the sun and the moon) or the center (in the case of stars and planets) of the heavenly body and the plane of apparent horizon to the observer's eye.

This observed altitude is under the effects of many factors and quite different from the true altitude.

To obtain the true altitude of a heavenly body, the correction (astronomical refraction, dip of horizon, parallax, apparent semidiameter, index error) should be added to the sextant altitude.

Altitude correction

The altitude of a heavenly body is the angular distance from the horizon to the heavenly body on the vertical circle. The altitude is an included angle between the center of the heavenly body and the plane of the celestial horizon at the center of the earth. But as a matter of fact, it is impossible for us to observe this altitude (see true altitude) or the included angle. Usually navigators observe altitude by sextant, and the altitude is the angular distance from the apparent horizon to the heavenly body.

Nautical Almanac

52 Example of 1985 MARCH 5, 6, 7 (TUES., WED., THURS.)

Table with columns for G.M.T. (M, D, H), Planets (ARIES, VENUS, MARS, JUPITER, SATURN), and STARS. Rows represent dates from March 5 to March 23, 1985. Data includes G.H.A., Dec., and Name for stars.

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Computation of DMS by CASIO fx-4000 p.

Example

$41^{\circ}49'8$

$11^{\circ}48'3 +$

$53^{\circ}38'1$

Keystrokes

4	1	°"	4	9	'	8	°"	+
1	1	°"	4	8	'	3	°"	EXE
SHIFT	°"							

Display

53.635

$53^{\circ}38'6''$

(= $53^{\circ}38'1$)

$\frac{6''}{60''} = 0.1$

Example

$18^{\circ}33'2$

$0'5 -$

$18^{\circ}32'7$

1	8	°"	3	3	'	2	°"	-
0	0	°"	/	0	'	5	°"	EXE
SHIFT	°"							

18.545

$18^{\circ}32'42''$

(= $18^{\circ}32'7$)

$\frac{42''}{60''} = 0.7$

Example

$297^{\circ}12'0$

$11^{\circ}16'0$

$8'0 +$

$308^{\circ}36'0$

2	9	7	°"	1	2	'	0	°"	+
/	1	1	°"	1	6	'	0	°"	+
/	0	0	°"	/	8	'	0	°"	EXE
SHIFT	°"								

308.600

$308^{\circ}36'00''$

(= $308^{\circ}36'0$)

$\frac{00''}{60''} = 0.0$

Example

$319^{\circ}54'9$

$14^{\circ}22'0$

$(-) 0'3 +$

$334^{\circ}16'6$

3	1	9	°"	5	4	'	9	°"	+
/	1	4	°"	2	2	'	0	°"	+
(-)	0	0	°"	/	0	'	3	°"	EXE
SHIFT	°"								

334.227

$334^{\circ}16'36''$

(= $334^{\circ}16'6$)

$\frac{36''}{60''} = 0.6$

Example

1	5	8	0''	5	1	0	5	0''	+
2	1	5	0''	4	4	0	9	0''	+
/	/	7	0''	4	2	0	5	0''	+
(-)	3	6	0	'	EXE				
SHIFT	0''								

$158^{\circ}51'5$ →
 $215^{\circ}44'9$ →
 $7^{\circ}42'5$ →
 $-)360^{\circ} +$ →
 $22^{\circ}18'9$

22.35
 $22^{\circ}18'54''$
 $(=22^{\circ}18'9)$
 $\frac{54''}{60''} = 0.9$

Example

/	2	4	0''	4	9	0	3	0''	+
/	1	2	0''	1	2	0	8	0''	+
/	0	0	0''	/	0	0	6	0''	+
(-)	7	1	0''	1	2	0	0	0''	+
3	6	0	0''	EXE					
SHIFT	0''								

$24^{\circ}49'3$ →
 $12^{\circ}12'8$ →
 $0'6$ →
 $(-)71^{\circ}12'6$ →
 $360^{\circ} +$ →
 $325^{\circ}50'7$

325.845
 $325^{\circ}50'42''$
 $(=325^{\circ}50'7)$
 $\frac{42''}{60''} = 0.7$

How to compute Greenwich Day (GD) and Greenwich Mean Time (GMT)

Example

Required:- Approximate Greenwich Day (GD) and Greenwich Mean Time (GMT)

where :- Ship's time = March 21st 14^h 25^m 18^s. Longitude = 139°46'E.

Ans. 21/3 05^h 06^m 14^s

Ship's time 21/3 14^h 25^m 18^s
 Long. in time 09 19 04 ⊖ (= 139°46'E + 15)
 Approx. GD & GMT 21/3 05^h 06^m 14^s

Keystrokes (fx-4000 p)										Display
1	4	0 ^o ''	2	5	0 ^o ''	1	8	0 ^o ''	-	
(1	3	9	0 ^o ''	4	6	0 ^o ''	+	1	
5	EXE	→								5.104
SHIFT	0 ^o ''	→								5°6'14"

Ref. 1. 1 hour = 15°, See NAVIGATION TABLES TD/LN/52 Rev. page 1 "Conversion of Arc to Time".

-(E)

2. GMT = Local Mean Time (or ship's time) +(W) longitude (⊖) See NAVIGATION TABLE TD/LN/52 Rev. page 97 & 104.

Example

Required:- Approximate GD & GMT and also GMT.

where :- Ship's time November 16th, 14^h 15^m. Chronometer time (CT) 04^h 50^m 20^s. Chronometer error (CE) ⊖ 0^m 28^s. Longitude 38°48'W.

Ans. 16/11 16^h 49^m 52^s

Ship's time 16/11	14 ^h 15 ^m 00 ^s
Long. in time	2 35 12 ⊕ (= 38°48'W ÷ 15)
GD & Approx. GMT 16/11	16 50 12
CT	04 ^h 50 ^m 20 ^s
CE	0 28 ⊖
Corr. ^d CT	04 49 52
	+ 12 (Because of Approx. GMT. = 16 ^h 50 ^m 12 ^s)
GD & GMT 16/11	16 ^h 49 ^m 52 ^s

Keystrokes (fx-4000 p)										Display
1	4	°	1	5	°	+	(3	8	
°	4	8	°	÷	1	5	EXE			16.837
SHIFT	°									16°50'12" ← Approx. GMT
4	°	5	0	°	2	0	°	-	0	
°	0	°	2	8	°	+	1	2	°	
EXE										16.831
SHIFT	°									16°49'52" ← GMT

Example

Required:- Approximate GD & GMT and also GMT.

Where :- Ship's time April 27th 05^h 22^m. GT 07^h 13^m 17^s
 Longitude 155°07'E. CE ⊖ 12^m 58^s

Ans. 26/4 19^h 00^m 19^s

Ship's time 27/4	05 ^h 22 ^m 00 ^s
Long. in time (LT)	10 20 28 ⊖ (= 155°07'E + 15)
	- 04 58 28
	+ 24
Approx. GD & GMT 26/4	19 01 32
CT	07 13 17
CE	12 58 ⊖
Corr. ^d CT	07 00 19
	+ 12 (Because of Approx. GMT
	= 19 ^h 01 ^m 32 ^s)
GD & GMT 26/4	19 ^h 00 ^m 19 ^s

Keystrokes (fx-4000 p)										Display
5	0 ^o "	2	2	0 ^o "	-	(1	5	5	
0 ^o "	7	0 ^o "	+	1	5	0 ^o ")	+	2	
4	0 ^o "	EXE								19.026
SHIFT	0 ^o "									19°01'32" ← Approx. GMT
7	0 ^o "	1	3	0 ^o "	1	7	0 ^o "	-	0	
0 ^o "	1	2	0 ^o "	5	8	0 ^o "	+	1	2	
0 ^o "	EXE									19.005
SHIFT	0 ^o "									19°00'19" ← GMT

Problems: Required approximate GD, GMT and GMT.

#	Date	Ship's time	D.R.P.	Chro. time	Chro. error	Approx. GD&GMT	GD & GMT
1.	14/9/56	18h 00m	26°15' N 141°27' E	09h 46m 25s	⊖ 01h 01m 12s	?	?
2.	6/7/56	06h 50m	34°28' N 135°00' E	10h 21m 50s	⊖ 00h 29m 26s	?	?
3.	27/4/56	04h 20m	32°32' N 133°46' E	07h 24m 18s	⊖ 00h 01m 36s	?	?
4.	5/8/56	04h 35m	21°13' N 161°35' W	03h 14m 35s	⊕ 00h 12m 43s	?	?
5.	16/11/56	12h 00m	04°06' S 41°28' E	08h 21m 38s	⊕ 00h 04m 13s	?	?
6.	22/3/56	12h 00m	02°10' N 70°10' E	06h 58m 53s	⊖ 00h 00m 16s	?	?
7.	10/6/56	09h 20m	32°32' N 133°46' E	00h 43m 37s	⊖ 00h 16m 17s	?	?
8.	12/12/56	15h 30m	04°06' S 41°28' E	00h 40m 20s	⊖ 00h 02m 35s	?	?
9.	6/5/79	05h 00m	06°10' N 141°35' E	07h 54m 57s	⊕ 00h 00m 05s	?	?
10.	6/5/79	05h 00m	06°10' N 141°35' E	08h 00m 41s	⊕ 00h 00m 05s	?	?
11.	10/10/79	05h 00m	18°47' S 103°43' W	11h 54m 44s	⊕ 00h 00m 04s	?	?

#	Date	Ship's time	D.R.P.	Chro. time	Chro. error	Approx. GD&GMT	GD & GMT
12.	10/10/79	05 ^h 00 ^m	18°47' S 103°43' W	11 ^h 58 ^m 20 ^s	⊕ 00 ^h 00 ^m 04 ^s	?	?
13.	10/9/63	07 ^h 30 ^m	19°56' N 128°24' E	10 ^h 31 ^m 24 ^s	⊕ 00 ^h 23 ^m 10 ^s	?	?
14.	10/9/63	11 ^h 00 ^m	19°26.4N 128°20.6E	02 ^h 04 ^m 02 ^s	⊕ 00 ^h 23 ^m 10 ^s	?	?
15.	13/6/85	05 ^h 17 ^m	17°11.3N 118°23.4E	09 ^h 08 ^m 00 ^s	Nil	?	?
16.	13/6/85	05 ^h 17 ^m	17°11.3N 118°23.4E	09 ^h 10 ^m 30 ^s	Nil	?	?

Answers:

#	Approx. GD & GMT		GD & GMT		Remarks
1.	14/9	08 ^h 34 ^m 12 ^s	14/9	08 ^h 45 ^m 13 ^s	P. 60 Textbook TD/TRB/37 Rev.
2.	5/7	21 ^h 50 ^m 00 ^s	5/7	21 ^h 52 ^m 24 ^s	P. 88
3.	26/4	19 ^h 24 ^m 56 ^s	26/4	19 ^h 22 ^m 42 ^s	P. 91
4.	5/8	15 ^h 21 ^m 00 ^s	5/8	15 ^h 27 ^m 18 ^s	P. 101
5.	16/11	09 ^h 14 ^m 08 ^s	16/11	08 ^h 25 ^m 51 ^s	P. 108
6.	22/3	07 ^h 19 ^m 20 ^s	22/3	06 ^h 58 ^m 37 ^s	P. 110
7.	10/6	00 ^h 24 ^m 56 ^s	10/6	00 ^h 27 ^m 20 ^s	P. 126
8.	12/12	12 ^h 44 ^m 08 ^s	12/12	12 ^h 37 ^m 45 ^s	P. 162
9.	5/5	19 ^h 33 ^m 40 ^s	5/5	19 ^h 55 ^m 02 ^s	P. 190
10.	5/5	19 ^h 33 ^m 40 ^s	5/5	20 ^h 00 ^m 46 ^s	P. 191
11.	10/10	11 ^h 54 ^m 52 ^s	10/10	11 ^h 54 ^m 48 ^s	P. 197
12.	10/10	11 ^h 54 ^m 52 ^s	10/10	11 ^h 58 ^m 24 ^s	P. 198
13.	9/9	22 ^h 56 ^m 24 ^s	9/9	22 ^h 54 ^m 34 ^s	P. 205
14.	10/9	02 ^h 26 ^m 37.6 ^s	10/9	02 ^h 27 ^m 12 ^s	P. 209
15.	12/6	21 ^h 23 ^m 26.4 ^s	12/6	21 ^h 08 ^m 00 ^s	P. 239
16.	12/6	21 ^h 23 ^m 26.4 ^s	12/6	21 ^h 10 ^m 30 ^s	P. 240

INCREMENTS AND CORRECTIONS Page 60

47^m

47 ^m	SUN PLANETS	ARIES	MOON	v or Corr ⁿ d	v or Corr ⁿ d	v or Corr ⁿ d
00 ^s	11°45!0	11°46!9	11°12!9	0!0 0!0	6!0 4!8	12!0 9!5
01	11°45!3	11°47!2	11°13!1	0!1 0!1	6!1 4!8	12!1 9!6
---	---	---	---	---	---	---
05	11°46!3	11°48!2	11°14!1	0!5 0!4	6!5 5!1	12!5 9!9
06	11°46!5	11°48!4	11°14!3	0!6 0!5	6!6 5!2	12!6 10!0
---	---	---	---	---	---	---
13	11°48!3	11°50!2	11°16!0	1!3 1!0	7!3 5!8	13!3 10!5
14	11°48!5	11°50!4	11°16!2	1!4 1!1	7!4 5!9	13!4 10!6
---	---	---	---	---	---	---

The sun

GMT. 22 Jan. 83
 15h.....
 47^m-13^s
 15h-47^m-13^s

GHA
 42° - 06!6 (from almanac)
 11° - 48!3 ⊕ (from "increments and
 corrections")
 53° - 54!9 attention!
 =====

GMT. 22 Jan. 83
 15h.....
 47^m
 15h-47^m-13^s...

Declination
 S 19°- 42!7 d = 0!6 (from almanac ... at
 the foot of column)
 0!5 ⊖ -0.5 correction from the
 table "INCREMENTS AND
 CORRECTIONS".
 S 19°- 42!2
 ===== attention!

Ans. GHA 53°-54!9, Declination S. 19°-42!2

The moon

GMT. 22 Jan. '83	<u>GHA</u>	
15h.....	310°- 25!9	(from almanac)
47 ^m - 13 ^s	<u>11°- 16!0</u> ⊕	(from "increments and corrections")
	321°- 41!9	↑ attention!
	<u>9!6</u> ⊕	(from almanac, v is 12!1) v = 12.1 → correction = 9!6
15h - 47 ^m - 13 ^s	<u>321°-51!5</u> =====	from "increments and correction".
GMT. 22 Jan. 83	<u>Declination</u>	
15h.....	N 9°- 38!2	d = 12!3 → Correction 9!7
47 ^m	<u>9!7</u> ⊕	
15h - 47 ^m - 13 ^s	<u>N 9°- 47!9</u> =====	

Ans. GHA 321° - 51!5, Declination n 09° - 47!9

Example 2

What were the LHA and the declination of Venus on 22 Jan. 1983 at GMT 12^h 57^m 28^s at longitude E. 91° - 12'?

Solution

$$\text{LHA}(h) = \text{GHA} \pm \text{Longitude} \begin{matrix} \text{E } \oplus \\ \text{W } \ominus \end{matrix}$$

GMT	22 Jan. 83	GAH	v	Dec.	d
	12 ^h	337°- 23'3	0'6	S 15°- 59'1	1'0 (from almanac)
	57 ^m 28 ^s	$\frac{14^{\circ}- 22':0}{351^{\circ}- 45:3} +$			
	v or d correction..	- 0'6		$\frac{- 1'0}{- 1'0}$	(incr. and corr.)
	GHA	351°- 44'7		Dec. S 15°- 58'1	
	Longitude	E 91°- 12'0 \oplus		=====	
		442°- 56'7	increments and corrections		
	LHA	$\frac{360^{\circ}}{82^{\circ}- 56'7} \ominus$			
		=====			

Ans. LHA 82°- 56'7, Declination S 15°- 58'1

Example 3

What were the LHA and the declination of Jupiter on 22 Jan. 1983 at GMT 11^h 48^m 51^s at longitude W. 120°- 45'?

Solution

GMT 22 Jan, 83	GAH	v	Dec	d
11 ^h	42°- 56.4	2.0	S. 20°- 19.5	0.1 (from almanac)
48 ^m - 51 ^s	12°- 12.8 ⊕ 54°- 69.2 55°- 09.2			
v or d - correction	1.6 ⊕		0.1 ⊕	(incr. and corr.)
	55°- 10.8			
GHA	(415°- 10.8)		Dec. S. 20°- 19.6	
Longitude W	120°- 45.0 ⊖			
L H A	294°- 25.8			

Ans. LHA 294°- 25.8, Declination S. 20°- 19.6

Example 4

What were the GHA and the declination of Aldebaran on 22 Jan. 1983 at GMT 15^h 55^m 13^s?

Solution

GMT 22 Jan. 83	GHA	Declination
	291°- 15'9	N. 16°- 28'5 from almanac
GHA - Aries (15 ^h)	346°- 23'6	from almanac
55 ^m 13 ^s	13°- 50'5 ⊕	from INCREMENTS and CORRECTIONS
GHA	$\begin{array}{r} 651^\circ - 30'0 \\ \underline{360^\circ} \ominus \\ 291^\circ - 30'0 \\ \hline \hline \hline \end{array}$	

Ans. GHA 291°- 30'0, Declination N 16°- 28'5

Example 5

What were the GHA and the declination of Vega on 22 Jan. 1983 at GMT 18^h- 02^m- 45^s?

Solution

GMT 22 Jan. 83	GHA	Declination
	80°- 55!1	N. 38°- 45!9 from almanac
GHA Aries 18 ^h	31°- 31!0	
02 ^m - 45 ^s	0°- 41!4 ⊕	from INCREMENTS and CORRECTIONS
	111°- 127!5	
	120!0 ⊖	
GHA	113°- 007!5	
	=====	

Ans. GHA 113°- 007!5, Declination N 38°- 45!9

Refer to page 260.

Sight Reduction Table

2^m

INCREMENTS AND CORRECTIONS

3^m

2 ^m			INCREMENTS AND CORRECTIONS						3 ^m									
°	SUN PLANETS		ARIES	MOON	v or d		v or d		v or d		ARIES	MOON	v or d		v or d		v or d	
	+	-			+	-	+	-	+	-			+	-	+	-	+	-
00	0 30 0	0 30 1	0 29 6	0 0 0	0 0	6 0	0 1	12 0	0 5	00	0 45 0	0 45 1	0 43 0	0 0	6 0	0 4	12 0	0 7
01	0 30 3	0 30 3	0 28 7	0 0 0	0 1	6 1	0 3	12 1	0 5	01	0 45 3	0 45 4	0 43 2	0 1	6 1	0 4	12 1	0 7
02	0 30 5	0 30 6	0 29 1	0 0 0	0 2	6 2	0 3	12 2	0 5	02	0 45 5	0 45 6	0 43 4	0 2	6 2	0 4	12 2	0 7
03	0 30 6	0 30 8	0 29 3	0 0 0	0 3	6 3	0 3	12 3	0 5	03	0 45 8	0 45 9	0 43 7	0 3	6 3	0 4	12 3	0 7
04	0 31 0	0 31 1	0 29 6	0 0 0	0 4	6 4	0 3	12 4	0 5	04	0 46 0	0 46 1	0 43 9	0 4	6 4	0 4	12 4	0 7
05	0 31 3	0 31 3	0 29 8	0 0 0	0 5	6 5	0 3	12 5	0 5	05	0 46 3	0 46 4	0 44 1	0 5	6 5	0 4	12 5	0 7
06	0 31 5	0 31 6	0 30 1	0 0 0	0 6	6 6	0 3	12 6	0 5	06	0 46 5	0 46 6	0 44 1	0 6	6 6	0 4	12 6	0 7
07	0 31 6	0 31 8	0 30 3	0 0 0	0 7	6 7	0 3	12 7	0 5	07	0 46 8	0 46 9	0 44 6	0 7	6 7	0 4	12 7	0 7
08	0 32 0	0 32 1	0 30 5	0 0 0	0 8	6 8	0 3	12 8	0 5	08	0 47 0	0 47 1	0 44 9	0 8	6 8	0 4	12 8	0 7
09	0 32 3	0 32 3	0 30 8	0 0 0	0 9	6 9	0 3	12 9	0 5	09	0 47 3	0 47 4	0 45 1	0 9	6 9	0 4	12 9	0 8
10	0 32 5	0 32 6	0 31 0	0 0 0	1 0	7 0	0 3	13 0	0 5	10	0 47 5	0 47 6	0 45 3	1 0	7 0	0 4	13 0	0 8
11	0 32 8	0 32 8	0 31 3	0 0 0	1 1	7 1	0 3	13 1	0 5	11	0 47 8	0 47 9	0 45 6	1 1	7 1	0 4	13 1	0 8
12	0 33 0	0 33 1	0 31 5	0 0 0	1 2	7 2	0 3	13 2	0 6	12	0 48 0	0 48 1	0 45 8	1 2	7 2	0 4	13 2	0 8
13	0 33 3	0 33 3	0 31 7	0 0 0	1 3	7 3	0 3	13 3	0 6	13	0 48 3	0 48 4	0 46 1	1 3	7 3	0 4	13 3	0 8
14	0 33 5	0 33 6	0 32 0	0 0 0	1 4	7 4	0 3	13 4	0 6	14	0 48 5	0 48 6	0 46 3	1 4	7 4	0 4	13 4	0 8
15	0 33 8	0 33 8	0 32 2	0 0 0	1 5	7 5	0 3	13 5	0 6	15	0 48 8	0 48 9	0 46 5	1 5	7 5	0 4	13 5	0 8
16	0 34 0	0 34 1	0 32 5	0 0 0	1 6	7 6	0 3	13 6	0 6	16	0 49 0	0 49 1	0 46 8	1 6	7 6	0 4	13 6	0 8
17	0 34 3	0 34 3	0 32 7	0 0 0	1 7	7 7	0 3	13 7	0 6	17	0 49 3	0 49 4	0 47 0	1 7	7 7	0 4	13 7	0 8
18	0 34 5	0 34 6	0 32 9	0 0 0	1 8	7 8	0 3	13 8	0 6	18	0 49 5	0 49 6	0 47 2	1 8	7 8	0 5	13 8	0 8
19	0 34 8	0 34 8	0 33 2	0 0 0	1 9	7 9	0 3	13 9	0 6	19	0 49 8	0 49 9	0 47 5	1 9	7 9	0 5	13 9	0 8
20	0 35 0	0 35 1	0 33 4	0 0 0	2 0	8 0	0 3	14 0	0 6	20	0 50 0	0 50 1	0 47 7	2 0	8 0	0 5	14 0	0 8
21	0 35 3	0 35 3	0 33 6	0 0 0	2 1	8 1	0 3	14 1	0 6	21	0 50 3	0 50 4	0 48 0	2 1	8 1	0 5	14 1	0 8
22	0 35 5	0 35 6	0 33 9	0 0 0	2 2	8 2	0 3	14 2	0 6	22	0 50 5	0 50 6	0 48 2	2 2	8 2	0 5	14 2	0 8
23	0 35 8	0 35 8	0 34 1	0 0 0	2 3	8 3	0 3	14 3	0 6	23	0 50 8	0 50 9	0 48 4	2 3	8 3	0 5	14 3	0 8
24	0 36 0	0 36 1	0 34 4	0 0 0	2 4	8 4	0 4	14 4	0 6	24	0 51 0	0 51 1	0 48 7	2 4	8 4	0 5	14 4	0 8
25	0 36 3	0 36 3	0 34 6	0 0 0	2 5	8 5	0 4	14 5	0 6	25	0 51 3	0 51 4	0 48 9	2 5	8 5	0 5	14 5	0 8
26	0 36 5	0 36 6	0 34 8	0 0 0	2 6	8 6	0 4	14 6	0 6	26	0 51 5	0 51 6	0 49 2	2 6	8 6	0 5	14 6	0 9
27	0 36 8	0 36 9	0 35 1	0 0 0	2 7	8 7	0 4	14 7	0 6	27	0 51 8	0 51 9	0 49 4	2 7	8 7	0 5	14 7	0 9
28	0 37 0	0 37 1	0 35 3	0 0 0	2 8	8 8	0 4	14 8	0 6	28	0 52 0	0 52 1	0 49 6	2 8	8 8	0 5	14 8	0 9
29	0 37 3	0 37 4	0 35 6	0 0 0	2 9	8 9	0 4	14 9	0 6	29	0 52 3	0 52 4	0 49 9	2 9	8 9	0 5	14 9	0 9
30	0 37 5	0 37 6	0 35 8	0 0 0	3 0	9 0	0 4	15 0	0 6	30	0 52 5	0 52 6	0 50 1	3 0	9 0	0 5	15 0	0 9
31	0 37 8	0 37 9	0 36 0	0 0 0	3 1	9 1	0 4	15 1	0 6	31	0 52 8	0 52 9	0 50 3	3 1	9 1	0 5	15 1	0 9
32	0 38 0	0 38 1	0 36 3	0 0 0	3 2	9 2	0 4	15 2	0 6	32	0 53 0	0 53 1	0 50 6	3 2	9 2	0 5	15 2	0 9
33	0 38 3	0 38 4	0 36 5	0 0 0	3 3	9 3	0 4	15 3	0 6	33	0 53 3	0 53 4	0 50 8	3 3	9 3	0 5	15 3	0 9
34	0 38 5	0 38 6	0 36 7	0 0 0	3 4	9 4	0 4	15 4	0 6	34	0 53 5	0 53 6	0 51 1	3 4	9 4	0 5	15 4	0 9
35	0 38 8	0 38 9	0 37 0	0 0 0	3 5	9 5	0 4	15 5	0 6	35	0 53 8	0 53 9	0 51 3	3 5	9 5	0 6	15 5	0 9
36	0 39 0	0 39 1	0 37 2	0 0 0	3 6	9 6	0 4	15 6	0 7	36	0 54 0	0 54 1	0 51 5	3 6	9 6	0 6	15 6	0 9
37	0 39 3	0 39 4	0 37 5	0 0 0	3 7	9 7	0 4	15 7	0 7	37	0 54 3	0 54 4	0 51 8	3 7	9 7	0 6	15 7	0 9
38	0 39 5	0 39 6	0 37 7	0 0 0	3 8	9 8	0 4	15 8	0 7	38	0 54 5	0 54 6	0 52 0	3 8	9 8	0 6	15 8	0 9
39	0 39 8	0 39 9	0 37 9	0 0 0	3 9	9 9	0 4	15 9	0 7	39	0 54 8	0 54 9	0 52 3	3 9	9 9	0 6	15 9	0 9
40	0 40 0	0 40 1	0 38 2	0 0 0	4 0	10 0	0 4	16 0	0 7	40	0 55 0	0 55 2	0 52 5	4 0	10 0	0 6	16 0	0 9
41	0 40 3	0 40 4	0 38 4	0 0 0	4 1	10 1	0 4	16 1	0 7	41	0 55 3	0 55 4	0 52 7	4 1	10 1	0 6	16 1	0 9
42	0 40 5	0 40 6	0 38 7	0 0 0	4 2	10 2	0 4	16 2	0 7	42	0 55 5	0 55 7	0 53 0	4 2	10 2	0 6	16 2	0 9
43	0 40 8	0 40 9	0 38 9	0 0 0	4 3	10 3	0 4	16 3	0 7	43	0 55 8	0 55 9	0 53 2	4 3	10 3	0 6	16 3	1 0
44	0 41 0	0 41 1	0 39 1	0 0 0	4 4	10 4	0 4	16 4	0 7	44	0 56 0	0 56 2	0 53 4	4 4	10 4	0 6	16 4	1 0
45	0 41 3	0 41 4	0 39 4	0 0 0	4 5	10 5	0 4	16 5	0 7	45	0 56 3	0 56 4	0 53 7	4 5	10 5	0 6	16 5	1 0
46	0 41 5	0 41 6	0 39 6	0 0 0	4 6	10 6	0 4	16 6	0 7	46	0 56 5	0 56 7	0 53 9	4 6	10 6	0 6	16 6	1 0
47	0 41 8	0 41 9	0 39 8	0 0 0	4 7	10 7	0 4	16 7	0 7	47	0 56 8	0 56 9	0 54 2	4 7	10 7	0 6	16 7	1 0
48	0 42 0	0 42 1	0 40 1	0 0 0	4 8	10 8	0 5	16 8	0 7	48	0 57 0	0 57 2	0 54 4	4 8	10 8	0 6	16 8	1 0
49	0 42 3	0 42 4	0 40 3	0 0 0	4 9	10 9	0 5	16 9	0 7	49	0 57 3	0 57 4	0 54 6	4 9	10 9	0 6	16 9	1 0
50	0 42 5	0 42 6	0 40 6	0 0 0	5 0	11 0	0 5	17 0	0 7	50	0 57 5	0 57 7	0 54 9	5 0	11 0	0 6	17 0	1 0
51	0 42 8	0 42 9	0 40 8	0 0 0	5 1	11 1	0 5	17 1	0 7	51	0 57 8	0 57 9	0 55 1	5 1	11 1	0 6	17 1	1 0
52	0 43 0	0 43 1	0 41 0	0 0 0	5 2	11 2	0 5	17 2	0 7	52	0 58 0	0 58 2	0 55 4	5 2	11 2	0 7	17 2	1 0
53	0 43 3	0 43 4	0 41 3	0 0 0	5 3	11 3	0 5	17 3	0 7	53	0 58 3	0 58 4	0 55 6	5 3	11 3	0 7	17 3	1 0
54	0 43 5	0 43 6	0 41 5	0 0 0	5 4	11 4	0 5	17 4	0 7	54	0 58 5	0 58 7	0 55 8	5 4	11 4	0 7	17 4	1 0
55	0 43 8	0 43 9	0 41 8	0 0 0	5 5	11 5	0 5	17 5	0 7	55	0 58 8	0 58 9	0 56 1	5 5	11 5	0 7	17 5	1 0
56	0 44 0	0 44 1	0 42 0	0 0 0	5 6	11 6	0 5	17 6	0 7	56	0 59 0	0 59 2	0 56 3	5 6	11 6	0 7	17 6	1 0
57	0 44 3	0 44 4	0 42 2	0 0 0	5 7	11 7	0 5	17 7	0 7	57	0 59 3	0 59 4	0 56 6	5 7	11 7	0 7	17 7	1 0
58	0 44 5	0 44 6	0 42 5	0 0 0	5 8	11 8	0 5	17 8	0 7	58	0 59 5	0 59 7	0 56 8	5 8	11 8	0 7	17 8	1 0
59	0 44 8	0 44 9	0 42 7	0 0 0	5 9	11 9	0 5	17 9	0 7	59	0 59 8	0 59 9	0 57 0	5 9	11 9	0 7	17 9	1 0
60	0 45 0	0 45 1	0 43 0	0 0 0	6 0	12 0	0 5	18 0	0 8	60	1 00 0	1 00 2	0 57 3	6 0	12 0	0 7	18 0	1 1

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Sight Reduction Table
INCREMENTS AND CORRECTIONS

46^m

47^m

Table with 3 main sections: 46m, 47m, and 48m. Each section contains columns for Sun Planets, Aries, Moon, and various correction values (v or Corr, d). The 47m section has a circled 13 in the first column of its main data area.

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Sight Reduction Table

56^m

INCREMENTS AND CORRECTIONS

57^m

56	SUN PLANETS	ARIES	MOON	V or Corr ^a			57	SUN PLANETS	ARIES	MOON	V or Corr ^a				
				d	+	-					d	+	-		
00	14 00-0	14 02-3	13 21-7	0-0	0-0	6-0	5-7	12-0	11-3	0-0	0-0	6-0	5-8	12-0	11-5
01	14 00-3	14 02-6	13 22-0	0-1	0-1	6-1	5-7	12-1	11-4	0-1	0-1	6-1	5-8	12-1	11-6
02	14 00-5	14 02-8	13 22-2	0-2	0-2	6-2	5-8	12-2	11-5	0-2	0-2	6-2	5-9	12-2	11-7
03	14 00-8	14 03-1	13 22-4	0-3	0-3	6-3	5-9	12-3	11-6	0-3	0-3	6-3	6-0	12-3	11-8
04	14 01-0	14 03-3	13 22-7	0-4	0-4	6-4	6-0	12-4	11-7	0-4	0-4	6-4	6-1	12-4	11-9
05	14 01-3	14 03-6	13 22-9	0-5	0-5	6-5	6-1	12-5	11-8	0-5	0-5	6-5	6-2	12-5	12-0
06	14 01-5	14 03-8	13 23-2	0-6	0-6	6-6	6-2	12-6	11-9	0-6	0-6	6-6	6-3	12-6	12-1
07	14 01-8	14 04-1	13 23-4	0-7	0-7	6-7	6-3	12-7	12-0	0-7	0-7	6-7	6-4	12-7	12-2
08	14 02-0	14 04-3	13 23-6	0-8	0-8	6-8	6-4	12-8	12-1	0-8	0-8	6-8	6-5	12-8	12-3
09	14 02-3	14 04-6	13 23-9	0-9	0-8	6-9	6-5	12-9	12-1	0-9	0-9	6-9	6-6	12-9	12-4
10	14 02-5	14 04-8	13 24-1	1-0	0-9	7-0	6-6	12-0	12-2	1-0	1-0	7-0	6-7	12-0	12-5
11	14 02-8	14 05-1	13 24-4	1-1	1-0	7-1	6-7	12-1	12-3	1-1	1-1	7-1	6-8	12-1	12-6
12	14 03-0	14 05-3	13 24-6	1-2	1-1	7-2	6-8	12-2	12-4	1-2	1-2	7-2	6-9	12-2	12-7
13	14 03-3	14 05-6	13 24-8	1-3	1-2	7-3	6-9	12-3	12-5	1-3	1-2	7-3	7-0	12-3	12-7
14	14 03-5	14 05-8	13 25-1	1-4	1-3	7-4	7-0	12-4	12-6	1-4	1-3	7-4	7-1	12-4	12-8
15	14 03-8	14 06-1	13 25-3	1-5	1-4	7-5	7-1	12-5	12-7	1-5	1-4	7-5	7-2	12-5	12-9
16	14 04-0	14 06-3	13 25-6	1-6	1-5	7-6	7-2	12-6	12-8	1-6	1-5	7-6	7-3	12-6	13-0
17	14 04-3	14 06-6	13 25-8	1-7	1-6	7-7	7-3	12-7	12-9	1-7	1-6	7-7	7-4	12-7	13-1
18	14 04-5	14 06-8	13 26-0	1-8	1-7	7-8	7-3	12-8	13-0	1-8	1-7	7-8	7-5	12-8	13-2
19	14 04-8	14 07-1	13 26-3	1-9	1-8	7-9	7-4	12-9	13-1	1-9	1-8	7-9	7-6	12-9	13-3
20	14 05-0	14 07-3	13 26-5	2-0	1-9	8-0	7-5	12-0	13-2	2-0	1-9	8-0	7-7	12-0	13-4
21	14 05-3	14 07-6	13 26-7	2-1	2-0	8-1	7-6	12-1	13-3	2-1	2-0	8-1	7-8	12-1	13-5
22	14 05-5	14 07-8	13 27-0	2-2	2-1	8-2	7-7	12-2	13-4	2-2	2-1	8-2	7-9	12-2	13-6
23	14 05-8	14 08-1	13 27-2	2-3	2-2	8-3	7-8	12-3	13-5	2-3	2-2	8-3	8-0	12-3	13-7
24	14 06-0	14 08-3	13 27-5	2-4	2-3	8-4	7-9	12-4	13-6	2-4	2-3	8-4	8-1	12-4	13-8
25	14 06-3	14 08-6	13 27-7	2-5	2-4	8-5	8-0	12-5	13-7	2-5	2-4	8-5	8-2	12-5	13-9
26	14 06-5	14 08-8	13 27-9	2-6	2-4	8-6	8-1	12-6	13-7	2-6	2-5	8-6	8-1	12-6	14-0
27	14 06-8	14 09-1	13 28-2	2-7	2-5	8-7	8-2	12-7	13-8	2-7	2-6	8-7	8-3	12-7	14-1
28	14 07-0	14 09-3	13 28-4	2-8	2-6	8-8	8-3	12-8	13-9	2-8	2-7	8-8	8-4	12-8	14-2
29	14 07-3	14 09-6	13 28-7	2-9	2-7	8-9	8-4	12-9	14-0	2-9	2-8	8-9	8-5	12-9	14-3
30	14 07-5	14 09-8	13 28-9	3-0	2-8	9-0	8-5	12-0	14-1	3-0	2-9	9-0	8-6	12-0	14-4
31	14 07-8	14 10-1	13 29-1	3-1	2-9	9-1	8-6	12-1	14-2	3-1	3-0	9-1	8-7	12-1	14-5
32	14 08-0	14 10-3	13 29-4	3-2	3-0	9-2	8-7	12-2	14-3	3-2	3-1	9-2	8-8	12-2	14-6
33	14 08-3	14 10-6	13 29-6	3-3	3-1	9-3	8-8	12-3	14-4	3-3	3-2	9-3	8-9	12-3	14-7
34	14 08-5	14 10-8	13 29-8	3-4	3-2	9-4	8-9	12-4	14-5	3-4	3-3	9-4	9-0	12-4	14-8
35	14 08-8	14 11-1	13 30-1	3-5	3-3	9-5	8-9	12-5	14-6	3-5	3-4	9-5	9-1	12-5	14-9
36	14 09-0	14 11-3	13 30-3	3-6	3-4	9-6	9-0	12-6	14-7	3-6	3-5	9-6	9-2	12-6	15-0
37	14 09-3	14 11-6	13 30-6	3-7	3-5	9-7	9-1	12-7	14-8	3-7	3-5	9-7	9-3	12-7	15-0
38	14 09-5	14 11-8	13 30-8	3-8	3-6	9-8	9-2	12-8	14-9	3-8	3-6	9-8	9-4	12-8	15-1
39	14 09-8	14 12-1	13 31-0	3-9	3-7	9-9	9-3	12-9	15-0	3-9	3-7	9-9	9-5	12-9	15-2
40	14 10-0	14 12-3	13 31-3	4-0	3-8	10-0	9-4	12-0	15-1	4-0	3-8	10-0	9-6	12-0	15-3
41	14 10-3	14 12-6	13 31-5	4-1	3-9	10-1	9-5	12-1	15-2	4-1	3-9	10-1	9-7	12-1	15-4
42	14 10-5	14 12-8	13 31-8	4-2	4-0	10-2	9-6	12-2	15-3	4-2	4-0	10-2	9-8	12-2	15-5
43	14 10-8	14 13-1	13 32-0	4-3	4-0	10-3	9-7	12-3	15-3	4-3	4-1	10-3	9-9	12-3	15-6
44	14 11-0	14 13-3	13 32-2	4-4	4-1	10-4	9-8	12-4	15-4	4-4	4-2	10-4	10-0	12-4	15-7
45	14 11-3	14 13-6	13 32-5	4-5	4-2	10-5	9-9	12-5	15-5	4-5	4-3	10-5	10-1	12-5	15-8
46	14 11-5	14 13-8	13 32-7	4-6	4-3	10-6	10-0	12-6	15-6	4-6	4-4	10-6	10-2	12-6	15-9
47	14 11-8	14 14-1	13 32-9	4-7	4-4	10-7	10-1	12-7	15-7	4-7	4-5	10-7	10-3	12-7	16-0
48	14 12-0	14 14-3	13 33-2	4-8	4-5	10-8	10-2	12-8	15-8	4-8	4-6	10-8	10-4	12-8	16-1
49	14 12-3	14 14-6	13 33-4	4-9	4-6	10-9	10-3	12-9	15-9	4-9	4-7	10-9	10-4	12-9	16-2
50	14 12-5	14 14-8	13 33-7	5-0	4-7	11-0	10-4	12-0	16-0	5-0	4-8	11-0	10-5	12-0	16-3
51	14 12-8	14 15-1	13 33-9	5-1	4-8	11-1	10-5	12-1	16-1	5-1	4-9	11-1	10-6	12-1	16-4
52	14 13-0	14 15-3	13 34-1	5-2	4-9	11-2	10-5	12-2	16-2	5-2	5-0	11-2	10-7	12-2	16-5
53	14 13-3	14 15-6	13 34-4	5-3	5-0	11-3	10-6	12-3	16-3	5-3	5-1	11-3	10-8	12-3	16-6
54	14 13-5	14 15-8	13 34-6	5-4	5-1	11-4	10-7	12-4	16-4	5-4	5-2	11-4	10-9	12-4	16-7
55	14 13-8	14 16-1	13 34-9	5-5	5-2	11-5	10-8	12-5	16-5	5-5	5-3	11-5	11-0	12-5	16-8
56	14 14-0	14 16-3	13 35-1	5-6	5-3	11-6	10-9	12-6	16-6	5-6	5-4	11-6	11-1	12-6	16-9
57	14 14-3	14 16-6	13 35-3	5-7	5-4	11-7	11-0	12-7	16-7	5-7	5-5	11-7	11-2	12-7	17-0
58	14 14-5	14 16-8	13 35-6	5-8	5-5	11-8	11-1	12-8	16-8	5-8	5-6	11-8	11-3	12-8	17-1
59	14 14-8	14 17-1	13 35-8	5-9	5-6	11-9	11-2	12-9	16-9	5-9	5-7	11-9	11-4	12-9	17-2
60	14 15-0	14 17-3	13 36-1	6-0	5-7	12-0	11-3	12-0	17-0	6-0	5-8	12-0	11-5	12-0	17-3

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Problem 1

What were the GHA and the declination of the sun on 22 Jan. 1978 at GMT $15^h - 47^m - 13^s$?

Problem 2

What were the GHA and the declination of the moon on 22 Jan. 1978 at GMT $15^h - 47^m - 13^s$?

Problem 3

What were the LHA and the declination of Venus on 6 Apr. 1978 at GMT $10^h - 57^m - 28^s$ at longitude E. $113^\circ - 55'$?

Problem 4

What were the LHA and the declination of Mars on 6 Apr. 1978 at GMT $23^h - 25^m - 12^s$ at longitude W. $71^\circ - 12'$?

Problem 5

What were the GHA and the declination of Aldebaran on 22 Jan. 1978 at GMT $15^h - 55^m - 13^s$?

Problem 6

What were the GHA and the declination of Vega on 22 Jan. 1978 at GMT $16^h - 02^m - 45^s$?

Sight Reduction Table

2^m

INCREMENTS AND CORRECTIONS

3^m

2		SUN PLANETS	ARIES	MOON	u or d		Corr ⁿ		3		SUN PLANETS	ARIES	MOON	u or d		Corr ⁿ		u or d		Corr ⁿ		
00	0 30-0	0 30-1	0 28-6	0-0	0-0	6-0	0-3	12-0	0-5	00	0 45-0	0 45-1	0 43-0	0-0	0-0	6-0	0-4	12-0	0-7			
01	0 30-3	0 30-3	0 28-9	0-1	0-0	6-1	0-3	12-1	0-5	01	0 45-3	0 45-4	0 43-2	0-1	0-0	6-1	0-4	12-1	0-7			
02	0 30-5	0 30-6	0 29-1	0-2	0-0	6-2	0-3	12-2	0-5	02	0 45-5	0 45-6	0 43-4	0-2	0-0	6-2	0-4	12-2	0-7			
03	0 30-8	0 30-8	0 29-3	0-3	0-0	6-3	0-3	12-3	0-5	03	0 45-8	0 45-9	0 43-7	0-3	0-0	6-3	0-4	12-3	0-7			
04	0 31-0	0 31-1	0 29-6	0-4	0-0	6-4	0-3	12-4	0-5	04	0 46-0	0 46-1	0 43-9	0-4	0-0	6-4	0-4	12-4	0-7			
05	0 31-3	0 31-3	0 29-8	0-5	0-0	6-5	0-3	12-5	0-5	05	0 46-3	0 46-4	0 44-1	0-5	0-0	6-5	0-4	12-5	0-7			
06	0 31-5	0 31-6	0 30-1	0-6	0-0	6-6	0-3	12-6	0-5	06	0 46-5	0 46-6	0 44-4	0-6	0-0	6-6	0-4	12-6	0-7			
07	0 31-8	0 31-8	0 30-3	0-7	0-0	6-7	0-3	12-7	0-5	07	0 46-8	0 46-9	0 44-6	0-7	0-0	6-7	0-4	12-7	0-7			
08	0 32-0	0 32-1	0 30-5	0-8	0-0	6-8	0-3	12-8	0-5	08	0 47-0	0 47-1	0 44-9	0-8	0-0	6-8	0-4	12-8	0-7			
09	0 32-3	0 32-3	0 30-8	0-9	0-0	6-9	0-3	12-9	0-5	09	0 47-3	0 47-4	0 45-1	0-9	0-1	6-9	0-4	12-9	0-8			
10	0 32-5	0 32-6	0 31-0	1-0	0-0	7-0	0-3	13-0	0-5	10	0 47-5	0 47-6	0 45-3	1-0	0-1	7-0	0-4	13-0	0-8			
11	0 32-8	0 32-8	0 31-3	1-1	0-0	7-1	0-3	13-1	0-5	11	0 47-8	0 47-9	0 45-6	1-1	0-1	7-1	0-4	13-1	0-8			
12	0 33-0	0 33-1	0 31-5	1-2	0-1	7-2	0-3	13-2	0-6	12	0 48-0	0 48-1	0 45-8	1-2	0-1	7-2	0-4	13-2	0-8			
13	0 33-3	0 33-3	0 31-7	1-3	0-1	7-3	0-3	13-3	0-6	13	0 48-3	0 48-4	0 46-1	1-3	0-1	7-3	0-4	13-3	0-8			
14	0 33-5	0 33-6	0 32-0	1-4	0-1	7-4	0-3	13-4	0-6	14	0 48-5	0 48-6	0 46-3	1-4	0-1	7-4	0-4	13-4	0-8			
15	0 33-8	0 33-8	0 32-2	1-5	0-1	7-5	0-3	13-5	0-6	15	0 48-8	0 48-9	0 46-5	1-5	0-1	7-5	0-4	13-5	0-8			
16	0 34-0	0 34-1	0 32-5	1-6	0-1	7-6	0-3	13-6	0-6	16	0 49-0	0 49-1	0 46-8	1-6	0-1	7-6	0-4	13-6	0-8			
17	0 34-3	0 34-3	0 32-7	1-7	0-1	7-7	0-3	13-7	0-6	17	0 49-3	0 49-4	0 47-0	1-7	0-1	7-7	0-4	13-7	0-8			
18	0 34-5	0 34-6	0 32-9	1-8	0-1	7-8	0-3	13-8	0-6	18	0 49-5	0 49-6	0 47-2	1-8	0-1	7-8	0-5	13-8	0-8			
19	0 34-8	0 34-8	0 33-2	1-9	0-1	7-9	0-3	13-9	0-6	19	0 49-8	0 49-9	0 47-5	1-9	0-1	7-9	0-5	13-9	0-8			
20	0 35-0	0 35-1	0 33-4	2-0	0-1	8-0	0-3	14-0	0-6	20	0 50-0	0 50-1	0 47-7	2-0	0-1	8-0	0-5	14-0	0-8			
21	0 35-3	0 35-3	0 33-6	2-1	0-1	8-1	0-3	14-1	0-6	21	0 50-3	0 50-4	0 48-0	2-1	0-1	8-1	0-5	14-1	0-8			
22	0 35-5	0 35-6	0 33-9	2-2	0-1	8-2	0-3	14-2	0-6	22	0 50-5	0 50-6	0 48-2	2-2	0-1	8-2	0-5	14-2	0-8			
23	0 35-8	0 35-8	0 34-1	2-3	0-1	8-3	0-3	14-3	0-6	23	0 50-8	0 50-9	0 48-4	2-3	0-1	8-3	0-5	14-3	0-8			
24	0 36-0	0 36-1	0 34-4	2-4	0-1	8-4	0-4	14-4	0-6	24	0 51-0	0 51-1	0 48-7	2-4	0-1	8-4	0-5	14-4	0-8			
25	0 36-3	0 36-3	0 34-6	2-5	0-1	8-5	0-4	14-5	0-6	25	0 51-3	0 51-4	0 48-9	2-5	0-1	8-5	0-5	14-5	0-8			
26	0 36-5	0 36-6	0 34-8	2-6	0-1	8-6	0-4	14-6	0-6	26	0 51-5	0 51-6	0 49-2	2-6	0-2	8-6	0-5	14-6	0-9			
27	0 36-8	0 36-9	0 35-1	2-7	0-1	8-7	0-4	14-7	0-6	27	0 51-8	0 51-9	0 49-4	2-7	0-2	8-7	0-5	14-7	0-9			
28	0 37-0	0 37-1	0 35-3	2-8	0-1	8-8	0-4	14-8	0-6	28	0 52-0	0 52-1	0 49-6	2-8	0-2	8-8	0-5	14-8	0-9			
29	0 37-3	0 37-4	0 35-6	2-9	0-1	8-9	0-4	14-9	0-6	29	0 52-3	0 52-4	0 49-9	2-9	0-2	8-9	0-5	14-9	0-9			
30	0 37-5	0 37-6	0 35-8	3-0	0-1	9-0	0-4	15-0	0-6	30	0 52-5	0 52-6	0 50-1	3-0	0-2	9-0	0-5	15-0	0-9			
31	0 37-8	0 37-9	0 36-0	3-1	0-1	9-1	0-4	15-1	0-6	31	0 52-8	0 52-9	0 50-3	3-1	0-2	9-1	0-5	15-1	0-9			
32	0 38-0	0 38-1	0 36-3	3-2	0-1	9-2	0-4	15-2	0-6	32	0 53-0	0 53-1	0 50-6	3-2	0-2	9-2	0-5	15-2	0-9			
33	0 38-3	0 38-4	0 36-5	3-3	0-1	9-3	0-4	15-3	0-6	33	0 53-3	0 53-4	0 50-8	3-3	0-2	9-3	0-5	15-3	0-9			
34	0 38-5	0 38-6	0 36-7	3-4	0-1	9-4	0-4	15-4	0-6	34	0 53-5	0 53-6	0 51-1	3-4	0-2	9-4	0-5	15-4	0-9			
35	0 38-8	0 38-9	0 37-0	3-5	0-1	9-5	0-4	15-5	0-6	35	0 53-8	0 53-9	0 51-3	3-5	0-2	9-5	0-6	15-5	0-9			
36	0 39-0	0 39-1	0 37-2	3-6	0-2	9-6	0-4	15-6	0-7	36	0 54-0	0 54-1	0 51-5	3-6	0-2	9-6	0-6	15-6	0-9			
37	0 39-3	0 39-4	0 37-5	3-7	0-2	9-7	0-4	15-7	0-7	37	0 54-3	0 54-4	0 51-8	3-7	0-2	9-7	0-6	15-7	0-9			
38	0 39-5	0 39-6	0 37-7	3-8	0-2	9-8	0-4	15-8	0-7	38	0 54-5	0 54-6	0 52-0	3-8	0-2	9-8	0-6	15-8	0-9			
39	0 39-8	0 39-9	0 37-9	3-9	0-2	9-9	0-4	15-9	0-7	39	0 54-8	0 54-9	0 52-3	3-9	0-2	9-9	0-6	15-9	0-9			
40	0 40-0	0 40-1	0 38-2	4-0	0-2	10-0	0-4	16-0	0-7	40	0 55-0	0 55-2	0 52-5	4-0	0-2	10-0	0-6	16-0	0-9			
41	0 40-3	0 40-4	0 38-4	4-1	0-2	10-1	0-4	16-1	0-7	41	0 55-3	0 55-4	0 52-7	4-1	0-2	10-1	0-6	16-1	0-9			
42	0 40-5	0 40-6	0 38-7	4-2	0-2	10-2	0-4	16-2	0-7	42	0 55-5	0 55-7	0 53-0	4-2	0-2	10-2	0-6	16-2	0-9			
43	0 40-8	0 40-9	0 38-9	4-3	0-2	10-3	0-4	16-3	0-7	43	0 55-8	0 55-9	0 53-2	4-3	0-3	10-3	0-6	16-3	1-0			
44	0 41-0	0 41-1	0 39-1	4-4	0-2	10-4	0-4	16-4	0-7	44	0 56-0	0 56-2	0 53-4	4-4	0-3	10-4	0-6	16-4	1-0			
45	0 41-3	0 41-4	0 39-4	4-5	0-2	10-5	0-4	16-5	0-7	45	0 56-3	0 56-4	0 53-7	4-5	0-3	10-5	0-6	16-5	1-0			
46	0 41-5	0 41-6	0 39-6	4-6	0-2	10-6	0-4	16-6	0-7	46	0 56-5	0 56-7	0 53-9	4-6	0-3	10-6	0-6	16-6	1-0			
47	0 41-8	0 41-9	0 39-8	4-7	0-2	10-7	0-4	16-7	0-7	47	0 56-8	0 56-9	0 54-2	4-7	0-3	10-7	0-6	16-7	1-0			
48	0 42-0	0 42-1	0 40-1	4-8	0-2	10-8	0-5	16-8	0-7	48	0 57-0	0 57-2	0 54-4	4-8	0-3	10-8	0-6	16-8	1-0			
49	0 42-3	0 42-4	0 40-3	4-9	0-2	10-9	0-5	16-9	0-7	49	0 57-3	0 57-4	0 54-6	4-9	0-3	10-9	0-6	16-9	1-0			
50	0 42-5	0 42-6	0 40-6	5-0	0-2	11-0	0-5	17-0	0-7	50	0 57-5	0 57-7	0 54-9	5-0	0-3	11-0	0-6	17-0	1-0			
51	0 42-8	0 42-9	0 40-8	5-1	0-2	11-1	0-5	17-1	0-7	51	0 57-8	0 57-9	0 55-1	5-1	0-3	11-1	0-6	17-1	1-0			
52	0 43-0	0 43-1	0 41-0	5-2	0-2	11-2	0-5	17-2	0-7	52	0 58-0	0 58-2	0 55-4	5-2	0-3	11-2	0-7	17-2	1-0			
53	0 43-3	0 43-4	0 41-3	5-3	0-2	11-3	0-5	17-3	0-7	53	0 58-3	0 58-4	0 55-6	5-3	0-3	11-3	0-7	17-3	1-0			
54	0 43-5	0 43-6	0 41-5	5-4	0-2	11-4	0-5	17-4	0-7	54	0 58-5	0 58-7	0 55-8	5-4	0-3	11-4	0-7	17-4	1-0			
55	0 43-8	0 43-9	0 41-8	5-5	0-2	11-5	0-5	17-5	0-7	55	0 58-8	0 58-9	0 56-1	5-5	0-3	11-5	0-7	17-5	1-0			
56	0 44-0	0 44-1	0 42-0	5-6	0-2	11-6	0-5	17-6	0-7	56	0 59-0	0 59-2	0 56-3	5-6	0-3	11-6	0-7	17-6	1-0			
57	0 44-3	0 44-4	0 42-2	5-7	0-2	11-7	0-5	17-7	0-7	57	0 59-3	0 59-4	0 56-6	5-7	0-3	11-7	0-7	17-7	1-0			
58	0 44-5	0 44-6	0 42-5	5-8	0-2	11-8	0-5	17-8	0-7	58	0 59-5	0 59-7	0 56-8	5-8	0-3	11-8	0-7	17-8	1-0			
59	0 44-8	0 44-9	0 42-7	5-9	0-2	11-9	0-5	17-9	0-7	59	0 59-8	0 59-9	0 57-0	5-9	0-3	11-9	0-7	17-9	1-0			
60	0 45-0	0 45-1	0 43-0	6-0	0-3	12-0	0-5	18-0	0-													

Sight Reduction Table

24^m

INCREMENTS AND CORRECTIONS

25^m

24 ^m								25 ^m											
h	SUN PLANETS	ARIES	MOON	v of d	Corr ⁿ	v of d	Corr ⁿ	v of d	Corr ⁿ	h	SUN PLANETS	ARIES	MOON	v of d	Corr ⁿ	v of d	Corr ⁿ		
00	6 00-0	6 01-0	5 43-6	0-0	0-0	6-0	2-5	12-0	4-9	00	6 15-0	6 16-0	5 57-9	0-0	0-0	6-0	2-6	12-0	5-1
01	6 00-3	6 01-2	5 43-8	0-1	0-0	6-1	2-5	12-1	4-9	01	6 15-3	6 16-3	5 58-2	0-1	0-0	6-1	2-6	12-1	5-1
02	6 00-5	6 01-5	5 44-1	0-2	0-1	6-2	2-5	12-2	5-0	02	6 15-5	6 16-5	5 58-4	0-2	0-1	6-2	2-6	12-2	5-2
03	6 00-8	6 01-7	5 44-3	0-3	0-1	6-3	2-6	12-3	5-0	03	6 15-8	6 16-8	5 58-6	0-3	0-1	6-3	2-7	12-3	5-2
04	6 01-0	6 02-0	5 44-6	0-4	0-2	6-4	2-6	12-4	5-1	04	6 16-0	6 17-0	5 58-9	0-4	0-2	6-4	2-7	12-4	5-3
05	6 01-3	6 02-2	5 44-8	0-5	0-2	6-5	2-7	12-5	5-1	05	6 16-3	6 17-3	5 59-1	0-5	0-2	6-5	2-8	12-5	5-3
06	6 01-5	6 02-5	5 45-0	0-6	0-2	6-6	2-7	12-6	5-1	06	6 16-5	6 17-5	5 59-3	0-6	0-3	6-6	2-8	12-6	5-4
07	6 01-8	6 02-7	5 45-3	0-7	0-3	6-7	2-7	12-7	5-2	07	6 16-8	6 17-8	5 59-6	0-7	0-3	6-7	2-8	12-7	5-4
08	6 02-0	6 03-0	5 45-5	0-8	0-3	6-8	2-8	12-8	5-2	08	6 17-0	6 18-0	5 59-8	0-8	0-3	6-8	2-9	12-8	5-4
09	6 02-3	6 03-2	5 45-7	0-9	0-4	6-9	2-8	12-9	5-3	09	6 17-3	6 18-3	6 00-1	0-9	0-4	6-9	2-9	12-9	5-5
10	6 02-5	6 03-5	5 46-0	1-0	0-4	7-0	2-9	13-0	5-3	10	6 17-5	6 18-5	6 00-3	1-0	0-4	7-0	3-0	13-0	5-5
11	6 02-8	6 03-7	5 46-2	1-1	0-4	7-1	2-9	13-1	5-3	11	6 17-8	6 18-8	6 00-5	1-1	0-5	7-1	3-0	13-1	5-6
12	6 03-0	6 04-0	5 46-5	1-2	0-5	7-2	2-9	13-2	5-4	12	6 18-0	6 19-0	6 00-8	1-2	0-5	7-2	3-1	13-2	5-6
13	6 03-3	6 04-2	5 46-7	1-3	0-5	7-3	3-0	13-3	5-4	13	6 18-3	6 19-3	6 01-0	1-3	0-6	7-3	3-1	13-3	5-7
14	6 03-5	6 04-5	5 46-9	1-4	0-6	7-4	3-0	13-4	5-5	14	6 18-5	6 19-5	6 01-3	1-4	0-6	7-4	3-1	13-4	5-7
15	6 03-8	6 04-7	5 47-2	1-5	0-6	7-5	3-1	13-5	5-5	15	6 18-8	6 19-8	6 01-5	1-5	0-6	7-5	3-2	13-5	5-7
16	6 04-0	6 05-0	5 47-4	1-6	0-7	7-6	3-1	13-6	5-6	16	6 19-0	6 20-0	6 01-7	1-6	0-7	7-6	3-2	13-6	5-8
17	6 04-3	6 05-2	5 47-7	1-7	0-7	7-7	3-1	13-7	5-6	17	6 19-3	6 20-3	6 02-0	1-7	0-7	7-7	3-3	13-7	5-8
18	6 04-5	6 05-5	5 47-9	1-8	0-7	7-8	3-2	13-8	5-6	18	6 19-5	6 20-5	6 02-2	1-8	0-8	7-8	3-3	13-8	5-9
19	6 04-8	6 05-7	5 48-1	1-9	0-8	7-9	3-2	13-9	5-7	19	6 19-8	6 20-8	6 02-5	1-9	0-8	7-9	3-4	13-9	5-9
20	6 05-0	6 06-0	5 48-4	2-0	0-8	8-0	3-3	14-0	5-7	20	6 20-0	6 21-0	6 02-7	2-0	0-9	8-0	3-4	14-0	6-0
21	6 05-3	6 06-3	5 48-6	2-1	0-9	8-1	3-3	14-1	5-8	21	6 20-3	6 21-3	6 02-9	2-1	0-9	8-1	3-4	14-1	6-0
22	6 05-5	6 06-5	5 48-8	2-2	0-9	8-2	3-3	14-2	5-8	22	6 20-5	6 21-5	6 03-2	2-2	0-9	8-2	3-5	14-2	6-0
23	6 05-8	6 06-8	5 49-1	2-3	0-9	8-3	3-4	14-3	5-8	23	6 20-8	6 21-8	6 03-4	2-3	1-0	8-3	3-5	14-3	6-1
24	6 06-0	6 07-0	5 49-3	2-4	1-0	8-4	3-4	14-4	5-9	24	6 21-0	6 22-0	6 03-6	2-4	1-0	8-4	3-6	14-4	6-1
25	6 06-3	6 07-3	5 49-6	2-5	1-0	8-5	3-5	14-5	5-9	25	6 21-3	6 22-3	6 03-9	2-5	1-1	8-5	3-6	14-5	6-2
26	6 06-5	6 07-5	5 49-8	2-6	1-1	8-6	3-5	14-6	6-0	26	6 21-5	6 22-5	6 04-1	2-6	1-1	8-6	3-7	14-6	6-2
27	6 06-8	6 07-8	5 50-0	2-7	1-1	8-7	3-6	14-7	6-0	27	6 21-8	6 22-8	6 04-4	2-7	1-1	8-7	3-7	14-7	6-2
28	6 07-0	6 08-0	5 50-3	2-8	1-1	8-8	3-6	14-8	6-0	28	6 22-0	6 23-0	6 04-6	2-8	1-2	8-8	3-7	14-8	6-3
29	6 07-3	6 08-3	5 50-5	2-9	1-2	8-9	3-6	14-9	6-1	29	6 22-3	6 23-3	6 04-8	2-9	1-2	8-9	3-8	14-9	6-3
30	6 07-5	6 08-5	5 50-8	3-0	1-2	9-0	3-7	15-0	6-1	30	6 22-5	6 23-5	6 05-1	3-0	1-3	9-0	3-8	15-0	6-4
31	6 07-8	6 08-8	5 51-0	3-1	1-3	9-1	3-7	15-1	6-2	31	6 22-8	6 23-8	6 05-3	3-1	1-3	9-1	3-9	15-1	6-4
32	6 08-0	6 09-0	5 51-2	3-2	1-3	9-2	3-8	15-2	6-2	32	6 23-0	6 24-0	6 05-6	3-2	1-4	9-2	3-9	15-2	6-5
33	6 08-3	6 09-3	5 51-5	3-3	1-3	9-3	3-8	15-3	6-2	33	6 23-3	6 24-3	6 05-8	3-3	1-4	9-3	4-0	15-3	6-5
34	6 08-5	6 09-5	5 51-7	3-4	1-4	9-4	3-8	15-4	6-3	34	6 23-5	6 24-5	6 06-0	3-4	1-4	9-4	4-0	15-4	6-5
35	6 08-8	6 09-8	5 52-0	3-5	1-4	9-5	3-9	15-5	6-3	35	6 23-8	6 24-8	6 06-3	3-5	1-5	9-5	4-0	15-5	6-6
36	6 09-0	6 10-0	5 52-2	3-6	1-5	9-6	3-9	15-6	6-4	36	6 24-0	6 25-0	6 06-5	3-6	1-5	9-6	4-1	15-6	6-6
37	6 09-3	6 10-3	5 52-4	3-7	1-5	9-7	4-0	15-7	6-4	37	6 24-3	6 25-3	6 06-7	3-7	1-6	9-7	4-1	15-7	6-7
38	6 09-5	6 10-5	5 52-7	3-8	1-6	9-8	4-0	15-8	6-5	38	6 24-5	6 25-5	6 07-0	3-8	1-6	9-8	4-2	15-8	6-7
39	6 09-8	6 10-8	5 52-9	3-9	1-6	9-9	4-0	15-9	6-5	39	6 24-8	6 25-8	6 07-2	3-9	1-7	9-9	4-2	15-9	6-8
40	6 10-0	6 11-0	5 53-1	4-0	1-6	10-0	4-1	16-0	6-5	40	6 25-0	6 26-0	6 07-5	4-0	1-7	10-0	4-3	16-0	6-8
41	6 10-3	6 11-3	5 53-4	4-1	1-7	10-1	4-1	16-1	6-6	41	6 25-3	6 26-3	6 07-7	4-1	1-7	10-1	4-3	16-1	6-8
42	6 10-5	6 11-5	5 53-6	4-2	1-7	10-2	4-2	16-2	6-6	42	6 25-5	6 26-5	6 07-9	4-2	1-8	10-2	4-3	16-2	6-9
43	6 10-8	6 11-8	5 53-9	4-3	1-8	10-3	4-2	16-3	6-7	43	6 25-8	6 26-8	6 08-2	4-3	1-8	10-3	4-4	16-3	6-9
44	6 11-0	6 12-0	5 54-1	4-4	1-8	10-4	4-2	16-4	6-7	44	6 26-0	6 27-0	6 08-4	4-4	1-9	10-4	4-4	16-4	7-0
45	6 11-3	6 12-3	5 54-3	4-5	1-8	10-5	4-3	16-5	6-7	45	6 26-3	6 27-3	6 08-7	4-5	1-9	10-5	4-5	16-5	7-0
46	6 11-5	6 12-5	5 54-6	4-6	1-9	10-6	4-3	16-6	6-8	46	6 26-5	6 27-5	6 08-9	4-6	2-0	10-6	4-5	16-6	7-1
47	6 11-8	6 12-8	5 54-8	4-7	1-9	10-7	4-4	16-7	6-8	47	6 26-8	6 27-8	6 09-1	4-7	2-0	10-7	4-5	16-7	7-1
48	6 12-0	6 13-0	5 55-1	4-8	2-0	10-8	4-4	16-8	6-9	48	6 27-0	6 28-0	6 09-4	4-8	2-0	10-8	4-6	16-8	7-1
49	6 12-3	6 13-3	5 55-3	4-9	2-0	10-9	4-5	16-9	6-9	49	6 27-3	6 28-3	6 09-6	4-9	2-1	10-9	4-6	16-9	7-2
50	6 12-5	6 13-5	5 55-5	5-0	2-0	11-0	4-5	17-0	6-9	50	6 27-5	6 28-5	6 09-8	5-0	2-1	11-0	4-7	17-0	7-2
51	6 12-8	6 13-8	5 55-8	5-1	2-1	11-1	4-5	17-1	7-0	51	6 27-8	6 28-8	6 10-1	5-1	2-2	11-1	4-7	17-1	7-3
52	6 13-0	6 14-0	5 56-0	5-2	2-1	11-2	4-6	17-2	7-0	52	6 28-0	6 29-0	6 10-3	5-2	2-2	11-2	4-8	17-2	7-3
53	6 13-3	6 14-3	5 56-2	5-3	2-2	11-3	4-6	17-3	7-1	53	6 28-3	6 29-3	6 10-6	5-3	2-3	11-3	4-8	17-3	7-4
54	6 13-5	6 14-5	5 56-5	5-4	2-2	11-4	4-7	17-4	7-1	54	6 28-5	6 29-5	6 10-8	5-4	2-3	11-4	4-8	17-4	7-4
55	6 13-8	6 14-8	5 56-7	5-5	2-2	11-5	4-7	17-5	7-1	55	6 28-8	6 29-8	6 11-0	5-5	2-3	11-5	4-9	17-5	7-4
56	6 14-0	6 15-0	5 57-0	5-6	2-3	11-6	4-7	17-6	7-2	56	6 29-0	6 30-0	6 11-3	5-6	2-4	11-6	4-9	17-6	7-5
57	6 14-3	6 15-3	5 57-2	5-7	2-3	11-7	4-8	17-7	7-2	57	6 29-3	6 30-3	6 11-5	5-7	2-4	11-7	5-0	17-7	7-5
58	6 14-5	6 15-5	5 57-4	5-8	2-4	11-8	4-8	17-8	7-3	58	6 29-5	6 30-5	6 11-8	5-8	2-5	11-8	5-0	17-8	7-6
59	6 14-8	6 15-8	5 57-7	5-9	2-4	11-9	4-9	17-9	7-3	59	6 29-8	6 30-8	6 12-0	5-9	2-5	11-9	5-1	17-9	7-6
60	6 15-0	6 16-0	5 57-9	6-0	2-5	12-0	4-9	18-0	7-4	60	6 30-0	6 31-0	6 12-2	6-0	2-6	12-0	5-1	18-0	7-7

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Nautical Almanac

1978 APRIL 4, 5, 6 (TUES., WED., THURS.)

GMT	ARIES			VENUS -3.3			MARS +0.6			JUPITER -1.7			SATURN +0.5			STARS		
	G.H.A.	G.M.A.	Dec.	G.H.A.	G.M.A.	Dec.	G.H.A.	G.M.A.	Dec.	G.H.A.	G.M.A.	Dec.	G.H.A.	G.M.A.	Dec.	Name	S.H.A.	Dec.
4 00	191 57.4	162 32.5	N11 27.2	71 30.4	N23 14.1	103 07.7	N23 25.4	45 03.3	N14 57.9	Acamar	315 38.9	S40 27.8						
01	206 59.9	177 37.0	28.4	86 32.1	13.9	118 09.8	25.4	60 05.8	58.0	Achernar	335 47.2	S57 21.0						
02	222 02.3	192 31.5	29.5	101 33.7	13.7	133 11.9	25.4	75 08.4	58.0	Acrux	173 38.3	S62 58.8						
03	237 04.8	207 31.1	30.7	116 35.4	13.5	148 14.0	25.4	90 10.9	58.0	Adhara	255 33.4	S28 56.9						
04	252 07.3	222 30.6	31.8	131 37.1	13.2	163 16.1	25.4	105 13.5	58.1	Aldebaran	291 20.1	N16 27.8						
05	267 09.7	237 30.2	33.0	146 38.7	13.0	178 18.3	25.5	120 16.0	58.1									
06	282 12.2	252 29.7	N11 34.2	161 40.4	N23 12.8	193 20.4	N23 25.5	135 18.6	N14 58.1	Alioth	166 43.5	N56 04.6						
07	297 14.7	267 29.3	35.3	176 42.1	12.6	208 22.5	25.5	150 21.2	58.1	Alkaid	153 19.4	N49 25.2						
08	312 17.1	282 28.8	36.5	191 43.7	12.3	223 24.6	25.5	165 23.7	58.2	Al Na'ir	28 17.4	S47 03.9						
09	327 19.6	297 28.4	37.6	206 45.4	12.1	238 26.8	25.5	180 26.3	58.2	Alnilam	276 13.5	S 1 13.2						
10	342 22.0	312 27.9	38.8	221 47.0	11.9	253 28.9	25.5	195 28.8	58.2	Alphard	218 22.0	S 8 34.1						
11	357 24.5	327 27.5	39.9	236 48.7	11.7	268 31.0	25.5	210 31.4	58.3									
12	12 27.0	342 27.0	N11 41.1	251 50.4	N23 11.5	283 33.1	N23 25.5	225 33.9	N14 58.3	Alphecca	126 33.3	N26 47.1						
13	27 29.4	357 26.5	42.2	266 52.0	11.2	298 35.2	25.5	240 36.5	58.3	Alpheratz	358 11.4	N28 58.1						
14	42 31.9	12 26.1	43.4	281 53.7	11.0	313 37.4	25.5	255 39.0	58.3	Alhair	62 34.2	N 8 48.6						
15	57 34.4	27 25.6	44.5	296 55.3	10.8	328 39.5	25.5	270 41.6	58.4	Ankaa	353 42.4	S42 25.5						
16	72 36.8	42 25.2	45.7	311 57.0	10.6	343 41.6	25.5	285 44.1	58.4	Antares	112 58.7	S26 23.0						
17	87 39.3	57 24.7	46.9	326 58.7	10.3	358 43.7	25.5	300 46.7	58.4									
18	102 41.8	72 24.2	N11 48.0	342 00.3	N23 10.1	13 45.8	N23 25.5	315 49.2	N14 58.4	Arcturus	146 19.7	N19 17.6						
19	117 44.2	87 23.8	49.2	357 02.0	09.9	28 47.9	25.6	330 51.8	58.5	Atria	108 24.1	S68 59.1						
20	132 46.7	102 23.3	50.3	12 03.6	09.7	43 50.1	25.6	345 54.4	58.5	Avior	234 28.6	S59 26.8						
21	147 49.2	117 22.9	51.5	27 05.3	09.4	58 52.2	25.6	0 56.9	58.5	Bellatrix	279 00.7	N 6 19.6						
22	162 51.6	132 22.4	52.6	42 06.9	09.2	73 54.3	25.6	15 59.5	58.6	Betelgeuse	271 30.2	N 7 24.0						
23	177 54.1	147 21.9	53.8	57 08.6	09.0	88 56.4	25.6	31 02.0	58.6									
5 00	192 56.5	162 21.5	N11 54.9	72 10.2	N23 08.8	103 58.5	N23 25.6	46 04.6	N14 58.6	Canopus	264 08.0	S52 41.5						
01	207 59.0	177 21.0	56.1	87 11.9	08.5	119 00.6	25.6	61 07.1	58.6	Capella	281 14.0	N45 58.6						
02	223 01.5	192 20.6	57.2	102 13.5	08.3	134 02.8	25.6	76 09.7	58.7	Deneb	49 49.7	N45 11.9						
03	238 03.9	207 20.1	58.3	117 15.2	08.1	149 04.9	25.6	91 12.2	58.7	Denebola	183 00.4	N14 41.5						
04	253 06.4	222 19.6	11 59.5	132 16.8	07.9	164 07.0	25.6	106 14.8	58.7	Diphda	349 22.9	S18 06.5						
05	268 08.9	237 19.2	12 00.6	147 18.5	07.6	179 09.1	25.6	121 17.3	58.8									
06	283 11.3	252 18.7	N12 01.8	162 20.1	N23 07.4	194 11.2	N23 25.6	136 19.7	N14 58.8	Dubhe	194 23.7	N61 52.2						
07	298 13.8	267 18.2	02.9	177 21.8	07.2	209 13.3	25.6	151 22.4	58.8	Einah	278 46.4	N28 35.3						
08	313 16.3	282 17.8	04.1	192 23.4	07.0	224 15.5	25.6	166 25.0	58.8	Elanin	90 58.4	N51 29.3						
09	328 18.7	297 17.3	05.2	207 25.1	06.7	239 17.6	25.7	181 27.5	58.9	Enif	34 13.4	N 9 46.4						
10	343 21.2	312 16.8	06.4	222 26.7	06.5	254 19.7	25.7	196 30.1	58.9	Fomalhaut	15 53.6	S29 44.3						
11	358 23.6	327 16.4	07.5	237 28.4	06.3	269 21.8	25.7	211 32.6	58.9									
12	13 26.1	342 15.9	N12 08.6	252 30.0	N23 06.1	284 23.9	N23 25.7	226 35.2	N14 58.9	Gacrux	172 29.9	S56 59.6						
13	28 28.6	357 15.5	09.8	267 31.6	05.8	299 26.0	25.7	241 37.7	59.0	Gienah	176 19.3	S17 25.4						
14	43 31.0	12 15.0	10.9	282 33.3	05.6	314 28.1	25.7	256 40.3	59.0	Hadar	149 25.0	S60 16.1						
15	58 33.5	27 14.5	12.1	297 34.9	05.4	329 30.3	25.7	271 42.8	59.0	Hamal	328 31.1	N23 21.5						
16	73 36.0	42 14.1	13.2	312 36.6	05.1	344 32.4	25.7	286 45.4	59.0	Kaus Aust.	84 19.0	S34 23.6						
17	88 38.4	57 13.6	14.4	327 38.2	04.9	359 34.5	25.7	301 47.9	59.1									
18	103 40.9	72 13.1	N12 15.5	342 39.8	N23 04.7	14 36.6	N23 25.7	316 50.5	N14 59.1	Kochab	137 18.0	N74 14.6						
19	118 43.4	87 12.6	16.6	357 41.5	04.5	29 38.7	25.7	331 53.0	59.1	Morkab	14 05.1	N15 05.2						
20	133 45.8	102 12.2	17.8	12 43.1	04.2	44 40.8	25.7	346 55.6	59.2	Menkar	314 43.1	N 4 00.1						
21	148 48.3	117 11.7	18.9	27 44.8	04.0	59 42.9	25.7	1 58.1	59.2	Menkent	148 38.6	S36 15.8						
22	163 50.8	132 11.2	20.0	42 46.4	03.8	74 45.0	25.7	17 00.7	59.2	Miaplacidus	221 44.7	S69 38.0						
23	178 53.2	147 10.8	21.2	57 48.0	03.6	89 47.1	25.7	32 03.2	59.2									
6 00	193 55.7	162 10.3	N12 22.3	72 49.7	N23 03.3	104 49.3	N23 25.8	47 05.8	N14 59.3	Mirfak	309 18.8	N49 47.0						
01	208 58.1	177 07.8	23.5	87 51.3	03.1	119 51.4	25.8	62 08.3	59.3	Nunki	76 31.2	S26 19.3						
02	224 00.6	192 09.4	24.6	102 52.7	02.9	134 53.5	25.8	77 10.9	59.3	Pegacock	54 01.3	S56 48.1						
03	239 03.1	207 08.9	25.7	117 54.6	02.6	149 55.6	25.8	92 13.4	59.3	Pollux	244 00.2	N28 04.7						
04	254 05.5	222 08.4	26.9	132 56.2	02.4	164 57.7	25.8	107 15.9	59.4	Procyon	245 27.5	N 5 16.7						
05	269 08.0	237 07.9	28.0	147 57.8	02.2	179 59.8	25.8	122 18.5	59.4									
06	284 10.5	252 07.5	N12 29.1	162 59.5	N23 01.9	195 01.9	N23 25.8	137 21.0	N14 59.4	Rosalhague	96 31.0	N12 34.4						
07	299 12.9	267 07.0	30.3	178 01.1	01.7	210 04.0	25.8	152 23.6	59.4	Regulus	208 11.6	N12 04.3						
08	314 15.4	282 06.5	31.4	193 02.7	01.5	225 06.1	25.8	167 26.1	59.5	Rigel	281 37.8	S 8 13.9						
09	329 17.9	297 06.1	32.5	208 04.4	01.3	240 08.2	25.8	182 28.7	59.5	Rigel Kent.	140 27.4	S60 44.6						
10	344 20.3	312 05.6	33.7	223 06.0	01.0	255 10.4	25.8	197 31.2	59.5	Sabik	102 42.9	S15 41.7						
11	359 22.8	327 05.1	34.8	238 07.6	00.8	270 12.5	25.8	212 33.8	59.5									
12	14 25.3	342 04.6	N12 35.9	253 09.2	N23 00.6	285 14.6	N23 25.8	227 36.3	N14 59.6	Schedar	350 11.4	N56 25.0						
13	29 27.7	357 04.2	37.1	268 10.9	00.3	300 16.7	25.8	242 38.9	59.6	Shaula	96 57.9	S37 05.1						
14	44 30.2	12 03.7	38.2	283 12.5	00.1	315 18.8	25.8	257 41.4	59.6	Sirius	258 57.2	S16 41.5						
15	59 32.6	27 03.2	39.3	298 14.1	22 59.9	330 20.9	25.9	272 44.0	59.6	Spica	158 59.0	S11 03.0						
16	74 35.1	42 02.7	40.4	313 15.7	59.6	345 23.0	25.9	287 46.5	59.7	Suhail	223 11.7	S43 21.0						
17	89 37.6	57 02.3	41.6	328 17.4	59.4	0 25.1	25.9	302 49.1	59.7									
18	104 40.0	72 01.8	N12 42.7	343 19.0	N22 59.2	15 27.2	N23 25.9	317 51.6	N14 59.7	Vega	80 56.9	N38 45.6						
19	119 42.5	87 01.3	43.8	358 20.6	58.9	30 29.3	25.9	332 54.1	59.7	Zuben'ubi	137 34.6	S15 57.1						
20	134 45.0	102 00.8	44.9	13 22.2	58.7	45 31.4	25.9	347 56.7	59.8									
21	149 47.4	117 00.3	46.1	28 23.9	58.5	60 33.5	25.9	2 59.2	59.8									
22	164 49.9	131 59.9	47.2	43 25.5	58.2	75 35.6	25.9	18 01.8	59.8	Venus	329 24.9	S 13 11						
23	179 52.4	146 59.4	48.3	58 27.1	58.0	90 37.7	25.9	33 04.3	59.8	Mars	239 13.7	S 19 09						
										Jupiter	271 02.0	S 17 02						
										Saturn	213 08.0	S 20 52						

Mer. Pass 11 06.4 v -0.5 d 1.1 e 1.6 d 0.2 c 2.1 d 0.0 s 2.5 d 0.0

Extracted from the NAUTICAL ALMANAC, HER MAJESTY'S NAUTICAL ALMANAC OFFICE, LONDON, U.K.

Identification of stars (*)

It is very important and necessary for navigators to be able to identify stars in the sky because of fixing position at sea. Navigators have to know the names of stars, so that they can obtain the stars' G.H.A. and declination from the nautical almanac.

Navigational stars can be distinguished from others by their relative positions, brightness and their characteristic colour.

On the other hand, we occasionally observe an unfamiliar star in the sky. In this case, we can also find its proper name by D.R.P., G.M.T., altitude and azimuth.

To memorize the names of navigational stars, it is convenient and effective for you to compare a Star Map with stars shining in the dark sky.

1. Star identification by Star Map or table "Position of navigational stars".

The positions of navigational stars are shown on a Star Map (Fig. 16 & 17) and a table for position of navigational stars, with their declination and right ascension.

The navigator has to choose the Star Map for north latitude or the Star Map for south latitude to identify a star (see Fig. 16, 17 and 18), depending on his own position. To use the Star Map, some calculations are necessary as follows:

1) According to the observer's latitude, he must choose the Star Map for north latitude or south latitude.

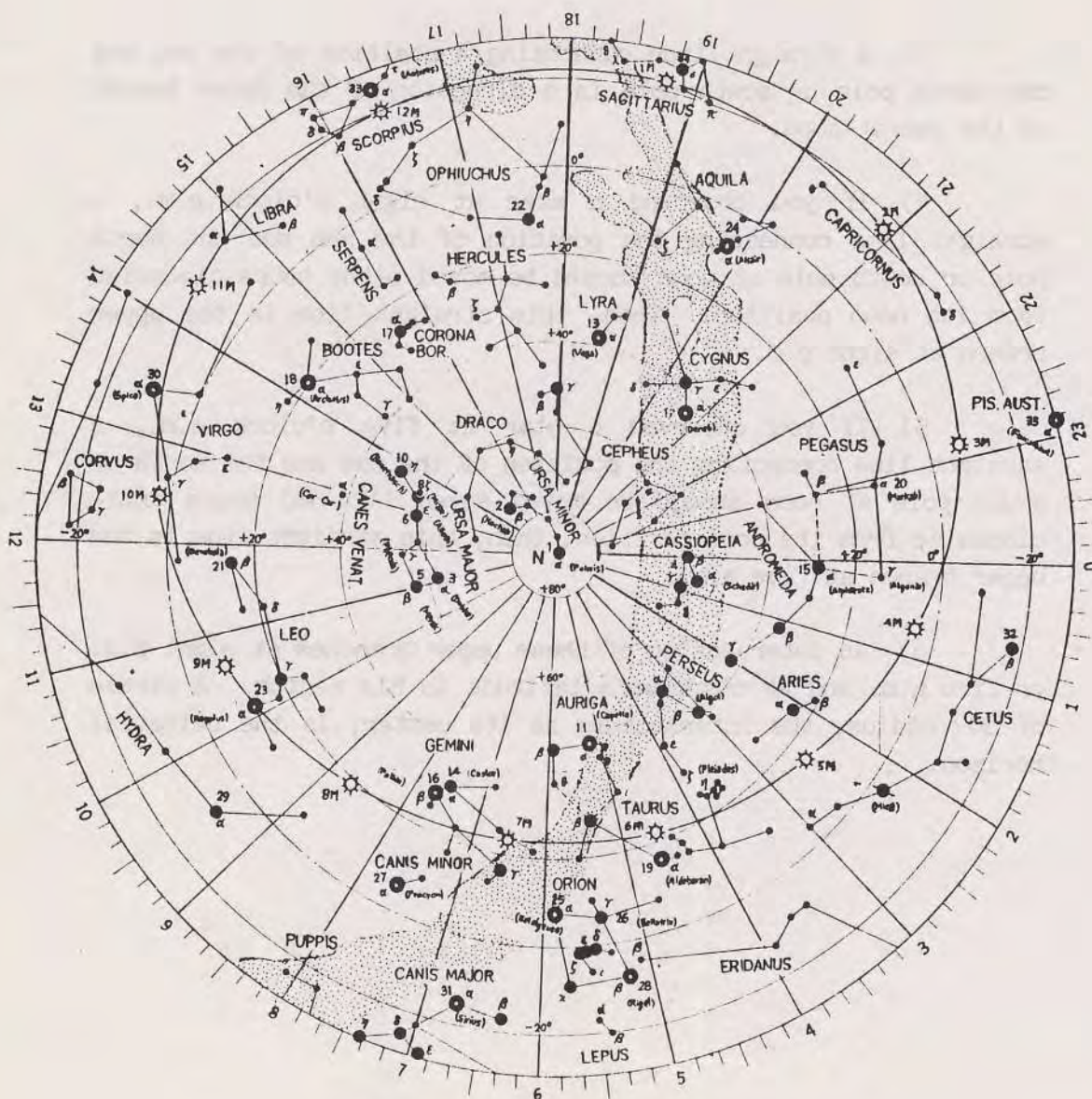
2) A star map has the position of the sun for the first day of each month on a circle of ecliptic (Fig. 16 and 17), so you should check the then position of the sun on the ecliptic.

3) A straight line connecting a position of the sun and the north pole or south pole is a direction of the upper branch of the sun at noon.

4) If you observed a star at eight o'clock p.m., a straight line connecting the position of the sun and the north pole or south pole at noon should be moved eight hours clockwise from its noon position. Then, this straight line is the upper branch at eight p.m..

5) If you observed a star at five o'clock a.m., a straight line connecting the position of the sun and the north or south pole at noon should be moved seven (12h-5h) hours anti-clockwise from its noon position, then, this straight line is the upper branch at five a.m..

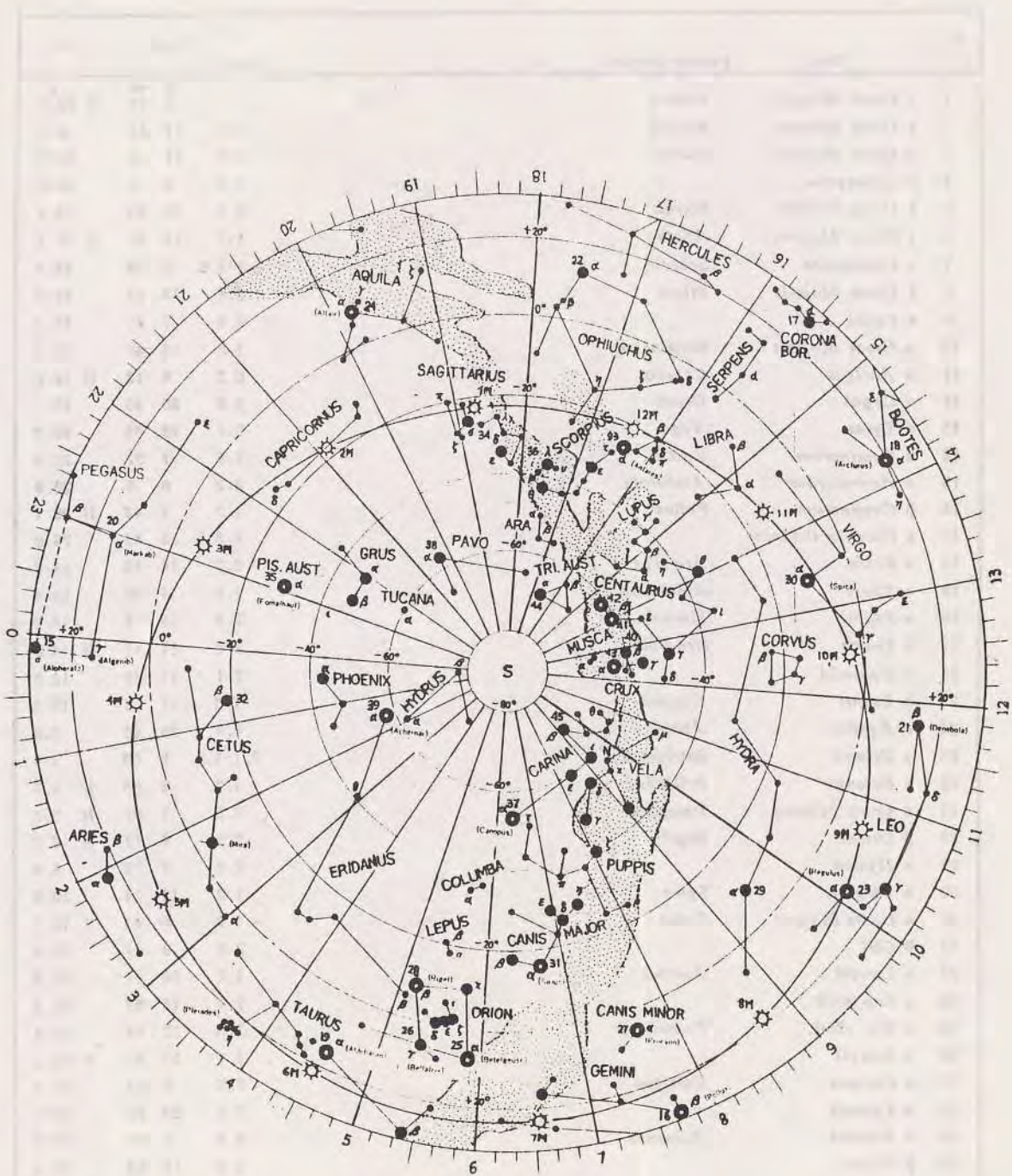
6) An intersection of these upper branches at eight p.m. or five a.m. and an observer's latitude is his zenith. A circle of 90° radius, the intersection as its center, is the celestial horizon.



Star Map (North Latitude)

Fig. 16-a

- First Magnitude or over
- Second Magnitude
- Third Magnitude
- Variable Star
- () Proper Name of Star
- Milky Way



Star Map (South Latitude)

Fig. 17

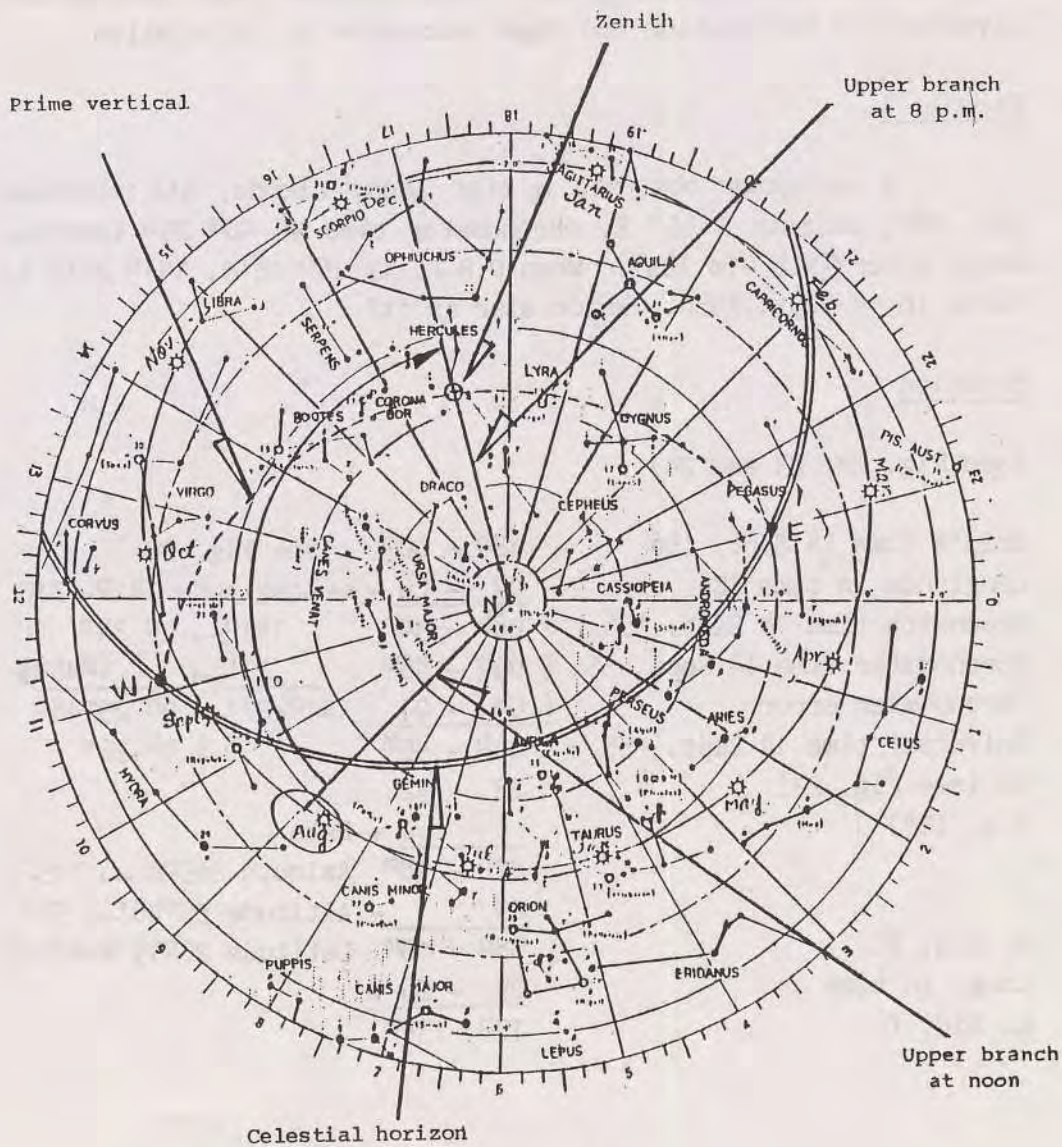
No.	Star	Proper Name	Mag.	R. A.		d
				h	m	
1	α <i>Ursae Minoris</i>	<i>Polaris</i>	2.1	1	53	N 89.1
2	β <i>Ursae Minoris</i>	<i>Kochab</i>	2.2	14	51	74.3
3	α <i>Ursae Majoris</i>	<i>Dubhe</i>	2.0	11	1	62.0
4	β <i>Cassiopeiae</i>		2.4	0	7	58.9
5	β <i>Ursae Majoris</i>	<i>Merak</i>	2.4	10	59	56.6
6	ϵ <i>Ursae Majoris</i>	<i>Alioth</i>	1.7	12	52	N 56.2
7	α <i>Cassiopeiae</i>	<i>Schedir</i>	2.1-2.6	0	38	56.3
8	ζ <i>Ursae Majoris</i>	<i>Mizar</i>	2.4	13	22	55.2
9	α <i>Persel</i>		1.9	8	21	49.7
10	η <i>Ursae Majoris</i>	<i>Benetnasch</i>	1.9	13	46	49.5
11	α <i>Aurigae</i>	<i>Capella</i>	0.2	5	13	N 46.0
12	α <i>Cygni</i>	<i>Deneb</i>	1.3	20	40	45.1
13	α <i>Lyrae</i>	<i>Vega</i>	0.1	18	35	38.7
14	α <i>Geminorum</i>	<i>Castor</i>	1.6	7	32	32.0
15	α <i>Andromedae</i>	<i>Alpheratz</i>	2.2	0	6	28.9
16	β <i>Geminorum</i>	<i>Pollux</i>	1.2	7	43	N 28.1
17	α <i>Coronae Borealis</i>		2.3	15	33	26.9
18	α <i>Bootis</i>	<i>Arcturus</i>	0.2	14	14	19.4
19	α <i>Tauri</i>	<i>Aldebaran</i>	1.1	4	33	16.4
20	α <i>Pegasi</i>	<i>Markab</i>	2.6	23	9	15.0
21	β <i>Leonis</i>	<i>Denebola</i>	2.2	11	47	N 14.8
22	α <i>Ophiuchi</i>		2.1	17	33	12.6
23	α <i>Leonis</i>	<i>Regulus</i>	1.3	10	6	12.2
24	α <i>Aquillae</i>	<i>Altair</i>	0.9	19	49	8.8
25	α <i>Orionis</i>	<i>Betelgeuse</i>	0.1-1.2	5	53	7.4
26	γ <i>Orionis</i>	<i>Bellatrix</i>	1.7	5	23	N 6.3
27	α <i>Canis Minoris</i>	<i>Procyon</i>	0.5	7	37	N 5.3
28	β <i>Orionis</i>	<i>Rigel</i>	0.3	5	12	S 8.3
29	α <i>Hydrae</i>		2.2	9	25	8.5
30	α <i>Virginis</i>	<i>Spica</i>	1.2	13	23	10.9
31	α <i>Canis Majoris</i>	<i>Sirius</i>	- 1.6	6	43	S 16.7
32	β <i>Celli</i>		2.2	0	41	18.2
33	α <i>Scorpii</i>	<i>Antares</i>	1.2	16	27	26.3
34	α <i>Sagittarii</i>		2.1	18	53	26.4
35	α <i>Pis. Aust.</i>	<i>Fomalhaut</i>	1.8	22	55	29.9
36	λ <i>Scorpii</i>		1.7	17	31	S 37.1
37	α <i>Carinae</i>	<i>Canopus</i>	- 0.9	6	23	52.7
38	α <i>Pavonis</i>		2.1	20	22	56.9
39	α <i>Eridani</i>	<i>Achernar</i>	0.6	1	36	57.5
40	β <i>Crucis</i>		1.5	12	45	59.4
41	β <i>Centauri</i>		0.9	14	1	S 60.2
42	α <i>Centauri</i>		0.1	14	37	60.7
43	α <i>Crucis</i>		1.1	12	24	62.9
44	α <i>Trianguli Australis</i>		1.9	16	44	68.9
45	β <i>Carinae</i>		1.8	9	13	S 69.5

Fig. 18 Position of navigational stars.

Example 6

Show navigational stars and their position in Lat. 35°N at 8 p.m.,
4 Aug. 1956, by Star Map.

Solution



Star map & Celestial horizon

Fig. 19

Identification by calculation

When the sky is clear, we can identify navigational stars by sight. But if we find a star among some clouds in the sky, it is very difficult to identify and find the name of the star using the Star Map. In this case, we can identify the star by observing its altitude, azimuth and time, because this information gives us its declination and right ascension by calculation.

Example 7

A navigator observed a star among clouds, its altitude $55^{\circ} 48'$, azimuth S 65° E, chronometer time $9^{\text{h}} 46^{\text{m}} 25^{\text{s}}$ (chronometer error $\ominus 1^{\text{h}} 01^{\text{m}} 12^{\text{s}}$). When D.R.P. is $26^{\circ} 15' \text{N}$, $141^{\circ} 27' \text{E}$ at 18:00 in 14 Sept. 1956. Which star is it?

Solution

(see Fig. 22, 23 and 24)

ship's time 14 Sept. '56	18h - 00m	see Fig. 20
Longitude in time (E)	09 - 26	↔ Longitude $141^{\circ} 27' \text{E}$
Greenwich time 14 Sept. '56	08h - 34m	$141^{\circ} \rightarrow 9^{\text{h}} 24^{\text{m}}$
Chronometer time 14 Sept. '56	09h - 46m	$\underline{27'} \rightarrow \underline{1^{\text{m}} 48^{\text{s}} \oplus}$
Chronometer error	01 - 01	$141^{\circ} 27' \rightarrow 9^{\text{h}} 25^{\text{m}} 48^{\text{s}}$
Universal time 14 Sept. '56	08h - 45m	$\div 9^{\text{h}} 26^{\text{m}}$
Ro (see Fig. 21)	23 - 32	
p.p. (E*)	<u>1</u> + Data	
	32h - 18m	Azimuth S $65^{\circ} \text{E} \rightarrow 115^{\circ} \text{E}$
	24	- Altitude $55^{\circ} 48' \rightarrow 56^{\circ}$
G. Sid. T.	08h - 18m	Latitude $26^{\circ} 15' \text{N} \rightarrow 26^{\circ} \text{N}$
Long. in time	09 - 26	+
L. Sid. T.	17h - 34m	

	K	D	H
Z = 115°E	K ₁ = 374		H ₁ = 3331
Alt. = 56°	<u>K₂ = 3171 ⊕</u>	D ₁ = 2919	
ℓ = ⊕ 26°N			
K = ⊖ 16° ←	K ₃ = 3545	D ₂ = 17	H ₂ = 2440
ℓ + K = ⊕ 10		D ₃ = 2240 ⊕	H ₃ = 7 ⊕
		D ₄ = 5176	H ₄ = 5778
		↓	↓
		d = 9°N	hE = 2 ^h - 04 ^m
			<u>L. sid, T = 17 - 34 ⊕</u>
			R.A. = 19 ^h 48 ^m

From d = 9°N, R.A. = 19^h 48^m, the star's proper name is Altair on Star map or table of Position of Navigational Stars.

Ans. Altair

h	m	o	h	m	o	h	m	o	h	m	o	h	m	o	h	m	o	m	s	l	s	i
0	0	0	4	0	60	8	0	120	12	0	180	16	0	240	20	0	300	0	0	0	0	0
4	1	1	4	4	64	8	4	124	12	4	184	16	4	244	20	4	304	0	4	0.1	0.1	0.0
8	2	2	8	8	68	8	8	128	12	8	188	16	8	248	20	8	308	0	8	0.2	0.1	0.1
12	3	3	12	12	72	8	12	132	12	12	192	16	12	252	20	12	312	0	12	0.3	0.1	0.1
16	4	4	16	16	76	8	16	136	12	16	196	16	16	256	20	16	316	0	16	0.4	0.1	0.1
20	5	5	20	20	80	8	20	140	12	20	200	16	20	260	20	20	320	0	20	0.5	0.1	0.1
24	6	6	24	24	84	8	24	144	12	24	204	16	24	264	20	24	324	0	24	0.6	0.2	0.2
28	7	7	28	28	88	8	28	148	12	28	208	16	28	268	20	28	328	0	28	0.7	0.2	0.2
32	8	8	32	32	92	8	32	152	12	32	212	16	32	272	20	32	332	0	32	0.8	0.2	0.2
36	9	9	36	36	96	8	36	156	12	36	216	16	36	276	20	36	336	0	36	0.9	0.2	0.2
40	10	10	40	40	100	8	40	160	12	40	220	16	40	280	20	40	340	0	40	1.0	0.3	0.3
44	11	11	44	44	104	8	44	164	12	44	224	16	44	284	20	44	344	0	44	1.1	0.3	0.3
48	12	12	48	48	108	8	48	168	12	48	228	16	48	288	20	48	348	0	48	1.2	0.3	0.3
52	13	13	52	52	112	8	52	172	12	52	232	16	52	292	20	52	352	0	52	1.3	0.3	0.3
56	14	14	56	56	116	8	56	176	12	56	236	16	56	296	20	56	356	0	56	1.4	0.4	0.4
1	0	15	6	0	75	9	0	135	13	0	195	17	0	255	21	0	315	1	0	1.5	0.4	0.4
4	16	16	4	4	78	9	4	138	13	4	198	17	4	258	21	4	318	1	4	1.6	0.4	0.4
8	17	17	8	8	81	9	8	141	13	8	201	17	8	261	21	8	321	1	8	1.7	0.4	0.4
12	18	18	12	12	84	9	12	144	13	12	204	17	12	264	21	12	324	1	12	1.8	0.5	0.5
16	19	19	16	16	87	9	16	147	13	16	207	17	16	267	21	16	327	1	16	1.9	0.5	0.5
20	20	20	20	20	90	9	20	150	13	20	210	17	20	270	21	20	330	1	20	2.0	0.5	0.5
24	21	21	24	24	93	9	24	153	13	24	213	17	24	273	21	24	333	1	24	2.1	0.5	0.5
28	22	22	28	28	96	9	28	156	13	28	216	17	28	276	21	28	336	1	28	2.2	0.6	0.6
32	23	23	32	32	99	9	32	159	13	32	219	17	32	279	21	32	339	1	32	2.3	0.6	0.6
36	24	24	36	36	102	9	36	162	13	36	222	17	36	282	21	36	342	1	36	2.4	0.6	0.6
40	25	25	40	40	105	9	40	165	13	40	225	17	40	285	21	40	345	1	40	2.5	0.6	0.6
44	26	26	44	44	108	9	44	168	13	44	228	17	44	288	21	44	348	1	44	2.6	0.7	0.7
48	27	27	48	48	111	9	48	171	13	48	231	17	48	291	21	48	351	1	48	2.7	0.7	0.7
52	28	28	52	52	114	9	52	174	13	52	234	17	52	294	21	52	354	1	52	2.8	0.7	0.7
56	29	29	56	56	117	9	56	177	13	56	237	17	56	297	21	56	357	1	56	2.9	0.7	0.7
2	0	30	6	0	90	10	0	150	14	0	210	18	0	270	22	0	330	2	0	3.0	0.8	0.8
4	31	31	4	4	93	10	4	153	14	4	213	18	4	273	22	4	333	2	4	3.1	0.8	0.8
8	32	32	8	8	96	10	8	156	14	8	216	18	8	276	22	8	336	2	8	3.2	0.8	0.8
12	33	33	12	12	99	10	12	159	14	12	219	18	12	279	22	12	339	2	12	3.3	0.8	0.8
16	34	34	16	16	102	10	16	162	14	16	222	18	16	282	22	16	342	2	16	3.4	0.9	0.9
20	35	35	20	20	105	10	20	165	14	20	225	18	20	285	22	20	345	2	20	3.5	0.9	0.9
24	36	36	24	24	108	10	24	168	14	24	228	18	24	288	22	24	348	2	24	3.6	0.9	0.9
28	37	37	28	28	111	10	28	171	14	28	231	18	28	291	22	28	351	2	28	3.7	0.9	0.9
32	38	38	32	32	114	10	32	174	14	32	234	18	32	294	22	32	354	2	32	3.8	1.0	1.0
36	39	39	36	36	117	10	36	177	14	36	237	18	36	297	22	36	357	2	36	3.9	1.0	1.0
40	40	40	40	40	120	10	40	180	14	40	240	18	40	300	22	40	360	2	40	4.0	1.0	1.0
44	41	41	44	44	123	10	44	183	14	44	243	18	44	303	22	44	363	2	44	4.1	1.0	1.0
48	42	42	48	48	126	10	48	186	14	48	246	18	48	306	22	48	366	2	48	4.2	1.0	1.0
52	43	43	52	52	129	10	52	189	14	52	249	18	52	309	22	52	369	2	52	4.3	1.0	1.0
56	44	44	56	56	132	10	56	192	14	56	252	18	56	312	22	56	372	2	56	4.4	1.0	1.0
3	0	45	7	0	105	11	0	165	15	0	225	19	0	285	23	0	345	3	0	4.5	1.0	1.0
4	46	46	4	4	108	11	4	168	15	4	228	19	4	288	23	4	348	3	4	4.6	1.0	1.0
8	47	47	8	8	111	11	8	171	15	8	231	19	8	291	23	8	351	3	8	4.7	1.0	1.0
12	48	48	12	12	114	11	12	174	15	12	234	19	12	294	23	12	354	3	12	4.8	1.0	1.0
16	49	49	16	16	117	11	16	177	15	16	237	19	16	297	23	16	357	3	16	4.9	1.0	1.0
20	50	50	20	20	120	11	20	180	15	20	240	19	20	300	23	20	360	3	20	5.0	1.0	1.0
24	51	51	24	24	123	11	24	183	15	24	243	19	24	303	23	24	363	3	24	5.1	1.0	1.0
28	52	52	28	28	126	11	28	186	15	28	246	19	28	306	23	28	366	3	28	5.2	1.0	1.0
32	53	53	32	32	129	11	32	189	15	32	249	19	32	309	23	32	369	3	32	5.3	1.0	1.0
36	54	54	36	36	132	11	36	192	15	36	252	19	36	312	23	36	372	3	36	5.4	1.0	1.0
40	55	55	40	40	135	11	40	195	15	40	255	19	40	315	23	40	375	3	40	5.5	1.0	1.0
44	56	56	44	44	138	11	44	198	15	44	258	19	44	318	23	44	378	3	44	5.6	1.0	1.0
48	57	57	48	48	141	11	48	201	15	48	261	19	48	321	23	48	381	3	48	5.7	1.0	1.0
52	58	58	52	52	144	11	52	204	15	52	264	19	52	324	23	52	384	3	52	5.8	1.0	1.0
56	59	59	56	56	147	11	56	207	15	56	267	19	56	327	23	56	387	3	56	5.9	1.0	1.0

Fig. 20 Conversion of Arc to Time.

Nautical Almanac

14 Sept. 1956

Lunar Age 9.2

☉ Sun					Planet					P.P.		☾ Moon Tr. 20 1					P.P.		
U	L _o	l	d	d	P.P.	U	E _p	d	E _p	d	U	E _l	d	E _l	d				
h m s	h m s	h m s	h m s	h m s	h m s	♀ Venus Tr. 8 59					h m s	h m s	h m s	h m s	h m s				
0 12 4 18	N 3	30.6	0 0	0.0	0 0 0 0														
2 20		28.7	10	2															
4 22		26.8	20	3															
6 24		24.9	30	5															
8 25		22.9	40	6															
10 27		21.0	0 50	0.8															
12 12 4 29	N 3	19.1	1 0	1.0															
14 31		17.2	10	1															
16 32		15.3	20	3															
18 34		13.3	30	4															
20 36		11.4	40	6															
22 38		9.5	1 50	7															
24 12 4 40	N 3	7.6	2 0	1.9															
S.D. 15 56)																			
U=0h					♂ Mars Tr. 23 46					♃ Jupiter Tr. 11 30					♄ Saturn Tr. 16 10				
No.	Star	E _k	d	d	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s				
1	Polaris	89	3.6		0 0 9 22	S 10	19.8	0 0 0 0	0 0 0 0	0 12 28 49	N 7	9.7	0 0 0 0	0 7 48 1	S 17	52.1	0 0 0 0		
2	Kochab	8 41	2	74	20.2					2 9 47		20.1	10 2 0	2 7 19		52.1	10 2 0		
3	Dubhe	12 30	44	61	53.0					4 10 12		20.4	20 4 1	4 37		52.2	20 3 0		
4	β Cassiopeia	23 24	52	58	51.8					6 10 37		20.7	30 6 1	6 48 56		52.3	30 5 0		
5	Merak	12 32	34	56	36.8					8 11 2		21.0	40 8 1	8 49 14		52.4	40 6 0		
6	Alioth	10 39	40	56	11.8					10 27		21.2	0 50 10	10 32		52.5	0 50 8 0		
7	Schedir	22 53	41	56	18.1					12 0 11 52	S 10	21.5	1 0 12 0.2	12 7 49 51	S 17	52.6	1 0 9 0.1		
8	Mizar	10 9	37	55	9.2					14 12 17		21.8	10 15 2	14 50 9		52.7	10 11 1		
9	α Persei	20 10	31	49	42.4					16 12 43		22.1	20 17 2	16 27		52.8	20 12 1		
10	Benetnasch	9 45	58	49	31.9					18 13 8		22.4	30 19 2	18 50 46		52.9	30 14 1		
11	Capella	18 18	16	57.2						20 33		22.6	40 21 3	20 51 4		53.0	40 15 1		
12	Deneb	2 51	47	45	7.8					22 13 58	S 10	22.9	1 50 23 3	22 22		53.1	1 50 17 1		
13	Vega	4 56	17	38	44.9					24 0 14 23	S 10	23.2	2 0 25 0.3	24 7 51 40	S 17	53.2	2 0 18 0.1		
14	Castor	15 59	56	31	59.0					♃ Jupiter Tr. 11 30									
15	Alpheratz	23 25	35	28	51.3					♄ Saturn Tr. 16 10									
16	Pollux	15 49	6	28	7.8					h m s	h m s	h m s	h m s	h m s	h m s				
17	α Cor. Bor.	7 58	55	26	51.8					0 12 28 49	N 7	9.7	0 0 0 0	0 7 48 1	S 17	52.1	0 0 0 0		
18	Arcturus	9 18	6	19	24.6					2 9 47		20.1	10 2 0	2 7 19		52.1	10 2 0		
19	Aldebaran	18 58	19	16	25.5					4 10 12		20.4	20 4 1	4 37		52.2	20 3 0		
20	Markab	0 29	8	14	58.6					6 10 37		20.7	30 6 1	6 48 56		52.3	30 5 0		
21	Denebola	11 44	56	14	48.9					8 11 2		21.0	40 8 1	8 49 14		52.4	40 6 0		
22	α Ophiuchi	5 58	50	12	35.7					10 27		21.2	0 50 10	10 32		52.5	0 50 8 0		
23	Regulus	13 25	43	12	10.8					12 12 30 23	N 7	7.2	1 0 8 0.2	12 7 49 51	S 17	52.6	1 0 9 0.1		
24	Altair	3 43	5	8	45.4					14 39		6.8	10 9 2	14 50 9		52.7	10 11 1		
25	Betelgeuse	17 38	56	7	24.1					16 30 55		6.4	20 11 3	16 27		52.8	20 12 1		
26	β Latrix	18 8	57	6	18.8					18 31 10		6.0	30 12 3	18 50 46		52.9	30 14 1		
27	Procyon	15 54	44	5	20.3					20 26		5.5	40 13 3	20 51 4		53.0	40 15 1		
28	Rigel	18 19	18	8	14.9					22 42		5.1	1 50 15 4	22 22		53.1	1 50 17 1		
29	α Hydrae	14 6	19	8	28.2					24 12 31 57	N 7	4.7	2 0 16 0.4	24 7 51 40	S 17	53.2	2 0 18 0.1		
30	Spica	10 8	52	10	56.1					♃ Jupiter Tr. 11 30									
31	Sirius	16 48	32	16	39.2					♄ Saturn Tr. 16 10									
32	β Ceti	22 50	20	18	13.2					h m s	h m s	h m s	h m s	h m s	h m s				
33	Antares	7 5	1	26	20.3					0 7 48 1	S 17	52.1	0 0 0 0	0 7 48 1	S 17	52.1	0 0 0 0		
34	♆ Sagittarii	4 39	10	26	21.1					2 9 47		20.1	10 2 0	2 7 19		52.1	10 2 0		
35	Fomalhaut	0 36	29	29	50.9					4 10 12		20.4	20 4 1	4 37		52.2	20 3 0		
36	λ Scorpii	6 1	5	5	37	4.5				6 10 37		20.7	30 6 1	6 48 56		52.3	30 5 0		
37	Canopus	17 8	47	52	40.0					8 11 2		21.0	40 8 1	8 49 14		52.4	40 6 0		
38	α Pavonis	3 9	30	56	52.5					10 27		21.2	0 50 10	10 32		52.5	0 50 8 0		
39	Achernar	21 55	38	57	27.1					12 12 30 23	N 7	7.2	1 0 8 0.2	12 7 49 51	S 17	52.6	1 0 9 0.1		
40	β Crucis	10 46	37	59	27.3					14 39		6.8	10 9 2	14 50 9		52.7	10 11 1		
41	β Centauri	9 31	2	860	10.1					16 30 55		6.4	20 11 3	16 27		52.8	20 12 1		
42	α Centauri	8 55	8	60	39.7					18 31 10		6.0	30 12 3	18 50 46		52.9	30 14 1		
43	δ Crucis	11 7	37	62	51.7					20 26		5.5	40 13 3	20 51 4		53.0	40 15 1		
44	α Tri. Aust.	6 47	41	68	57.3					22 42		5.1	1 50 15 4	22 22		53.1	1 50 17 1		
45	β Carinae	14 19	5	869	32.2					24 12 31 57	N 7	4.7	2 0 16 0.4	24 7 51 40	S 17	53.2	2 0 18 0.1		
h m s																			
Ro 23 31 47																			
Planets																			
					R.A.		d		Mag.		H.P.		S.D.						
					♃	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s					
					♃	8 31	N 17 15	-3.9	0.2	10									
					♂	23 22	S 10 20	-2.6	0.4	12									
					♃	11 3	N 7 10	-1.2	0.0	14									
					♃	15 44	S 17 52	+0.8	0.0	7									
					♃	12 38	S 8 29	+1.0	0.2	5									

Fig. 21

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Star Identification

Z						d										
Z		K ₁	H ₁	Z		K ₁	H ₁	d		K ₂	D ₁	d		K ₂	D ₁	
°	'			°	'			°	'			°	'			
0	180	0	- ∞	45	135	151	3000	0	- ∞	- ∞		45	3000	2849		
1	179	0	+ 1242	46	134	158	3015	1	+ 1242	+ 1242		46	3015	2857		
2	178	0	1543	47	133	166	3030	2	1543	1543		47	3030	2864		
3	177	1	1719	48	132	174	3046	3	1719	1719		48	3046	2871		
4	176	1	1845	49	131	183	3061	4	1845	1844		49	3061	2878		
5	175	2	1942	50	130	192	3076	5	1942	1940		50	3076	2884		
6	174	2	2022	51	129	201	3092	6	2022	2019		51	3092	2891		
7	173	3	2089	52	128	211	3107	7	2089	2086		52	3107	2897		
8	172	4	2148	53	127	221	3123	8	2148	2144		53	3123	2902		
9	171	5	2200	54	126	231	3139	9	2200	2194		54	3139	2908		
10	170	7	2246	55	125	241	3155	10	2246	2240		55	3155	2913		
11	169	8	2289	56	124	252	3171	11	2289	2281		56	3171	2919		
12	168	10	2327	57	123	264	3187	12	2327	2318		57	3187	2924		
13	167	11	2363	58	122	276	3204	13	2363	2352		58	3204	2928		
14	166	13	2397	59	121	288	3221	14	2397	2384		59	3221	2933		
15	165	15	2428	60	120	301	3239	15	2428	2413		60	3239	2938		
16	164	17	2457	61	119	314	3256	16	2457	2440		61	3256	2942		
17	163	19	2485	62	118	328	3274	17	2485	2466		62	3274	2946		
18	162	22	2512	63	117	343	3293	18	2512	2490		63	3293	2950		
19	161	24	2537	64	116	358	3312	19	2537	2513		64	3312	2954		
20	160	27	2561	65	115	374	3331	20	2561	2534		65	3331	2957		
21	159	30	2584	66	114	391	3351	21	2584	2554		66	3351	2961		
22	158	33	2606	67	113	408	3372	22	2606	2574		67	3372	2964		
23	157	36	2628	68	112	426	3394	23	2628	2592		68	3394	2967		
24	156	39	2649	69	111	446	3416	24	2649	2609		69	3416	2970		
25	155	43	2669	70	110	466	3439	25	2669	2626		70	3439	2973		
26	154	46	2688	71	109	487	3463	26	2688	2642		71	3463	2976		
27	153	50	2707	72	108	510	3488	27	2707	2657		72	3488	2978		
28	152	54	2725	73	107	534	3515	28	2726	2672		73	3515	2981		
29	151	58	2744	74	106	560	3543	29	2744	2686		74	3543	2983		
30	150	62	2761	75	105	587	3572	30	2761	2699		75	3572	2985		
31	149	67	2779	76	104	616	3603	31	2779	2712		76	3603	2987		
32	148	72	2796	77	103	648	3637	32	2796	2724		77	3637	2989		
33	147	76	2813	78	102	682	3673	33	2813	2736		78	3673	2990		
34	146	81	2829	79	101	719	3711	34	2829	2748		79	3711	2992		
35	145	87	2845	80	100	760	3754	35	2845	2759		80	3754	2993		
36	144	92	2861	81	99	806	3800	36	2861	2769		81	3800	2995		
37	143	98	2877	82	98	856	3852	37	2877	2779		82	3852	2996		
38	142	103	2893	83	97	914	3911	38	2893	2789		83	3911	2997		
39	141	109	2908	84	96	981	3978	39	2908	2799		84	3978	2998		
40	140	116	2924	85	95	1060	4058	40	2924	2808		85	4058	2998		
41	139	122	2939	86	94	1156	4155	41	2939	2817		86	4155	2999		
42	138	129	2954	87	93	1261	4261	42	2954	2826		87	4261	2999		
43	137	136	2970	88	92	1457	4457	43	2970	2834		88	4457	3000		
44	136	143	2985	89	91	1758	4758	44	2985	2842		89	4758	3000		
45	135	151	3000	90	90	+ ∞	+ ∞	45	3000	2849		90	+ ∞	3000		

Measurement of Z (Azimuth)

Start from North as 0° to
180° easterly or westerly

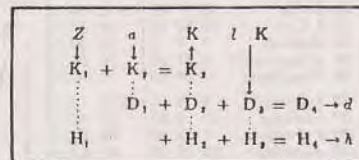


Fig. 22

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

K								l + K							
K ₃	K	D ₂	H ₂	K ₂	K	D ₂	H ₂	l+K		D ₃	H ₃	l+K		D ₃	H ₃
± ∞	0	0	- ∞	3000	45	151	2849	± 0	± 180	- ∞	0	± 45	± 135	2849	151
4758	1	0	+1242	2985	46	158	2857	1	179	+1242	0	46	134	2857	158
4457	2	0	1543	2970	47	166	2864	2	178	1543	0	47	133	2864	166
4281	3	1	1719	2954	48	174	2871	3	177	1719	1	48	132	2871	174
4155	4	1	1844	2939	49	183	2878	4	176	1844	1	49	131	2878	183
4058	5	2	1940	2924	50	192	2884	5	175	1940	2	50	130	2884	192
3978	6	2	2019	2908	51	201	2891	6	174	2019	2	51	129	2891	201
3911	7	3	2086	2893	52	211	2897	7	173	2086	3	52	128	2897	211
3852	8	4	2144	2877	53	221	2902	8	172	2144	4	53	127	2902	221
3800	9	5	2194	2861	54	231	2908	9	171	2194	5	54	126	2908	231
3754	10	7	2240	2845	55	241	2913	10	170	2240	7	55	125	2913	241
3711	11	8	2281	2829	56	252	2919	11	169	2281	8	56	124	2919	252
3673	12	10	2318	2813	57	264	2924	12	168	2318	10	57	123	2924	264
3637	13	11	2352	2796	58	276	2928	13	167	2352	11	58	122	2928	276
3603	14	13	2384	2779	59	288	2933	14	166	2384	13	59	121	2933	288
3572	15	15	2413	2761	60	301	2938	15	165	2413	15	60	120	2938	301
3543	16	17	2440	2744	61	314	2942	16	164	2440	17	61	119	2942	314
3515	17	19	2466	2726	62	328	2946	17	163	2466	19	62	118	2946	328
3488	18	22	2490	2707	63	343	2950	18	162	2490	22	63	117	2950	343
3463	19	24	2513	2688	64	358	2954	19	161	2513	24	64	116	2954	358
3439	20	27	2534	2669	65	374	2957	20	160	2534	27	65	115	2957	374
3416	21	30	2554	2649	66	391	2961	21	159	2554	30	66	114	2961	391
3394	22	33	2574	2628	67	408	2964	22	158	2574	33	67	113	2964	408
3372	23	36	2592	2606	68	426	2967	23	157	2592	36	68	112	2967	426
3351	24	39	2609	2584	69	446	2970	24	156	2609	39	69	111	2970	446
3331	25	43	2626	2561	70	466	2973	25	155	2626	43	70	110	2973	466
3312	26	46	2642	2537	71	487	2976	26	154	2642	46	71	109	2976	487
3293	27	50	2657	2512	72	510	2978	27	153	2657	50	72	108	2978	510
3274	28	54	2672	2485	73	534	2981	28	152	2672	54	73	107	2981	534
3256	29	58	2686	2457	74	560	2983	29	151	2686	58	74	106	2983	560
3239	30	62	2699	2428	75	587	2985	30	150	2699	62	75	105	2985	587
3221	31	67	2712	2397	76	616	2987	31	149	2712	67	76	104	2987	616
3204	32	72	2724	2363	77	648	2989	32	148	2724	72	77	103	2989	648
3187	33	76	2736	2327	78	682	2990	33	147	2736	76	78	102	2990	682
3171	34	81	2748	2289	79	719	2992	34	146	2748	81	79	101	2992	719
3155	35	87	2759	2246	80	760	2993	35	145	2759	87	80	100	2993	760
3139	36	92	2769	2200	81	806	2995	36	144	2769	92	81	99	2995	806
3123	37	98	2779	2148	82	856	2996	37	143	2779	98	82	98	2996	856
3107	38	103	2789	2089	83	914	2997	38	142	2789	103	83	97	2997	914
3092	39	109	2799	2022	84	981	2998	39	141	2799	109	84	96	2998	981
3076	40	116	2808	1942	85	1060	2998	40	140	2808	116	85	95	2998	1060
3061	41	122	2817	1845	86	1156	2999	41	139	2817	122	86	94	2999	1156
3046	42	129	2826	1719	87	1281	2999	42	138	2826	129	87	93	2999	1281
3030	43	136	2834	1543	88	1457	3000	43	137	2834	136	88	92	3000	1457
3015	44	143	2842	+1242	89	1758	3000	44	136	2842	143	89	91	3000	1758
3000	45	151	2849	- ∞	90	+ ∞	3000	± 45	± 135	2849	151	± 90	± 90	3000	+ ∞

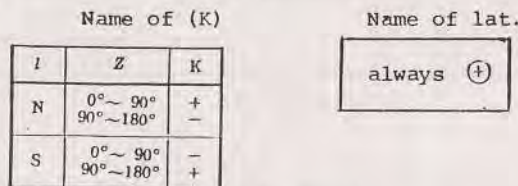


Fig. 23

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

d, h																		
D_4		d	D_4		d	H_4				H_4								
						h				h								
						k	m	o	h	m	o	h	m	o				
-	∞	0	5849	45	-	∞	0	0	12	0	180	6000	3	0	45	8	0	135
+	4242	1	5857	46	+	4242	0	4	11	56	179	6015	3	4	46	8	56	134
	4543	2	5864	47		4543	0	8	11	52	178	6030	3	8	47	8	52	133
	4719	3	5871	48		4719	0	12	11	48	177	6045	3	12	48	8	48	132
	4844	4	5878	49		4844	0	16	11	44	176	6061	3	16	49	8	44	131
	4940	5	5884	50		4942	0	20	11	40	175	6076	3	20	50	8	40	130
	5019	6	5891	51		5022	0	24	11	36	174	6092	3	24	51	8	36	129
	5086	7	5897	52		5089	0	28	11	32	173	6107	3	28	52	8	32	128
	5144	8	5902	53		5148	0	32	11	28	172	6123	3	32	53	8	28	127
	5194	9	5908	54		5200	0	36	11	24	171	6139	3	36	54	8	24	126
	5240	10	5913	55		5246	0	40	11	20	170	6155	3	40	55	8	20	125
	5281	11	5919	56		5289	0	44	11	16	169	6171	3	44	56	8	16	124
	5318	12	5924	57		5327	0	48	11	12	168	6187	3	48	57	8	12	123
	5352	13	5928	58		5363	0	52	11	8	167	6204	3	52	58	8	8	122
	5384	14	5933	59		5397	0	56	11	4	166	6221	3	56	59	8	4	121
	5413	15	5938	60		5428	1	0	11	0	165	6239	4	0	60	8	0	120
	5440	16	5942	61		5457	1	4	10	56	164	6256	4	4	61	7	56	119
	5466	17	5946	62		5485	1	8	10	52	163	6274	4	8	62	7	52	118
	5490	18	5950	63		5512	1	12	10	48	162	6293	4	12	63	7	48	117
	5513	19	5954	64		5537	1	16	10	44	161	6312	4	16	64	7	44	116
	5534	20	5957	65		5561	1	20	10	40	160	6331	4	20	65	7	40	115
	5554	21	5961	66		5584	1	24	10	36	159	6351	4	24	66	7	36	114
	5574	22	5964	67		5606	1	28	10	32	158	6372	4	28	67	7	32	113
	5592	23	5967	68		5628	1	32	10	28	157	6394	4	32	68	7	28	112
	5609	24	5970	69		5649	1	36	10	24	156	6416	4	36	69	7	24	111
	5626	25	5973	70		5669	1	40	10	20	155	6439	4	40	70	7	20	110
	5642	26	5976	71		5688	1	44	10	16	154	6463	4	44	71	7	16	109
	5657	27	5978	72		5707	1	48	10	12	153	6488	4	48	72	7	12	108
	5672	28	5981	73		5726	1	52	10	8	152	6515	4	52	73	7	8	107
	5686	29	5983	74		5744	1	56	10	4	151	6543	4	56	74	7	4	106
	5699	30	5985	75		5761	2	0	10	0	150	6572	5	0	75	7	0	105
	5712	31	5987	76		5779	2	4	9	56	149	6603	5	4	76	6	56	104
	5724	32	5989	77		5796	2	8	9	52	148	6637	5	8	77	6	52	103
	5736	33	5990	78		5813	2	12	9	48	147	6673	5	12	78	6	48	102
	5748	34	5992	79		5829	2	16	9	44	146	6711	5	16	79	6	44	101
	5759	35	5993	80		5845	2	20	9	40	145	6754	5	20	80	6	40	100
	5769	36	5995	81		5861	2	24	9	36	144	6800	5	24	81	6	36	99
	5779	37	5996	82		5877	2	28	9	32	143	6852	5	28	82	6	32	98
	5789	38	5997	83		5893	2	32	9	28	142	6911	5	32	83	6	28	97
	5799	39	5998	84		5908	2	36	9	24	141	6978	5	36	84	6	24	96
	5808	40	5998	85		5924	2	40	9	20	140	7058	5	40	85	6	20	95
	5817	41	5999	86		5939	2	44	9	16	139	7155	5	44	86	6	16	94
	5826	42	5999	87		5954	2	48	9	12	138	7281	5	48	87	6	12	93
	5834	43	6000	88		5970	2	52	9	8	137	7457	5	52	88	6	8	92
	5842	44	6000	89		5985	2	56	9	4	136	7758	5	56	89	6	4	91
	5849	45	6000	90		6000	3	0	9	0	135	+ ∞	6	0	90	6	0	90

Name of Dec. and R.A.

1. N or S of d.	when $l + k > 0$, same name as l $l + k < 0$, contrary name to l .
2. E or W of h	h should be measured from meridian to 12h, easterly or westerly. when l and d are the same name and $l + k > 90^\circ$, $h_1 > 6h$
3. R.A.	Sid. T. = $U + R + L$ in T. + E.L - W.L R.A. = Sid. T. $\pm h$ + Easterly from meridian - Westerly from meridian

Fig. 24

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Problem

A star's altitude is 50°2 and its azimuth is 057° in D.R.P. lat. 34°28'N, long. 135°0'E. Chronometer time is 10^h 21^m 50^s (C.E. = 029^m 26^s ⊖) and local time 06:50, 6 July 1956. (see Figs. 25, 26 and 27) What is the star's name? (See page 88&89)

6 July 1956 Lunar
Nautical Almanac Age 27.1

☉ Sun			Planet			☾ Moon		
U	E _s	d	U	E _p	d	U	E _t	d
h m s	° ' "	° ' "	h m s	° ' "	° ' "	h m s	° ' "	° ' "
0 11 55 20	N22 43.2	0 0 0.0	☿ Venus	Tr. 10 35	h m s	° ' "	° ' "	
2 27	42.7	10 0 0	h m s	° ' "	h m s	° ' "	° ' "	
4 26	42.2	20 1 1	0 13 22 13	N18 41.9	0 0 0.0	0 14 9 3	N21 53.5	1 3 0.0
6 25	41.7	30 1 1	2 22 39	41.8	10 2 1	7 49	54.1	2 5 0
8 24	41.2	40 2 2	4 23 5	40.6	20 4 1	9 34	54.7	3 8 0
10 24	40.7	50 2 2	6 31	40.0	30 7 2	11 50	55.2	4 10 1
12 11 55 23	N22 40.2	1 0 0.3	8 23 57	39.3	40 9 2	13 25	56.7	5 13 1
14 22	39.6	10 3 3	10 24 23	38.7	50 11 3	14 40	57.0	6 20 1
16 21	39.1	20 3 3	12 13 24 49	N18 38.0	1 0 13 0.3	16 59	57.4	7 23 1
18 20	38.6	30 4 4	14 25 14	37.4	10 15 4	18 15	57.7	8 25 1
20 20	38.1	40 4 4	16 25 40	36.8	20 17 4	19 40	58.0	9 28 1
22 19	37.6	50 5 5	18 26 5	36.2	30 20 5	21 10	58.2	10 30 2
24 11 55 18	N22 37.0	2 0 0.5	20 31	35.6	40 22 5	22 35	58.2	11 28 2
			22 26 56	35.0	50 24 6	24 10	58.2	12 20 2
			24 13 27 22	N18 34.3	2 0 26 0.6			13 33 2
								14 35 2
								15 36 2
								16 40 2
								17 43 2
								18 45 2
								19 48 3
								20 50 3
								21 53 3
								22 55 3
								23 58 3
								24 58 3
								25 58 3
								26 55 3
								27 48 4
								28 30 4
								29 33 4
								30 35 4
								31 35 4
								32 35 4
								33 35 4
								34 35 4
								35 35 4
								36 35 4
								37 35 4
								38 35 4
								39 35 4
								40 35 4
								41 35 4
								42 35 4
								43 35 4
								44 35 4
								45 35 4
								46 35 4
								47 35 4
								48 35 4
								49 35 4
								50 35 4
								51 35 4
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								66 35 4
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								72 35 4
								73 35 4
								74 35 4
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								77 35 4
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								80 35 4
								81 35 4
								82 35 4
								83 35 4
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								90 35 4
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								94 35 4
								95 35 4
								96 35 4
								97 35 4
								98 35 4
								99 35 4
								100 35 4

Fig. 25

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

5 July 1956
Nautical Almanac

Lunar
Age 26.1

☉ Sun				Planet			P.P.		☾ Moon Tr. ^{h m} 9 15		P.P.			
U	E _s	d	d の比部分 P.P.	U	E _s	d	E _s	d	U	E _t	d	E _t	d	
h h m s	° ′ ″	° ′ ″	° ′ ″	♀ Venus ^{h m} Tr. 10 41				h h m s	° ′ ″	m s	° ′ ″	m s	° ′ ″	
0 11 55 38	N 22 48.9	0 0	0.0	h h m s	° ′ ″	h m s	° ′ ″	0 15 7 23	N 20 39.3	1 2	0 0	1 2	0 0	
2 37	49.4	10	0	0 13 16 55	N 18 50.1	0 0	0 0	1 5 1	44.0	3 7	2	5 1		
4 37	49.0	20	1	2 17 22	49.4	10 2	1	2 3 50	46.3	4 10	3	5 2		
6 36	47.5	30	1	4 17 49	48.7	20 5	1	2 2 38	48.6	5 12	3	5 3		
8 35	47.0	40	2	6 18 16	48.0	30 7	2	3 15 0 15	50.8	6 14	4	5 4		
10 34	46.6	50	2	8 18 42	47.3	40 9	2	14 59 4	55.2	7 17	5	5 5		
12 11 55 33	N 22 46.1	1 0	0.3	10 19 9	46.6	0 50	11 3	4 57 52	57.4	8 19	5	6 6		
14 32	45.6	10	3	12 13 19 35	N 18 45.9	1 0	14 0.4	5 56 40	20 59.5	10 24	7	7 7		
16 31	45.1	20	3	14 20 2	45.2	10 16	4	5 55 29	21 1.5	11 26	7	8 8		
18 30	44.6	30	4	16 28	44.6	20 18	5	54 17	3.6	12 29	8	9 9		
20 30	44.1	40	4	18 20 55	43.9	30 20	5	(H.P.59.7, S.D.16 16)				13 31	9	
22 29	43.7	50	5	20 21 21	43.2	40 23	6	6 14 53 5	N 21 5.6	14 34	0.9	10 0		
24 11 55 28	N 22 43.2	2 0	0.5	22 21 47	42.6	1 50	25 6	7 51 53	7.6	15 36	1.0	1 1		
S.D. 15 46				24 13 22 13	N 18 41.9	2 0	27 0.7	7 50 41	9.5	16 38	1	1 1		
U=O ^h の値				♂ Mars ^{h m} Tr. 4 21				8 49 28	11.4	17 41	1	2 1		
No.	Star	E _s	d	h h m s	° ′ ″	h m s	° ′ ″	8 48 16	13.3	18 43	2	2 2		
1	Polaris	16 58 34	N 89 3.4	0 19 38 37	S 9 34.3	0 0	0 0 0.0	9 47 4	15.1	19 46	3	3 3		
2	Kochab	4 1 1	74 20.2	2 38 49	33.7	10 1	0	9 45 51	16.9	20 48	3	4 4		
3	Dubhe	7 50 48	61 59.3	4 39 0	33.2	20 2	1	10 44 38	18.6	21 50	4	5 5		
4	α Cassiop.	18 44 59	58 54.4	6 12	32.6	30 3	1	10 43 26	20.4	22 53	5	6 6		
5	Merak	7 52 38	56 37.1	8 24	32.1	40 4	2	11 42 13	22.0	23 55	6	7 7		
6	Alioth	5 59 43	N 56 11.9	10 36	31.5	0 50	5 2	11 41 0	23.7	25 60	7	8 8		
7	Schedir	18 13 48	56 17.8	12 19 39 48	S 9 31.0	1 0	6 0.3	11 39 47	25.3	26 62	7	9 9		
8	Mizar	5 29 40	55 9.3	14 40 0	30.4	10 7	3	12 14 38 35	N 21 26.9	27 70	1.9	10 10		
9	α Persei	15 30 39	49 42.3	16 12	29.9	20 8	3	12 14 38 35	N 21 26.9	30 72	2.0	11 11		
10	β Benetnasch	5 6 0	49 32.0	18 24	29.3	30 9	4	13 37 22	28.4	1 2	0.0	12 12		
11	Capella	13 38 23	N 45 57.2	20 36	28.8	40 10	4	13 36 8	29.9	2 5	1	13 13		
12	Deneb	22 11 52	45 7.5	22 40 48	28.3	1 50	11 5	14 34 55	31.4	3 7	1	14 14		
13	Vega	0 16 21	38 44.7	24 19 41 0	S 9 27.7	2 0	12 0.5	14 33 42	32.8	4 10	1	15 15		
14	Castor	11 20 2	31 59.1	♃ Jupiter ^{h m} Tr. 15 14				15 32 29	34.2	5 12	2	16 16		
15	Alpheratz	18 45 42	28 51.0	h h m s	° ′ ″	h m s	° ′ ″	16 31 15	35.6	6 15	2	17 17		
16	Pollux	11 9 12	N 28 7.9	0 8 44 1	N 12 34.2	0 0	0 0.0	16 30 2	36.9	7 17	3	18 18		
17	α Cor. Bor.	3 18 59	26 51.7	2 17	33.9	10 1	0	16 28 48	38.2	8 19	3	19 19		
18	Arcturus	4 38 9	19 24.6	4 33	33.6	20 3	1	17 27 35	39.4	9 22	3	20 20		
19	Aldebaran	14 18 26	16 25.4	6 44 50	33.3	30 4	1	17 26 21	40.6	10 24	4	21 21		
20	Markab	19 49 14	14 58.3	8 45 6	33.0	40 5	1	17 25 7	41.8	11 27	4	22 22		
21	Denebola	7 5 0	N 14 48.9	10 22	32.6	0 50	7 1	(H.P.60.1, S.D.16 23)				12 29	4	
22	α Ophiuchi	1 18 54	12 35.5	12 8 45 38	N 12 32.3	1 0	8 0.2	18 14 23 54	N 21 42.9	13 32	5	13 32		
23	Regulus	8 45 48	12 10.8	14 45 55	32.0	10 9	2	18 22 40	44.0	14 34	5	14 34		
24	Allair	23 3 9	8 45.3	16 46 11	31.7	20 11	2	19 21 26	45.1	15 37	6	15 37		
25	Betelgeuse	12 59 3	7 24.0	18 27	31.4	30 12	2	19 20 12	46.1	16 39	6	16 39		
26	Bellatrix	13 29 4	N 6 18.7	20 46 43	31.0	40 13	3	19 18 58	47.1	17 41	6	17 41		
27	Procyon	11 14 50	N 5 20.2	22 47 0	30.7	1 50	15 3	20 17 44	48.0	18 44	7	18 44		
28	Rigel	13 39 25	S 8 15.0	24 8 47 16	N 12 30.4	2 0	16 0.3	20 16 30	49.9	19 46	7	19 46		
29	α Hydrae	9 26 24	8 28.3	♄ Saturn ^{h m} Tr. 20 44				21 15 15	49.8	20 49	7	20 49		
30	Spica	5 28 56	10 56.2	h h m s	° ′ ″	h m s	° ′ ″	22 14 1	50.6	21 51	8	21 51		
31	Sirius	12 8 38	S 16 39.4	0 3 12 15	S 17 21.0	0 0	0 0.0	22 12 47	51.4	22 58	9	22 58		
32	β Ceti	18 10 26	18 13.3	2 35	21.0	10 2	0	23 11 32	52.1	23 61	0.9	23 61		
33	Antares	2 25 5	26 20.3	4 12 56	20.9	20 4	0	23 10 18	52.8	24 63	1.0	24 63		
34	α Sagittarii	23 59 14	26 21.0	6 13 16	20.9	30 5	0	24 14 9 3	N 21 53.5	25 65	0	25 65		
35	Fomalhaut	19 56 34	29 59.9	8 37	20.9	40 7	0	(H.P.60.3, S.D.16 26)				26 63	0	
36	λ Scorpii	1 21 9	S 37 4.4	10 13 57	20.9	0 50	9 0	27 11	51.4	27 71	1	27 71		
37	Canopus	12 28 54	S 2 40.3	12 3 14 18	S 17 20.8	1 0	11 0.0	Planet				28 69	0	
38	α Faoonis	22 29 35	S 6 52.3	14 38	20.8	10 12	0	R.A. d' Mag. H.P. S.D.				29 71	1	
39	Achernar	17 15 46	S 7 27.1	16 14 59	20.8	20 14	0	♀	5 35	N 18 50	-3.7	0.5	27	
40	β Crucis	6 6 40	S 9 27.4	18 15 19	20.8	30 16	0	♂	23 13	S 9 34	-1.1	0.2	8	
41	β Centauri	4 51 4	S 60 10.2	20 15 40	20.7	40 18	0	♂	10 8	N 12 34	-1.4	0.0	15	
42	α Centauri	4 15 11	60 39.8	22 16 1	20.7	1 50	19 0	♂	15 40	S 17 21	+0.5	0.0	8	
43	α Crucis	6 27 40	62 51.9	24 3 16 21	S 17 20.7	2 0	21 0.0	♀	5 46	N 22 40	-0.7	0.1	3	
44	α Tri. Aust.	2 7 43	68 57.2											
45	β Carinae	9 39 9	S 69 32.6											

Fig. 26

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

P.P. for E*				
U	m		m	
	0	10	20	30
h	m	s	m	s
0	0	00	0	02
1		10	11	13
2		20	21	23
3		30	31	33
4		39	41	43
5		49	0 51	0 53
6		0 59	1 01	1 02
7		1 09	1 11	1 12
8		1 19	1 20	1 22
9		1 29	1 30	1 32
10		1 39	1 40	1 42
11		1 48	1 50	1 52
12		1 58	2 00	2 02
13		2 08	2 10	2 11
14		2 18	2 20	2 21
15		2 28	2 29	2 31
16		2 38	2 39	2 41
17		2 48	2 49	2 51
18		2 57	3 00	3 01
19		3 07	3 09	3 11
20		3 17	3 19	3 20
21		3 27	3 29	3 30
22		3 37	3 38	3 40
23		3 47	3 48	3 50

U	m		m	
	30	40	50	60
h	m	s	m	s
0	0	05	0	07
1		15	16	18
2		25	26	28
3		34	36	38
4		44	46	48
5		0 54	0 56	0 57
6		1 04	1 06	1 07
7		1 14	1 16	1 17
8		1 24	1 25	1 27
9		1 34	1 35	1 37
10		1 43	1 45	1 47
11		1 53	1 55	1 57
12		2 03	2 05	2 06
13		2 13	2 15	2 16
14		2 23	2 25	2 26
15		2 33	2 34	2 36
16		2 43	2 44	2 46
17		2 52	2 54	2 56
18		3 02	3 04	3 06
19		3 12	3 14	3 15
20		3 22	3 24	3 25
21		3 32	3 34	3 35
22		3 42	3 43	3 45
23		3 52	3 53	3 55

Table of Proportional Parts

Fig. 27

Extracted from NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Latitude observation

1. Solution for meridian altitude

It is possible to give a latitude line for any celestial body when we observe its altitude at transit. The sun and Polaris are most commonly used for a latitude line. The sun transits the observer's meridian at local apparent noon (LAN). The LAN observation for a latitude line is very important, because this observation can show the most dependable celestial line of position of the day. The sun should be observed at local apparent noon as part of routine work on board vessel.

When the celestial body is either due north or south of the observer,

Transit upper branch $h = 0^h$ (h : Hour angle)
Transit lower branch $h = 12^h$

The formulae of spherical triangle are known as below,

$$\cos Z = \pm \sin \ell \sin d + \cos \ell \cos d \cos h \quad (Z : \text{Zenith distance})$$

$$\sin a = \sin \ell \cos p + \cos \ell \sin p \cos h$$

When a celestial body transits upper branch, "h" should be 0^h (0^0) then

$$\begin{aligned} \cos Z &= \pm \sin \ell \sin d + \cos \ell \cos d \frac{\cos 0^0}{1} \\ &= \pm \sin \ell \sin d + \cos \ell \cos d \times 1 \\ &= \pm \sin \ell \sin d + \cos \ell \cos d \\ &= \cos \ell \cos d \pm \sin \ell \sin d \\ &= \cos (\ell \tilde{+} d) \quad \text{Ref. Additive formulae of trigonometry} \end{aligned}$$

$$\begin{aligned} \therefore \cos z &= \cos (\ell \tilde{+} d) \times \cos (\theta \pm \Psi) = \cos \theta \cos \Psi \pm \sin \theta \sin \Psi \\ &\times \sin (\theta \pm \Psi) = \sin \theta \cos \Psi \pm \cos \theta \sin \Psi \\ \tan (\theta \pm \Psi) &= \frac{\tan \theta \pm \tan \psi}{1 \pm \tan \theta \tan \psi} \end{aligned}$$

In this case, zenith distance is meridian zenith distance (Z_m), So $Z = Z_m$.

$$\underline{Z_m = \ell + d}$$

When a celestial body transits lower branch, "h" should be 12^h (180°), so

$$\sin a = \sin \ell \cos p + \cos \ell \sin p \underbrace{\cos 180^\circ}_{\downarrow} \quad (P : \text{Polar distance})$$

$$= \sin \ell \cos p + \cos \ell \sin p \times (-1)$$

$$= \sin \ell \cos p - \cos \ell \sin p \quad \text{Refer additive formulae of trigonometry.}$$

$$= \sin (\ell - p)$$

$$\sin a = \sin (\ell - p)$$

$$\therefore a = \ell - p$$

In this case, the altitude (a) is meridian altitude (a_m) so $a = a_m$. then

$$\underline{a_m = \ell - p}$$

If we know the meridian zenith distance (Z_m) or meridian altitude (a_m) and declination of a celestial body, by the formulae both $Z_m = \ell + d$ and $a_m = \ell - p$, a latitude line of observer is obtainable as shown in Fig. 28.

Transit	d and Zm	Latitude	Name of latitude
Upper branch	d same name as Zm	$l = Zm + d$	Same name as d or Zm
	d contrary name to Zm	$d > Zm$	Same name as bigger value of d or Zm
		$d < Zm$	
Lower branch		$l = am + P$	Same name as d

Attention

About name of Zm (N or S).

N → Direction of Zm from celestial body is north.

S → Direction of Zm from celestial body is south.

Ref. A) lat & dec same names,
lat > dec
Latitude = $Zm + \hat{d}ec$.

B) 1. lat & dec same names,
lat < dec

2. lat & dec contrary names,
Latitude = $Zm \sim dec$.

Fig. 28

* Compare fixed lat. with D.R. lat..

Example 8

Find the Japan Standard Time of upper branch transit of the sun in longitude $141^{\circ} 20'E$, 10 June 1956.

At this standard time, a navigator observed the southerly meridian altitude (or apparent maximum altitude) of the sun's lower limb (\ominus) as $75^{\circ} - 12!2$.

What was the latitude at the time when he observed the sun?

where : Index error (I.E.) $\ominus 5!5$, Height of eye (H.E.) 8 metres
Air temperature was $3^{\circ}C$ warmer than the sea water temperature.

Solution

L.A.T. 10 June 1956 $12^h - 00^m - 00^s$

L. in T. ($141^{\circ} - 20'E$) $9 - 25 - 20 \ominus \leftarrow 141^{\circ} - 21'$ (see Fig. 20)

G.A.T. 10 June 1956 $2 - 34 - 40$

E.T. $0 - 46 \ominus \leftarrow E.T. = E_{\ominus} - 12$
(see Fig. 25)
 $= (12^h - 00^m - 46^s$
 $- 12 \text{ (MT = AT - ET)})$

U $2^h - 33^m - 54^s \rightarrow d = 23^{\circ} - 00' .2N$
(see Fig. 29)

L. in T. ($135^{\circ}E$, JAPAN) $9 - 00 - 00 \oplus$

J.S.T. $11^h - 33^m - 54^s$

$$\begin{aligned} \text{Ref. : } E_{\ominus} &= -12^h + E.T. + (24h) \\ E_{\oplus} &= R - R.A. + (24h) \\ E_p &= R - R.A.P. + (24h) \\ E_* &= R - R.A.* + (24h) \\ R &= -12^h + R.A.M.S. \\ &+ (24h) \end{aligned}$$

$$S = 24^h - R.A.*$$

$$h_G = U + E$$

$$h_{G\odot} = U + E_{\odot}$$

$$h_{G\bullet} = U + E_{\bullet}$$

$$h_{G^P} = U + E_P$$

$$h_{G^*} = U + E^*$$

$$h = h_{G\pm L} \begin{cases} \text{Long. E } \oplus \\ \text{Long. W } \ominus \end{cases}$$

Altitude correction

Sex. alt. \odot		75° - 12'.2
I, E	\ominus	5.5
Obs. alt. \odot		75° - 06'.7
Corr. 1	\oplus	10.5 (see Fig. 30)
		75° - 17'.2
Corr. 2		0.0 (see Fig. 30)
		75° - 17'.2
Corr. temp.	\oplus	0.6 (see Fig. 30)
True Alt. \odot		75° - 17'.8
		90 - 00.0 \ominus
Zm		14° - 42'.2N
d		23 - 00.2N \oplus
l		37° - 42'.4N

Ans. Time of transit = JST 11^h 33^m 54^s (10 June 1956)
 Latitude = 37° - 42'.4N.

Problem

On 4 August 1956, a navigator observed the northerly altitude of the sun's lower limb when it transited the upper branch in longitude 7°15'W. as 66°05'.5. When index error was \oplus 2'.4, height of eye 12 metres, air temperature 25°C, sea water temperature 24°C, What was his latitude?

4 August 1956 Lunar Age 26.8
Nautical Almanac

☉ Sun					Planet					☾ Moon							
U	E ₀	d	d	P.P.	U	E _p	d	P.P.	Tr.	h	m	s	U	E _c	d	E _c	d
h h m s 0 11 53 59 N17 18.9 0 0 0.0 2 53 59 17.5 10 1 4 54 0 16.2 20 2 6 0 14.9 30 3 8 0 13.5 40 4 10 1 12.2 50 5 12 11 54 1 N17 10.9 1 0 0.7 14 2 9.5 10 8 16 2 8.2 20 0.9 18 3 6.9 30 1.0 20 3 5.5 40 1 22 4 4.2 1 50 2 24 11 54 4 N17 2.8 2 0 1.3 (S.D. 15 48)					♀ Venus Tr. h m s 0 14 51 12 N18 29.0 0 0 0 0.0 2 19 29.2 10 1 0 4 25 29.5 20 1 1 6 32 29.8 30 2 1 8 39 30.1 40 2 1 10 45 30.4 0 50 3 1 12 14 51 52 N18 30.7 1 0 4 0.2 14 51 59 30.9 10 4 2 16 52 5 31.2 20 5 2 18 11 31.5 30 5 2 20 18 31.8 40 6 3 22 24 32.1 1 50 6 3 24 14 52 30 N18 32.3 2 0 7 0.3					h h m s 0 14 22 31 N20 42.0 1 21 17 40.6 2 20 3 38.2 3 18 49 35.8 4 17 35 33.4 5 16 20 30.9 6 15 6 28.4 7 13 52 25.8 8 12 38 23.2 9 11 24 20.6 10 10 10 17.9 11 8 56 15.2 12 30 1 13 32 2 14 35 3 15 37 4 16 39 4 17 42 5 18 44 6 19 47 7 20 49 8 21 52 1.0 22 54 2.0 23 57 1 24 59 2 25 52 3 26 44 3 27 37 4 28 30 5 29 22 6 30 14 7 (H.P.60.8, S.D.16 34) 6 14 7 42 N20 12.5 7 6 28 9.7 8 5 14 6.9 9 4 0 4.0 10 2 46 20 1.1 11 32 19 58.2 12 0 18 55.2 13 59 4 52.2 14 57 50 49.1 15 56 36 46.1 16 55 22 42.9 17 54 8 39.8 18 53 5 19 52 6 20 51 7 21 50 8 22 49 9 23 48 10 24 47 11 25 46 12 26 45 13 27 44 14 28 43 15 29 42 16 30 41 17 (H.P.60.9, S.D.16 36) 12 13 52 55 N19 36.6 13 51 41 33.4 14 50 27 30.1 15 49 13 26.8 16 48 0 23.5 17 46 46 20.1 18 45 32 16.7 19 44 19 13.2 20 43 5 9.7 21 41 52 6.2 22 40 38 2.7 23 39 25 18 59.1 24 38 11 25 36 58 26 35 45 27 34 31 28 33 18 29 32 5 30 30 52 31 29 39 32 28 25 33 27 12 34 25 59 35 24 46 36 23 33 37 22 19 38 21 5 39 20 50 40 19 36 41 18 22 42 17 8 43 16 5 44 15 51 45 14 37 46 13 23 47 12 9 48 11 5 49 10 42 50 9 28 51 8 14 52 7 0 53 5 48 54 4 34 55 3 20 56 2 6 57 1 52 58 0 38 59 0 24 60 0 10 (H.P.61.0, S.D.16 38) 18 13 39 11 N18 55.5 19 36 58 51.8 20 35 45 48.1 21 34 31 44.4 22 33 18 40.6 23 32 5 36.8 24 30 52 33.0 25 29 39 29.1 26 28 25 25.2 27 27 12 21.3 28 25 59 17.3 29 24 46 13.3 30 23 33 9.3 31 22 19 32 21 5 33 20 50 34 19 36 35 18 22 36 17 8 37 16 5 38 15 51 39 14 37 40 13 23 41 12 9 42 11 5 43 10 42 44 9 28 45 8 14 46 7 0 47 6 58 48 5 44 49 4 30 50 3 16 51 2 2 52 1 50 53 0 36 54 0 22 55 0 8 56 0 0 57 0 0 58 0 0 59 0 0 60 0 0 (H.P.61.1, S.D.16 39) Planet R.A. d Mag. H.P. S.D. ♀ 5 59 N18 29 -4.2 0.5 17 ♂ 23 45 S 7 50 -1.9 0.3 10 ♃ 10 30 N10 27 -1.3 0.0 15 ♄ 15 37 S17 21 +0.7 0.0 8 ♀ 9 58 N13 52 -0.5 0.1 3							
U=0h No. Star E _s d 1 Polaris 18 56 9 N89 3.4 2 Kochab 5 59 20 74 20.3 3 Dubhe 9 49 6 61 59.2 4 β Cassiop. 20 43 14 58 54.6 5 Merak 9 50 55 56 37.0 6 Alioth 7 58 1 N56 11.9 7 Schedir 20 12 4 56 17.9 8 Mizar 7 27 57 55 9.3 9 α Persei 17 28 54 49 42.3 10 Benetnasch 7 4 18 49 32.0 11 Capella 15 36 39 N45 57.2 12 Deneb 0 10 8 45 7.6 13 Vega 2 14 38 38 44.8 14 Castor 13 18 18 31 59.1 15 Alpheratz 20 43 58 28 51.1 16 Pollux 13 7 29 N28 7.9 17 α Cor. Bor. 5 17 16 26 51.8 18 Arcturus 6 36 26 19 24.6 19 Aldebaran 16 16 42 16 25.4 20 Markab 21 47 30 14 58.4 21 Denebola 9 3 17 N14 48.9 22 α Ophiuchi 3 17 11 12 35.6 23 Regulus 10 44 4 12 10.8 24 Altair 1 1 26 8 45.4 25 Betelgeuse 14 57 19 7 24.0 26 Bellatrix 15 27 20 N 6 18.7 27 Procyon 13 13 6 N 5 29.2 28 Rigel 15 37 41 S 8 14.9 29 α Hydrae 11 24 41 8 28.2 30 Spica 7 27 13 10 56.2 31 Sirius 14 6 54 S16 39.3 32 β Ceti 20 8 42 18 13.2 33 Antares 4 23 22 26 20.8 34 α Seginiani 1 57 31 26 21.0 35 Fomalhaut 21 54 50 29 59.9 36 λ Scorpii 3 19 26 S37 4.5 37 Canopus 14 27 10 52 40.2 38 α Pavonis 0 27 51 56 52.4 39 Achernar 19 14 1 57 27.0 40 β Crucis 8 4 57 59 27.4 41 β Centauri 6 49 22 S60 10.2 42 α Centauri 6 13 28 60 38.8 43 α Crucis 8 25 57 62 51.8 44 α Tri. Aust. 4 6 1 68 57.3 45 β Carinae 11 37 27 S69 32.4 R ₀ 20 50 8					♂ Mars Tr. h m s 0 21 5 32 S 7 49.6 0 0 0 0.0 2 5 50 49.6 10 2 0 4 6 7 49.7 20 3 0 6 25 49.7 30 5 0 8 6 43 49.7 40 6 0 10 7 1 49.7 0 50 8 0 12 21 7 18 S 7 49.7 1 0 9 0.0 14 36 49.8 10 11 0 16 7 54 49.8 20 12 0 18 0 12 49.8 30 14 0 20 30 49.9 40 15 0 22 8 48 49.9 1 50 17 0 24 21 9 6 S 7 49.9 2 0 18 0.0					♃ Jupiter Tr. h m s 0 10 20 7 N10 27.5 0 0 0 0.0 2 23 27.1 10 1 0 4 38 26.7 20 3 1 6 20 54 26.3 30 4 1 8 21 10 26.0 40 5 1 10 26 25.6 0 50 7 2 12 10 21 42 N10 25.2 1 0 8 0.2 14 21 57 24.8 10 9 2 16 22 13 24.4 20 11 3 18 29 24.0 30 12 3 20 22 45 23.7 40 13 3 22 23 1 23.3 1 50 15 4 24 10 23 16 N10 22.9 2 0 16 0.4							
♄ Saturn Tr. h m s 0 5 12 42 S17 20.9 0 0 0 0.0 2 13 2 21.0 10 2 0 4 22 21.0 20 3 0 6 13 41 21.0 30 5 0 8 14 1 21.0 40 7 0 10 20 21.1 0 50 8 0 12 5 14 40 S17 21.1 1 0 10 0.0 14 15 0 21.1 10 12 0 16 19 21.2 20 13 0 18 39 21.2 30 15 0 20 15 58 21.2 40 17 0 22 16 18 21.3 1 50 18 0 24 5 16 37 S17 21.3 2 0 20 0.0																	

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Altitude Correction of Sun 6° ~ 90°

Alt. Obs.	Height of Eye (m)																	Alt. Obs.
	0	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17		
	(+)																	
6 0	7.5	4.3	3.8	3.4	3.0	2.7	2.3	2.0	1.7	1.4	1.2	0.9	0.7	0.4	0.2	0.0	6 0	
20	7.8	4.7	4.2	3.8	3.4	3.1	2.7	2.4	2.1	1.8	1.6	1.3	1.1	0.8	0.6	0.4	20	
40	8.2	5.1	4.6	4.2	3.8	3.4	3.1	2.8	2.5	2.2	1.9	1.7	1.4	1.2	1.0	0.8	40	
7 0	8.5	5.4	4.9	4.5	4.1	3.8	3.4	3.1	2.8	2.5	2.3	2.0	1.8	1.5	1.3	1.1	7 0	
20	8.8	5.7	5.2	4.8	4.4	4.1	3.7	3.4	3.1	2.9	2.6	2.3	2.1	1.8	1.6	1.4	20	
40	9.1	6.0	5.5	5.1	4.7	4.3	4.0	3.7	3.4	3.1	2.9	2.6	2.4	2.1	1.9	1.7	40	
8 0	9.4	6.3	5.8	5.4	5.0	4.6	4.3	4.0	3.7	3.4	3.1	2.9	2.6	2.4	2.2	2.0	8 0	
20	9.6	6.5	6.0	5.6	5.2	4.9	4.5	4.2	3.9	3.7	3.4	3.1	2.9	2.6	2.4	2.2	20	
40	9.8	6.7	6.2	5.8	5.4	5.1	4.8	4.4	4.1	3.9	3.6	3.4	3.1	2.9	2.7	2.4	40	
9 0	10.0	6.9	6.5	6.0	5.6	5.3	5.0	4.7	4.4	4.1	3.8	3.6	3.3	3.1	2.9	2.6	9 0	
20	10.2	7.1	6.7	6.2	5.8	5.5	5.2	4.9	4.6	4.3	4.0	3.8	3.5	3.3	3.1	2.8	20	
40	10.4	7.3	6.8	6.4	6.0	5.7	5.4	5.0	4.7	4.5	4.2	4.0	3.7	3.5	3.3	3.0	40	
10 0	10.6	7.5	7.0	6.6	6.2	5.9	5.5	5.2	4.9	4.7	4.4	4.1	3.9	3.7	3.4	3.2	10 0	
30	10.8	7.7	7.3	6.8	6.5	6.1	5.8	5.5	5.2	4.9	4.6	4.4	4.1	3.9	3.7	3.5	30	
11 0	11.1	8.0	7.5	7.1	6.7	6.3	6.0	5.7	5.4	5.1	4.9	4.6	4.4	4.1	3.9	3.7	11 0	
30	11.3	8.2	7.7	7.3	6.9	6.5	6.2	5.9	5.6	5.3	5.1	4.8	4.6	4.3	4.1	3.9	30	
12 0	11.5	8.4	7.9	7.5	7.1	6.7	6.4	6.1	5.8	5.5	5.3	5.0	4.8	4.5	4.3	4.1	12 0	
30	11.6	8.5	8.1	7.6	7.3	6.9	6.6	6.3	6.0	5.7	5.4	5.2	4.9	4.7	4.5	4.3	30	
13 0	11.8	8.7	8.2	7.8	7.4	7.1	6.7	6.4	6.1	5.9	5.6	5.4	5.1	4.9	4.7	4.4	13 0	
30	11.9	8.8	8.4	8.0	7.6	7.2	6.9	6.6	6.3	6.0	5.8	5.5	5.3	5.0	4.8	4.6	30	
14 0	12.1	9.0	8.5	8.1	7.7	7.4	7.0	6.7	6.4	6.2	5.9	5.7	5.4	5.2	4.9	4.7	14 0	
30	12.2	9.1	8.7	8.2	7.9	7.5	7.2	6.9	6.6	6.3	6.0	5.8	5.5	5.3	5.1	4.9	30	
15 0	12.3	9.3	8.8	8.4	8.0	7.6	7.3	7.0	6.7	6.4	6.2	5.9	5.7	5.4	5.2	5.0	15 0	
16 0	12.6	9.5	9.0	8.6	8.2	7.8	7.5	7.2	6.9	6.7	6.4	6.1	5.9	5.7	5.4	5.2	16 0	
17 0	12.8	9.7	9.2	8.8	8.4	8.1	7.7	7.4	7.1	6.9	6.6	6.4	6.1	5.9	5.6	5.4	17 0	
18 0	12.9	9.9	9.4	9.0	8.6	8.2	7.9	7.6	7.3	7.0	6.8	6.5	6.3	6.1	5.8	5.6	18 0	
19 0	13.1	10.0	9.6	9.1	8.7	8.4	8.1	7.8	7.5	7.2	6.9	6.7	6.4	6.2	6.0	5.8	19 0	
20 0	13.3	10.2	9.7	9.3	8.9	8.6	8.2	7.9	7.6	7.4	7.1	6.9	6.6	6.4	6.2	5.9	20 0	
22 0	13.5	10.4	10.0	9.5	9.1	8.8	8.5	8.2	7.9	7.6	7.3	7.1	6.8	6.6	6.4	6.2	22 0	
24 0	13.7	10.6	10.2	9.8	9.4	9.0	8.7	8.4	8.1	7.8	7.6	7.3	7.1	6.8	6.6	6.4	24 0	
26 0	13.9	10.8	10.4	9.9	9.6	9.2	8.9	8.6	8.3	8.0	7.8	7.5	7.3	7.0	6.8	6.6	26 0	
28 0	14.1	11.0	10.5	10.1	9.7	9.4	9.0	8.7	8.4	8.2	7.9	7.7	7.4	7.2	7.0	6.7	28 0	
30 0	14.2	11.1	10.7	10.2	9.9	9.5	9.2	8.9	8.6	8.3	8.1	7.8	7.6	7.3	7.1	6.9	30 0	
32 0	14.3	11.2	10.8	10.4	10.0	9.6	9.3	9.0	8.7	8.4	8.2	7.9	7.7	7.4	7.2	7.0	32 0	
34 0	14.4	11.4	10.9	10.5	10.1	9.7	9.4	9.1	8.8	8.5	8.3	8.0	7.8	7.6	7.3	7.1	34 0	
36 0	14.5	11.5	11.0	10.6	10.2	9.8	9.5	9.2	8.9	8.6	8.4	8.1	7.9	7.7	7.4	7.2	36 0	
38 0	14.6	11.5	11.1	10.7	10.3	9.9	9.6	9.3	9.0	8.7	8.5	8.2	8.0	7.7	7.5	7.3	38 0	
40 0	14.7	11.6	11.2	10.7	10.4	10.0	9.7	9.4	9.1	8.8	8.6	8.3	8.1	7.8	7.6	7.4	40 0	
45 0	14.9	11.8	11.3	10.9	10.5	10.2	9.9	9.6	9.3	9.0	8.7	8.5	8.2	8.0	7.8	7.6	45 0	
50 0	15.0	12.0	11.5	11.1	10.7	10.3	10.0	9.7	9.4	9.1	8.9	8.6	8.4	8.2	7.9	7.7	50 0	
55 0	15.2	12.1	11.6	11.2	10.8	10.5	10.1	9.8	9.5	9.3	9.0	8.8	8.5	8.3	8.1	7.8	55 0	
60 0	15.3	12.2	11.7	11.3	10.9	10.6	10.2	9.9	9.6	9.4	9.1	8.9	8.6	8.4	8.2	7.9	60 0	
65 0	15.4	12.3	11.8	11.4	11.0	10.7	10.3	10.0	9.7	9.5	9.2	9.0	8.7	8.5	8.3	8.0	65 0	
70 0	15.4	12.4	11.9	11.5	11.1	10.7	10.4	10.1	9.8	9.6	9.3	9.0	8.8	8.6	8.3	8.1	70 0	
75 0	15.5	12.4	12.0	11.6	11.2	10.8	10.5	10.2	9.9	9.6	9.4	9.1	8.9	8.6	8.4	8.2	75 0	
80 0	15.6	12.5	12.1	11.6	11.3	10.9	10.6	10.3	10.0	9.7	9.5	9.2	9.0	8.7	8.5	8.3	80 0	
85 0	15.7	12.6	12.1	11.7	11.3	11.0	10.7	10.3	10.1	9.8	9.5	9.3	9.0	8.8	8.6	8.4	85 0	
90 0	15.8	12.7	12.2	11.8	11.4	11.0	10.7	10.4	10.1	9.9	9.6	9.3	9.1	8.9	8.6	8.4	90 0	
Dip.	0.0	3.1	3.6	4.0	4.4	4.7	5.0	5.3	5.6	5.9	6.2	6.4	6.6	6.9	7.1	7.3		
H.P. dist.	0.0	3.6	4.1	4.6	5.1	5.5	5.9	6.2	6.6	6.9	7.2	7.5	7.8	8.0	8.3	8.5		

Corr. for S. D.	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.
	Lower ☉	+ 0.5	+ 0.5	+ 0.4	+ 0.2	+ 0.1	0.0	0.0	+ 0.1	+ 0.2	+ 0.3	+ 0.5
Upper ☉	- 32.0	- 32.0	- 31.9	- 31.7	- 31.6	- 31.5	- 31.5	- 31.6	- 31.7	- 31.8	- 32.0	- 32.0

Diff. of temp. between Air and sea water	(°C)	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
	Corr.	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8

when Air temp. > Sea water temp. ⊕ ; Air temp. → at height of eye.
 Air temp. < Sea water temp. ⊖

Fig. 30

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY JAPAN.

Method of inverse operation for meridian altitude

Differentiation of the formula $Z_m = \ell \mp d$ is

$$\Delta Z_m = \Delta \ell \mp \Delta d$$

and declination (d) is constant for very short time,
then $|\Delta Z_m| = |\Delta \ell|$ because of $\Delta d = 0$.

The formula $|\Delta Z_m| = |\Delta \ell|$ shows that if two navigators who are on the same meridian and different latitudes observe meridian zenith distance (Z_m) at the same time, the difference $|\Delta Z_m|$ between two navigators is equal to the difference of latitude $|\Delta \ell|$.

So before observing meridian altitude, if you set up D.R. latitude (ℓD) and declination (d) of the celestial body when it transits the upper branch, you can have the following formula,

$$(Am)_c = 90^\circ - (\ell D \mp d)$$

$(Am)_c$ = Calculated (assumed) meridian altitude

ℓD = latitude by dead reckoning

By above mentioned formula, you compute Calculated meridian altitude {Cal. meri. alt. $\iff (Am)_c$ } beforehand. Next procedure is that you observe Meridian True Altitude {Meri. True Alt. $\iff (Am)_t$ } by sextant, so you can know

$$\Delta Am = (Am)_c - (Am)_t$$

According to $|\Delta Am| = |\Delta \ell|$, you can calculate the latitude as shown below,

$$\ell = \ell D \pm |\Delta \ell|$$

Note

Name of $\Delta \ell$, When $(Am)_t > (Am)_c$ same name as observed direction.

$(Am)_t < (Am)_c$ contrary name to observed direction.

Actual procedure of calculation on board ship is that inverse name of altitude corrections and index error of sextant should add to $(Am)_c$ and subtract it from meridian sextant altitude {Meri. Sex. Alt. $\implies (Am)_s$ }, then you can have $|\Delta Am|$.

Note

In case of upper branch transit

name of $|\Delta \ell|$; when $(Am)_s > (Am)_c'$, same name as observed direction.

$(Am)_s < (Am)_c'$, contrary name to observed direction.

$$\ast (Am)_c' = (Am)_c + (\text{inverse altitude correction})$$

when you observe lower branch transit, the formula

$$Am = \ell - P$$

can give latitude,

and

$$Am = \ell - P$$



$$Am = \Delta \ell - P$$

when polar distance (P) is constant,

$$|\Delta Am| = |\Delta \ell|$$

By $|\Delta Am| = |\Delta \ell|$, you also calculate latitude.

Note

In the case of lower branch transit

name of $|\Delta \ell|$; when $(Am)_s > (Am)_c'$, same name as declination.

$(Am)_s < (Am)_c'$, contrary to declination.

Example 9

Calculate the time of the sun's upper branch transit by using ship's chronometer (Universal time $3^h 30^m$) on 22 October 1956 in D.R.P. $08^{\circ}20'N$, $56^{\circ}40'W$. and at local apparent noon, a

navigator observed apparent maximum altitude of the sun's lower limb as $70^{\circ}16'.6$. What is latitude? Calculate by the method of inverse operation for meridian altitude.

where: Index error $\theta 0'.5$, Height of eye 14 metres,
Air temperature 28°C , Sea water temperature 25°C .

Solution (see Fig. 31)

L.A.T.	22 Oct. 1956	$12^{\text{h}} - 00^{\text{m}} - 00^{\text{s}}$	
L. in T.		$3 - 46 - 40$	\oplus
G.A.T.	22 Oct. 1956	$15^{\text{h}} - 46^{\text{m}} - 40^{\text{s}}$	
E.T.		$\oplus 15 - 32$	\ominus
U.	22 Oct. 1956	$15^{\text{h}} - 31^{\text{m}} - 08^{\text{s}}$	$d = 11^{\circ} - 11'.8 \text{ S}$
L. in T.		$3 - 30 - 00$	\ominus
Ship's T.	22 Oct. 1956	$12^{\text{h}} - 01^{\text{m}} - 08^{\text{s}}$	
ℓD		$8^{\circ} - 20'.0 \text{ N}$	
d		$11 - 11.8 \text{ S}$	\oplus
(Zm)c		$19 - 31.8$	
		$90 - 00.0$	\ominus
(Am)c		$70^{\circ} - 28'.2$	
Corr. 1		8.8	\ominus
		$70^{\circ} - 19'.4$	
Corr. 2		0.3	\ominus
		$70^{\circ} - 19'.1$	
Corr. t		0.6	\ominus
		$70^{\circ} - 18'.5$	
I.E.		0.5	\oplus
(Am)c'		$70^{\circ} - 19'.0$	
(Am)s		$70^{\circ} - 16.6$	\ominus
$\Delta \text{Am} = \Delta \ell$		2.4 N.	
ℓD		$8^{\circ} - 20.0$	\oplus
ℓ		$8^{\circ} - 22'.4 \text{ N}$	

Ans. Transit time $12^{\text{h}} - 01^{\text{m}} - 08^{\text{s}}$

lat. = $8^{\circ} - 22'.4 \text{ N}$

22 October 1956

Age 17.8

☉ Sun					Planet					☾ Moon																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
U	E ₂	d	d'	P.P.	U	E _p	d	P.P.	U	E _c	d	P.P.	U	E _c	d																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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<tr><td></td><td></td><td></td><td></td><td>0</td></tr> <tr><td></td><td></td><td></td><td></td><td>1.6</td></tr> <tr><td></td><td></td><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td><td></td><td>S.D. 16 6)</td></tr> </table>					h	m	s	o	z	0	12	15	26	S 10	2				10	4				11	6				3.3	8				5.1	10				6.8	12	12	15	30	S 11	14				8.6	16				10	18				12.1	20				13.9	22				15.7	24	12	15	35	S 11					19.2					2					0					1.6										S.D. 16 6)	<table border="1"> <tr><th>♀ Venus</th><th>♂ Mars</th><th>♃ Jupiter</th><th>♄ Saturn</th></tr> <tr><td colspan="4">Tr. h m 9 17</td></tr> <tr><td>0 14 42 44</td><td>N 5 36.3</td><td>0 0 0 0.0</td><td>0 0 0 0.0</td></tr> <tr><td>2 42</td><td>34.2</td><td>10 0 2</td><td></td></tr> <tr><td>4 40</td><td>32.1</td><td>20 0 4</td><td></td></tr> <tr><td>6 37</td><td>30.1</td><td>30 1 5</td><td></td></tr> <tr><td>8 35</td><td>28.0</td><td>40 1 7</td><td></td></tr> <tr><td>10 32</td><td>25.9</td><td>0 50 1 0.9</td><td></td></tr> <tr><td>12 14 42 30</td><td>N 5 23.8</td><td>1 0 1 1.1</td><td></td></tr> <tr><td>14 27</td><td>21.7</td><td>10 1 2</td><td></td></tr> <tr><td>16 25</td><td>19.6</td><td>20 1 4</td><td></td></tr> <tr><td>18 23</td><td>17.5</td><td>30 2 6</td><td></td></tr> <tr><td>20 20</td><td>15.5</td><td>40 2 8</td><td></td></tr> <tr><td>22 18</td><td>13.4</td><td>1 50 2 1.9</td><td></td></tr> <tr><td>24 14 42 15</td><td>N 5 11.3</td><td>2 0 2 2.1</td><td></td></tr> </table>					♀ Venus	♂ Mars	♃ Jupiter	♄ Saturn	Tr. h m 9 17				0 14 42 44	N 5 36.3	0 0 0 0.0	0 0 0 0.0	2 42	34.2	10 0 2		4 40	32.1	20 0 4		6 37	30.1	30 1 5		8 35	28.0	40 1 7		10 32	25.9	0 50 1 0.9		12 14 42 30	N 5 23.8	1 0 1 1.1		14 27	21.7	10 1 2		16 25	19.6	20 1 4		18 23	17.5	30 2 6		20 20	15.5	40 2 8		22 18	13.4	1 50 2 1.9		24 14 42 15	N 5 11.3	2 0 2 2.1		<table border="1"> <tr><th>♋♌♍♎♏♐♑♒♓</th></tr> <tr><td>0 22 23 28</td><td>N 19 40.2</td><td>1 2 0.1</td><td></td><td></td></tr> <tr><td>2 22 21</td><td>42.6</td><td>2 5 1</td><td></td><td></td></tr> 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26 Bellatrix	20 38 45	N 6 18.8																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
27 Procyon	18 24 32	N 5 20.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
28 Rigel	20 49 6	S 8 14.9																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
29 α Hydrae	16 36 7	8 29.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
30 Spica	12 39 41	10 56.1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
31 Sirius	19 18 20	S 16 39.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
32 β Ceti	1 20 8	18 13.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
33 Antares	9 34 50	26 20.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
34 α Sagittarii	7 9 0	26 21.1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
35 Fomalhaut	3 6 18	29 51.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
36 λ Scorpii	8 30 55	S 37 4.5																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
37 Canopus	19 33 35	52 40.1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
38 α Pavonis	5 39 20	56 52.6																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
39 Achernar	0 25 27	57 27.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
40 β Crucis	13 16 26	59 27.1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
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43 α Crucis	13 37 26	62 51.5																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
44 α Tri. Aust.	9 17 32	68 57.2																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
45 β Carinae	16 48 52	S 69 32.1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
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Planet	R.A.	d	Mag.	H.P.	S.D.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
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♂	23 6	S 9 0	-1.6	0.3	9																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
♃	11 32	N 4 8	-1.3	0.0	15																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
♄	15 59	S 18 42	+0.8	0.0	7																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
♅	12 56	S 3 54	-0.9	0.1	3																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															

Fig. 31

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Solution (Page 85)

Refer to Figs. 22, 23 and 24

Ship's T. 6 July 1956	06 ^h 50 ^m 00 ^s	
L. in T. (135° 00'E)	09	
G.D. 6 July 1956	21 ^h 50 ^m 00 ^s	←—————→
Chro. T.	22 ^h 21 ^m 50 ^s	(← 10h 21m 50s p.m.)
C.E.	29 26	⊖
U. 5 July 1956	21 ^h 52 ^m 24 ^s	
Ro (for 5 July 1956)→	18 51 51	← from the nautical almanac
P.P. E*	3 35	⊕ ← from Figure 27. (page 87)
	40 47 50	
	24	⊖
G. Sid. T.	16 ^h 47 ^m 50 ^s	
L. in T.	09	⊕
	25 47 50	
	24	⊖
L. Sid. T.	01 ^h 47 ^m 50 ^s	
	=====	

Data

Z - 57°E A = 50°2 ℓ = 34°28'N

		K		D		H			
Z	57°E	K ₁	264			H ₁	3187		
A	50°2	K ₂	3076 ⊕	D ₁	2884				
ℓ	⊕ 34°28'N	K ₃	3340						
K	⊕ 25°			D ₂	43	H ₂	2626		
ℓ + K	⊕ 59°28'N			D ₃	2933 ⊕	H ₃	288⊖		
				D ₄	5860	H ₄	6101	→ hE	= 3h28m00s
								L.Sid.T	= 1 47 50⊕
				d	46°N			→ R.A.	= 5h15m50s
					=====				=====

By the table positions of navigational stars (page 76) or the star map for the Northern hemisphere the name of the star should be Capella.

Ans. Capella

Solution (Page 92)

L.A.T.	4 Aug. 1956	12 ^h 00 ^m 00 ^s	
L. in T. (7°15'W)		<u>0 29 00</u>	⊕ (see page 80)
G.A.T.	4 Aug. 1956	12 ^h 29 ^m 00 ^s	
E.T.		<u>5 59</u>	⊖ → { E.T. = E ₀ + 12 ^h - (24h) } { see page , Ref. and } { nautical almanac }

d = 17° - 10!6N (From nautical almanac)

Note

How to calculate d.

In the nautical almanac for 4 Aug. 1956
d for Universal time 12h is N 17° - 10.9,
P.P. of d for 34m 59s = is 0.3 ⊖
17° - 10!6 N
=====

Sex. Alt.	⊙	66° - 05!5	
I.E		<u>2.4</u>	⊕
Abs. Alt.	⊙	66° - 07!9	
Corr. 1		<u>9.2</u>	⊕ (see page 94)
		66° - 17!1	
Corr. 2		<u>0.1</u>	⊕ (see page 94)
		66° - 17!2	
Corr. t.		<u>0.2</u>	⊕ (see page 94)
True Alt.	⊖	66° - 17!4	
		<u>90°</u>	⊖
		23° - 42!6 S	(Direction of zenith from the sun is south, see page 90)
d		<u>17° - 10!6 N</u>	⊖ (when d < Z _m , ℓ = Z _m ⊖ d, see page 90)
ℓ		6° - 32!0 S	(when d is contrary name to Z _m , the name of latitude should be the same as the name of the larger value. See page 90.)
Ans. Lat	=	<u>06° - 32!0 S</u>	

Determination of latitude by Polaris

The latitude of a location is equal to the altitude of the elevated pole as shown in figure 32.

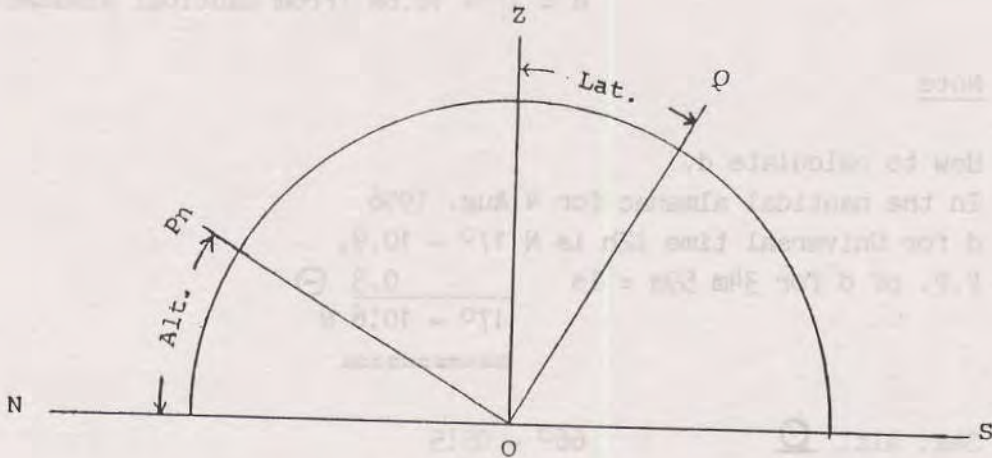


Fig. 32

Both the latitude of the observer (= QOZ) and the altitude of the pole (= NOPn) equals 90° minus $PnOZ$. If a star is located exactly at each celestial pole, the corrected altitude of the star should be equal to the observer's latitude.

Actually a star is not located at the north or south celestial poles, but Polaris is less than one degree from the north celestial pole. Polaris alternately transits the upper and lower branches of each celestial meridian in completing its diurnal circle. Twice during every 24 hours, as it moves in its diurnal circle, Polaris is at the same altitude as the celestial pole, and at that moment no correction would be required to its observed altitude to obtain latitude.

At all other times, a correction must be applied. The value for any instant may be obtained from Tables for Finding Latitude by Observing Polaris in the nautical almanac.

The corrections are tabulated in three tables, the first table is for "h" correction, the second table is for "altitude h" correction and the third table is for "Date h" correction.

So,

$$\text{Latitude} = (\text{Obs. true Alt.}) + (\text{table 1 correction}) \\ + (\text{table 2 correction}) + (\text{table 3 correction})$$

$$h = U + E^* \pm \text{Longitude in Time}$$

where; East longitude $\rightarrow \oplus$

West longitude $\rightarrow \ominus$

Example

At 04^h 20^m on 27 April 1956, a navigator observed the altitude of Polaris as 32° 19'8 in D.R.P. 32° 32'0 N, 133° 46'E. What was his latitude?

Where : Chronometer time when he observed Polaris was 7^h 24^m 18^s, chronometer error - 1^m 36^s, index error + 2.7, height of eye 15 metres, air temperature 13°C, sea water temperature 22°C

Solution

Ship's time 27 April 1956	04 ^h 20 ^m 00 ^s	\longleftrightarrow	28 ^h 20 ^m 00 ^s
L in T. (133° 46'E)	8 55 04	\ominus	(see fig. 20)
G.D.	26 April 1956		
(Greenwich Day)	19 ^h 24 ^m 56 ^s		
Chro. T.	26 April 1956	19 ^h 24 ^m 18 ^s	
C.E.		1 36	\ominus
U.	26 April 1956	19 ^h 22 ^m 42 ^s	

E* (U = 0h)	12 23 42	(see Fig. 35)
P.P. (E*)*	3 11	⊕ (see Fig. 27)
	31 49 35	
	24	⊖
h_G	07 ^h 49 ^m 35 ^s	
L. in T. (133°46'E)	08 55 04	
h	16 ^h 44 ^m 39 ^s	
Sex. Alt.*	32°- 19'8	
I.E.	2.7	⊕
Obs. Alt.	32°- 22'5	
Corr. 1	8.4	⊖ (see Fig. 32)
	32°- 14'1	
Corr. 2	1.8	⊖ (see Fig. 32. 13°C-22°C = -9°C)
True Alt. *	32°- 12'3	
Corr. I.	17.3	⊕ (see Fig. 38 Table 1)
	32°- 29'6	
Corr. II.	0.2	⊕ (see Fig. 39 Table 2)
	32°- 29'8	
Corr. III.	1.0	⊕ (see Fig. 39 Table 3)
	32°- 30.8 N	
<u>Ans. Lat. = 32° - 30'8 N</u>		

Where: Chronometer time when he observed Point was 7h 57m 15s
 chronometer error - 7h 55m, index error = 5.7', height of
 eye 15 metres, air temperature 17°C, sea water tempera-
 ture 22°C

Solution

Ship's time 27 April 1955	07 ^h 57 ^m 15 ^s
L. in T. (133° 46'E)	08 55 04
0.D.	0.0
(Greenwich Day)	
Obs. T. 28 April 1955	16 ^h 44 ^m 39 ^s
C.E.	2.7
U.	0.0

P* Altitude correction of star & planet

Obs. alt.	Height of eye (m)																	Obs. Alt.
	0	3	4	6	6	7	8	9	10	11	12	13	14	15	16	17		
	Subtract from Obs.alt. (-)																	
3 0	14.5	17.7	18.2	18.6	19.0	19.4	19.7	20.1	20.4	20.7	20.9	21.2	21.5	21.7	21.9	22.2	3 0	
4 0	13.5	16.7	17.2	17.6	18.0	18.4	18.7	19.0	19.3	19.6	19.9	20.2	20.4	20.7	20.9	21.1	4 0	
5 0	12.6	15.8	16.3	16.7	17.1	17.5	17.8	18.1	18.4	18.7	19.0	19.3	19.5	19.8	20.0	20.2	5 0	
6 0	11.8	15.0	15.5	15.9	16.3	16.7	17.0	17.3	17.6	17.9	18.2	18.4	18.7	18.9	19.2	19.4	6 0	
7 0	11.1	14.3	14.8	15.2	15.6	16.0	16.3	16.6	16.9	17.2	17.5	17.7	18.0	18.2	18.4	18.7	7 0	
8 0	10.5	13.6	14.1	14.5	14.9	15.3	15.6	16.0	16.3	16.6	16.8	17.1	17.3	17.6	17.8	18.0	8 0	
9 0	9.9	13.1	13.6	14.0	14.4	14.7	15.1	15.4	15.7	16.0	16.2	16.5	16.8	17.0	17.2	17.4	9 0	
10 0	9.4	12.5	13.0	13.5	13.8	14.2	14.5	14.9	15.1	15.4	15.7	15.9	16.2	16.4	16.7	16.9	10 0	
11 0	8.9	12.1	12.6	13.0	13.4	13.8	14.1	14.4	14.7	15.0	15.2	15.5	15.7	16.0	16.2	16.4	11 0	
12 0	8.5	11.6	12.1	12.6	12.9	13.3	13.6	13.9	14.2	14.5	14.8	15.0	15.3	15.5	15.8	16.0	12 0	
13 0	8.1	11.3	11.7	12.2	12.5	12.9	13.2	13.5	13.9	14.1	14.4	14.6	14.9	15.1	15.3	15.6	13 0	
14 0	7.8	10.9	11.4	11.8	12.2	12.5	12.9	13.2	13.5	13.7	14.0	14.3	14.5	14.8	15.0	15.2	14 0	
15 0	7.4	10.6	11.0	11.5	11.8	12.2	12.5	12.8	13.1	13.4	13.7	13.9	14.2	14.4	14.6	14.9	15 0	
16 0	7.1	10.3	10.7	11.2	11.5	11.9	12.2	12.5	12.8	13.1	13.4	13.6	13.9	14.1	14.3	14.5	16 0	
17 0	6.8	10.0	10.4	10.9	11.3	11.6	11.9	12.2	12.5	12.8	13.1	13.3	13.6	13.8	14.0	14.3	17 0	
18 0	6.6	9.7	10.2	10.6	11.0	11.3	11.7	12.0	12.3	12.6	12.8	13.1	13.3	13.5	13.8	14.0	18 0	
19 0	6.3	9.5	9.9	10.4	10.7	11.1	11.4	11.7	12.0	12.3	12.6	12.8	13.1	13.3	13.5	13.7	19 0	
20 0	6.1	9.2	9.7	10.1	10.5	10.9	11.2	11.5	11.8	12.1	12.3	12.6	12.8	13.1	13.3	13.5	20 0	
21 0	5.9	9.0	9.5	9.9	10.3	10.6	11.0	11.3	11.6	11.8	12.1	12.4	12.6	12.8	13.1	13.3	21 0	
22 0	5.7	8.8	9.3	9.7	10.1	10.5	10.8	11.1	11.4	11.7	11.9	12.2	12.4	12.7	12.9	13.1	22 0	
23 0	5.5	8.6	9.1	9.5	9.9	10.3	10.6	10.9	11.2	11.5	11.7	12.0	12.2	12.5	12.7	12.9	23 0	
24 0	5.3	8.4	8.9	9.3	9.7	10.1	10.4	10.7	11.0	11.3	11.6	11.8	12.0	12.3	12.5	12.7	24 0	
25 0	5.1	8.1	8.6	9.0	9.4	9.8	10.1	10.4	10.7	11.0	11.2	11.5	11.7	11.9	12.2	12.4	25 0	
26 0	4.8	7.9	8.4	8.8	9.2	9.5	9.9	10.2	10.5	10.7	11.0	11.2	11.5	11.7	11.9	12.2	26 0	
27 0	4.6	7.7	8.2	8.6	9.0	9.3	9.7	10.0	10.3	10.5	10.8	11.0	11.3	11.5	11.7	12.0	27 0	
28 0	4.4	7.5	8.0	8.4	8.8	9.1	9.5	9.8	10.1	10.3	10.6	10.8	11.1	11.3	11.5	11.8	28 0	
29 0	4.3	7.4	7.8	8.2	8.6	9.0	9.3	9.6	9.9	10.2	10.4	10.7	10.9	11.2	11.4	11.6	29 0	
30 0	4.1	7.2	7.7	8.1	8.5	8.8	9.1	9.4	9.7	10.0	10.3	10.5	10.8	11.0	11.2	11.4	30 0	
31 0	3.8	6.9	7.5	7.9	8.3	8.7	9.0	9.3	9.6	9.8	10.1	10.4	10.6	10.8	11.1	11.3	31 0	
32 0	3.7	6.8	7.2	7.7	8.0	8.4	8.7	9.0	9.3	9.6	9.8	10.1	10.3	10.6	10.8	11.0	32 0	
33 0	3.6	6.6	7.1	7.5	7.9	8.3	8.6	8.9	9.2	9.4	9.7	10.0	10.2	10.4	10.7	10.9	33 0	
34 0	3.3	6.4	6.9	7.3	7.7	8.0	8.4	8.7	9.0	9.2	9.5	9.7	10.0	10.2	10.4	10.7	34 0	
35 0	3.1	6.2	6.7	7.1	7.5	7.8	8.2	8.5	8.8	9.0	9.3	9.5	9.8	10.0	10.2	10.5	35 0	
36 0	3.0	6.0	6.5	6.9	7.3	7.7	8.0	8.3	8.6	8.9	9.1	9.4	9.6	9.8	10.1	10.3	36 0	
37 0	2.8	5.9	6.3	6.8	7.1	7.5	7.8	8.1	8.4	8.7	8.9	9.2	9.4	9.7	9.9	10.1	37 0	
38 0	2.6	5.7	6.2	6.6	7.0	7.3	7.7	8.0	8.3	8.5	8.8	9.0	9.3	9.5	9.7	10.0	38 0	
39 0	2.4	5.5	6.0	6.4	6.7	7.1	7.4	7.7	8.0	8.3	8.5	8.8	9.0	9.3	9.5	9.7	39 0	
40 0	2.2	5.2	5.7	6.1	6.5	6.9	7.2	7.5	7.8	8.1	8.3	8.6	8.8	9.0	9.3	9.5	40 0	
41 0	2.0	5.1	5.5	5.9	6.3	6.7	7.0	7.3	7.6	7.9	8.1	8.4	8.6	8.9	9.1	9.3	41 0	
42 0	1.8	4.9	5.4	5.8	6.2	6.5	6.8	7.1	7.4	7.7	8.0	8.2	8.5	8.7	8.9	9.1	42 0	
43 0	1.7	4.8	5.2	5.6	6.0	6.4	6.7	7.0	7.3	7.6	7.8	8.1	8.3	8.6	8.8	9.0	43 0	
44 0	1.5	4.6	5.1	5.5	5.9	6.2	6.6	6.9	7.2	7.4	7.7	7.9	8.2	8.4	8.6	8.9	44 0	
45 0	1.4	4.5	5.0	5.4	5.8	6.1	6.5	6.8	7.1	7.3	7.6	7.8	8.1	8.3	8.5	8.8	45 0	
46 0	1.3	4.4	4.9	5.3	5.7	6.0	6.4	6.7	7.0	7.2	7.5	7.7	8.0	8.2	8.4	8.7	46 0	
47 0	1.2	4.3	4.8	5.2	5.6	5.9	6.3	6.6	6.9	7.1	7.4	7.6	7.9	8.1	8.3	8.6	47 0	
48 0	1.2	4.2	4.7	5.1	5.5	5.9	6.2	6.5	6.8	7.0	7.3	7.6	7.8	8.0	8.3	8.5	48 0	
49 0	1.0	4.1	4.5	4.9	5.3	5.7	6.0	6.3	6.6	6.9	7.1	7.4	7.6	7.9	8.1	8.3	49 0	
50 0	0.8	3.9	4.4	4.8	5.2	5.5	5.8	6.1	6.4	6.7	7.0	7.2	7.5	7.7	7.9	8.1	50 0	
55 0	0.7	3.8	4.2	4.7	5.0	5.4	5.7	6.0	6.3	6.6	6.8	7.1	7.3	7.6	7.8	8.0	55 0	
60 0	0.6	3.6	4.1	4.5	4.9	5.3	5.6	5.9	6.2	6.5	6.7	7.0	7.2	7.4	7.7	7.9	60 0	
65 0	0.5	3.5	4.0	4.4	4.8	5.2	5.5	5.8	6.1	6.3	6.6	6.9	7.1	7.3	7.6	7.8	65 0	
70 0	0.4	3.4	3.9	4.3	4.7	5.1	5.4	5.7	6.0	6.2	6.5	6.8	7.0	7.2	7.5	7.7	70 0	
75 0	0.3	3.3	3.8	4.2	4.6	5.0	5.3	5.6	5.9	6.2	6.4	6.7	6.9	7.1	7.4	7.6	75 0	
80 0	0.2	3.3	3.7	4.1	4.5	4.9	5.2	5.5	5.8	6.1	6.3	6.6	6.8	7.1	7.3	7.5	80 0	
85 0	0.1	3.2	3.6	4.1	4.4	4.8	5.1	5.4	5.7	6.0	6.2	6.5	6.7	7.0	7.2	7.4	85 0	
90 0	0.0	3.1	3.6	4.0	4.4	4.7	5.0	5.3	5.6	5.9	6.2	6.4	6.7	6.9	7.1	7.3	90 0	

Planet only	2nd Corr..	add to Obs.alt.	Obs. Alt.	Subtract from							Obs. alt.	add to Obs.alt.
				0.1	0.2	0.3	0.4	0.5	0.6			
				10	0.1	0.2	0.3	0.4	0.5	0.6		
30	0.1	0.2	0.3	0.3	0.4	0.5	30					
50	0.1	0.1	0.2	0.2	0.3	0.4	50					
70	0.0	0.1	0.1	0.1	0.2	0.2	70					
90	0.0	0.0	0.0	0.0	0.0	0.0	90					

Diff. of temp. (°C)	Correction														
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
Correction	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8
Note	When: air temp. > sea water temp. ⊕ temp. at height of eye														
	air temp. < sea water temp. ⊖														

Fig. 33

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

P* Altitude correction of star & planet.

Obs. Alt.	Height of eye (m)																Obs. Alt.
	17	18	19	20	21	22	23	24	25	26	27	28	29	30	32	34	
	Subtract from Obs.alt. (-)																
30	22.2	22.4	22.6	22.8	23.0	23.2	23.4	23.6	23.8	24.0	24.2	24.4	24.5	24.7	25.1	25.4	25.7
20	21.1	21.4	21.6	21.8	22.0	22.2	22.4	22.6	22.8	23.0	23.1	23.3	23.5	23.7	24.0	24.3	24.6
40	19.4	19.6	19.8	20.0	20.2	20.4	20.6	20.8	21.0	21.2	21.4	21.6	21.7	21.9	22.2	22.5	22.9
20	18.7	18.9	19.1	19.3	19.5	19.7	19.9	20.1	20.3	20.5	20.6	20.8	21.0	21.2	21.5	21.8	22.1
40	18.0	18.2	18.4	18.6	18.9	19.0	19.2	19.4	19.6	19.8	20.0	20.2	20.3	20.5	20.8	21.1	21.5
60	17.4	17.7	17.9	18.1	18.3	18.5	18.7	18.9	19.0	19.2	19.4	19.6	19.7	19.9	20.2	20.6	20.9
20	16.9	17.1	17.3	17.5	17.7	17.9	18.1	18.3	18.5	18.7	18.8	19.0	19.2	19.4	19.7	20.0	20.3
40	16.4	16.6	16.9	17.1	17.3	17.5	17.7	17.9	18.0	18.2	18.4	18.5	18.7	18.9	19.2	19.5	19.8
60	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.4	17.6	17.8	17.9	18.1	18.3	18.4	18.8	19.1	19.4
20	15.6	15.8	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.3	17.5	17.7	17.9	18.0	18.4	18.7	19.0
40	15.2	15.4	15.6	15.8	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.3	17.5	17.7	18.0	18.3	18.6
70	14.9	15.1	15.3	15.5	15.7	15.9	16.1	16.3	16.5	16.6	16.8	17.0	17.1	17.3	17.6	18.0	18.3
20	14.5	14.8	15.0	15.2	15.4	15.6	15.8	16.0	16.1	16.3	16.5	16.7	16.8	17.0	17.3	17.6	17.9
40	14.3	14.5	14.7	14.9	15.1	15.3	15.5	15.7	15.9	16.0	16.2	16.4	16.5	16.7	17.0	17.4	17.7
80	14.0	14.2	14.4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	15.9	16.1	16.3	16.4	16.8	17.1	17.4
20	13.7	14.0	14.2	14.4	14.6	14.8	15.0	15.1	15.3	15.5	15.7	15.8	16.0	16.2	16.5	16.8	17.1
40	13.5	13.7	13.9	14.1	14.3	14.5	14.7	14.9	15.1	15.3	15.5	15.6	15.8	16.0	16.3	16.6	16.9
90	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.7	14.9	15.1	15.2	15.4	15.6	15.7	16.1	16.4	16.7
20	13.1	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.7	14.8	15.0	15.2	15.4	15.5	15.9	16.2	16.5
40	12.9	13.1	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.6	14.8	15.0	15.1	15.5	15.8	16.1	16.4
100	12.7	12.9	13.1	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.6	14.8	15.0	15.1	15.5	15.8	16.1
30	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	13.9	14.1	14.3	14.5	14.6	14.8	15.1	15.4	15.7
110	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.5	13.7	13.9	14.1	14.2	14.4	14.6	14.9	15.3	15.6
30	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.3	13.5	13.7	13.9	14.0	14.2	14.4	14.7	15.0	15.3
120	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.1	13.3	13.5	13.7	13.8	14.0	14.2	14.5	14.8	15.1
30	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.3	13.5	13.7	13.8	14.0	14.3	14.6	14.9
130	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.3	13.5	13.7	13.8	14.2	14.5	14.8
30	11.3	11.5	11.7	11.9	12.1	12.3	12.5	12.7	12.8	13.0	13.2	13.4	13.5	13.7	14.0	14.3	14.6
140	11.1	11.3	11.6	11.8	12.0	12.1	12.3	12.5	12.7	12.9	13.0	13.2	13.4	13.5	13.9	14.2	14.5
30	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.7	12.9	13.1	13.2	13.4	13.7	14.0	14.3
150	10.9	11.1	11.3	11.5	11.7	11.9	12.1	12.3	12.4	12.6	12.8	13.0	13.1	13.3	13.6	13.9	14.2
30	10.7	10.9	11.1	11.3	11.5	11.7	11.9	12.0	12.2	12.4	12.6	12.7	12.9	13.1	13.4	13.7	14.0
160	10.5	10.7	10.9	11.1	11.3	11.5	11.7	11.8	12.0	12.2	12.4	12.5	12.7	12.9	13.2	13.5	13.8
30	10.3	10.5	10.7	10.9	11.1	11.3	11.5	11.7	11.8	12.0	12.2	12.4	12.5	12.7	13.0	13.3	13.6
170	10.1	10.3	10.5	10.7	10.9	11.1	11.3	11.5	11.7	11.8	12.0	12.2	12.3	12.5	12.8	13.1	13.4
30	10.0	10.2	10.4	10.6	10.8	11.0	11.2	11.3	11.5	11.7	11.9	12.0	12.2	12.4	12.7	13.0	13.3
180	9.7	9.9	10.1	10.3	10.5	10.7	10.9	11.1	11.3	11.4	11.6	11.8	11.9	12.1	12.4	12.7	13.0
30	9.5	9.7	9.9	10.1	10.3	10.5	10.7	10.9	11.0	11.2	11.4	11.6	11.7	11.9	12.2	12.5	12.8
190	9.3	9.5	9.7	9.9	10.1	10.3	10.5	10.7	10.9	11.0	11.2	11.4	11.5	11.7	12.0	12.3	12.6
30	9.1	9.3	9.5	9.7	9.9	10.1	10.3	10.5	10.7	10.9	11.0	11.2	11.4	11.5	11.9	12.2	12.5
200	8.9	9.1	9.3	9.5	9.7	9.9	10.1	10.2	10.4	10.6	10.7	10.9	11.1	11.2	11.4	11.7	12.0
30	8.8	9.0	9.2	9.4	9.6	9.8	10.0	10.1	10.3	10.5	10.7	10.8	11.0	11.2	11.5	11.8	12.1
210	8.7	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.6	10.7	10.9	11.1	11.4	11.7	12.0
30	8.6	8.8	9.0	9.2	9.4	9.6	9.8	9.9	10.1	10.3	10.5	10.6	10.8	11.0	11.3	11.6	11.9
220	8.5	8.7	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.6	10.7	10.9	11.2	11.5	11.8
30	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.8	9.9	10.1	10.3	10.5	10.6	10.8	11.1	11.4	11.7
230	8.3	8.5	8.7	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.6	10.7	11.0	11.3	11.6
30	8.1	8.3	8.5	8.7	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.5	10.9	11.2	11.5
240	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.4	9.6	9.7	9.9	10.1	10.2	10.4	10.7	11.0	11.3
30	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.3	9.4	9.6	9.8	10.0	10.1	10.3	10.6	10.9	11.2
250	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.2	9.3	9.5	9.7	9.9	10.0	10.2	10.5	10.8	11.1
30	7.7	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.2	9.4	9.6	9.8	9.9	10.1	10.4	10.7	11.0
260	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.1	9.3	9.5	9.7	9.8	10.0	10.3	10.6	10.9
30	7.5	7.7	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.2	9.4	9.6	9.7	9.9	10.2	10.5	10.8
270	7.4	7.6	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.1	9.3	9.5	9.6	9.8	10.1	10.4	10.7
30	7.3	7.5	7.7	7.9	8.1	8.3	8.5	8.7	8.9	9.1	9.2	9.4	9.6	9.7	10.1	10.4	10.7

Planet only	2nd Corr. add to Obs.alt.	Obs. alt.	H.P. of Planet						Obs. alt.	add to Obs.alt.
			0.1	0.2	0.3	0.4	0.5	0.6		
		10	0.1	0.2	0.3	0.4	0.5	0.6	10	
		30	0.1	0.2	0.3	0.3	0.4	0.5	30	
		50	0.1	0.1	0.2	0.2	0.3	0.4	50	
		70	0.0	0.1	0.1	0.1	0.2	0.2	70	
		90	0.0	0.0	0.0	0.0	0.0	0.0	90	

Diff. of temp. (°C)	0'	1'	2'	3'	4'	5'	6'	7'	8'	9'	10'	11'	12'	13'	14'
Correction	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8

Note When: air temp. > sea water temp. ⊕ temp. at height of eye
 air temp. < sea water temp. ⊖

Fig. 34

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

26 April 1956 Lunar Age 14.9
Nautical Almanac

☉ Sun				Planet				☾ Moon Tr.			
U	E _s	d	P.P. of d	U	E _s	d	P.P. d	U	E _t	d	P.P. d
h m s				♀ Venus				h m s			
0 12 2 10	N13	26.2	0 0 0.0	Tr. 15 2				h m s			
2 11		27.8	10 1	h h m s	r	h m s	r	0 23 21 8	S18	40.9	1 2 0.1
4 11		29.4	20 3	0 8 57 40	N27	1.0	0 0 0.0	20 8		44.1	2 4 2
6 12		31.0	30 4	2 41		2.2	10 0 0	1 19 7		47.4	3 6 3
8 13		32.6	40 5	4 42		2.6	20 0 1	10 6		50.6	4 8 4
10 14		34.2	50 7	6 42		3.1	30 0 1	2 17 5		53.0	5 10 5
				8 43		3.5	40 0 1	3 15 4	10	55.9	6 12 6
12 12 2 15	N13	35.8	1 0 0.8	10 44		3.9	50 0 2	4 14 3		58.2	7 14 7
14 16		37.4	10 0.9	12 8 57 45	N27	4.3	1 0 1.0 2	4 13 2		6.3	8 16 8
16 16		39.0	20 1.1	14 45		4.7	10 1 2	12 1		9.3	9 18 0.9
18 17		40.6	30 2	16 46		5.1	20 1 3	5 11 -1		12.4	11 22 1
20 18		42.2	40 3	18 47		5.5	30 1 3	10 0		15.4	12 24 2
22 19		43.8	50 5	20 48		5.9	40 1 3	(H.P.55.9, S.D.15 13)			
24 12 2 20	N13	45.4	1 50 1.6	22 49		6.3	1 50 1 4	6 23 8 59	S19	10.3	16 33 6
				24 8 57 50	N27	6.7	2 0 1 0.4	7 58		21.3	17 35 7
								7 6 57		24.2	19 39 1.9
S.D. 15 55				♂ Mars				h m s			
				Tr. 6 23				8 4 55		30.0	20 41 2.0
No.	* Star	E _s	d	h h m s	r	h m s	r	9 2 54		32.8	22 45 2
1	Polaris	12 23 42	N09 3.6	0 17 36 48	S19	53.5	0 0 0 0.0	1 53		39.5	23 47 3
2	Kochab	23 25 0	74 19.9	2 36 51		52.9	10 1 1	10 23 0 52		41.2	24 49 4
3	Dubhe	3 14 47	61 59.3	4 37 1		52.2	20 1 1	22 59 51		44.0	25 51 5
4	Cassiopeia	14 9 3	58 54.4	6 8		51.5	30 2 2	11 58 50		46.7	26 53 6
5	Merak	3 16 37	56 37.1	8 14		50.9	40 2 2	57 49		49.4	27 55 7
6	Aliah	1 23 43	N56 11.0	10 21		50.2	0 50 3 3	(H.P.55.7, S.D.15 11)			
7	Schedir	13 37 52	56 17.8	12 17 37 21	S19	49.5	1 0 4 0.4	12 22 56 48	S19	52.1	29 59 2.9
8	Mizar	0 53 39	55 9.1	14 31		49.9	10 4 4	7 55 47		54.7	1 2 0.1
9	Persi	10 54 41	49 42.5	16 41		48.2	20 5 5	13 54 46		57.3	2 4 2
10	Benetnasch	0 30 1	49 31.0	18 47		47.5	30 5 5	53 45	19	59.9	3 6 2
11	Capella	9 2 25	N45 57.4	20 37 51		46.9	40 6 6	14 52 44	20	2.5	4 8 3
12	Deneb	17 35 55	45 7.2	22 30 1		46.2	1 50 6 6	51 43		5.0	5 10 4
13	Vega	19 40 23	30 44.3	24 17 30 7	H19	45.5	2 0 7 0.7	15 59 42		7.5	6 12 5
14	Castor	6 44 3	31 59.2	♂ Jupiter				49 40		10.0	7 14 6
15	Alpheratz	14 9 45	29 50.9	Tr. 19 10				16 48 33		12.5	8 16 6
16	Pollux	6 33 13	N20 8.0	h h m s		h m s	r	17 46 37		14.9	9 18 7
17	Cor. Bor.	22 43 0	26 51.5	0 4 38 30	N15	21.2	0 0 0 0.0	45 35		19.7	10 20 8
18	Arcturus	0 2 10	19 24.4	2 38 50		21.1	10 2 0	(H.P.55.6, S.D.15 9)			
19	Aldebaran	9 42 20	16 25.3	4 33 9		21.1	20 3 0	18 22 44 35	S20	22.0	12 24 1.0
20	Maikab	15 13 17	14 50.1	6 28		21.0	30 5 0	43 34		24.3	13 26 0
21	Denebola	2 29 0	N14 48.0	8 39 47		21.0	40 6 0	19 42 33		26.6	14 28 1
22	Ophiuchi	20 42 55	12 35.3	10 40 6		20.9	0 50 8 0	41 32		28.9	15 31 2
23	Regulus	4 9 43	12 10.7	12 4 40 26	N15	20.9	1 0 10 0.1	20 40 31		31.1	16 33 3
24	Alair	18 27 12	8 45.0	14 40 45		20.8	10 11 1	19 39 29		33.3	17 35 4
25	Betelgeuse	8 23 4	7 23.9	16 41 4		20.7	20 13 1	21 38 28		35.5	18 37 4
26	Bellatrix	8 53 5	N 6 10.6	18 23		20.7	30 14 1	37 27		37.7	19 39 5
27	Procyon	6 39 51	N 5 20.1	20 41 42		20.8	40 16 1	22 36 26		39.8	20 41 6
28	Rigel	9 3 26	8 8 15.2	22 42 2		20.6	1 50 17 1	35 25		41.9	21 43 7
29	Hydrae	4 50 25	0 20.4	24 4 42 21	N15	20.5	2 0 19 0.1	23 34 21		44.0	22 45 8
30	Spica	0 52 57	10 56.2	♄ Saturn				33 23		46.0	23 49 1.9
31	Sirius	7 32 39	S16 39.5	Tr. 1 42				24 22 32 21	S20	48.1	24 51 2.0
32	Ceti	13 34 29	10 13.5	h h m s		h m s	r	(H.P.55.5, S.D.15 7)			
33	Antares	21 49 6	26 20.2	0 22 17 25	S18	13.9	0 0 0 0.0	Planet			
34	Sagittarii	19 23 17	26 21.1	2 17 46		13.8	10 2 0	R.A.	d	Mag.	H.P. S.D.
35	Fomalhaut	15 20 38	29 51.1	4 18 7		13.8	20 4 0	♀	5 19 N27	2	-4.1 0.2 14
36	Scorpii	20 45 12	S37 4.3	6 28		13.7	30 5 0	♂	20 39 S19	54	+0.4 0.1 4
37	Canopus	7 52 54	52 40.6	8 18 49		13.6	40 7 0	♀	9 37 N15	21	-1.8 0.0 18
38	Pavonis	17 53 39	56 52.3	10 19 10		13.6	0 50 9 0	♂	15 50 S18	14	+0.3 0.0 8
39	Achernar	12 39 49	57 21.4	12 22 19 31	S18	13.5	1 0 11 0.1	♂	3 27 N21	11	-0.3 0.1 3
40	Cruceis	1 30 30	59 27.3	14 19 52		13.4	10 12 1				
41	Centauri	0 15 5	S60 9.8	16 20 13		13.4	20 14 1				
42	Centauri	23 39 11	60 39.5	18 34		13.3	30 16 1				
43	Cruceis	1 51 39	62 51.7	20 20 55		13.2	40 18 1				
44	Tri. Ausl.	21 31 46	69 56.9	22 21 16		13.2	1 50 19 1				
45	Carinae	5 3 7	S69 32.7	24 22 21 37	S18	13.1	2 0 21 0.1				

Fig. 35

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

TABLES FOR FINDING LATITUDE BY OBSERVING POLARIS (1956)
Table (1)

<i>m</i>	<i>h</i> 0	<i>h</i> 1	<i>h</i> 2	<i>h</i> 3	<i>h</i> 4	<i>h</i> 5	<i>h</i> 6	<i>h</i> 7	<i>h</i> 8	<i>h</i> 9	<i>h</i> 10	<i>h</i> 11
0	-57.4	-55.4	-49.8	-40.9	-29.2	-15.6	-1.0	+13.6	+27.2	+38.9	+47.8	+53.4
1	57.4	55.4	49.7	40.7	29.0	15.4	0.8	13.8	27.4	39.0	47.9	53.5
2	57.4	55.3	49.6	40.5	28.8	15.1	0.5	14.1	27.6	39.2	48.1	53.6
3	57.4	55.2	49.4	40.3	28.5	14.9	-0.3	14.3	27.8	39.4	48.2	53.6
4	57.3	55.2	49.3	40.2	28.3	14.6	0.0	14.5	28.0	39.5	48.3	53.7
5	-57.3	-55.1	-49.2	-40.0	-23.1	-14.4	+0.2	+14.8	+28.2	+39.7	+48.4	+53.8
6	57.3	55.0	49.1	39.8	27.9	14.2	0.5	15.0	28.5	39.9	48.5	53.8
7	57.3	55.0	48.9	39.6	27.7	13.9	0.7	15.3	28.7	40.1	48.6	53.9
8	57.3	54.9	48.8	39.4	27.5	13.7	1.0	15.5	28.9	40.2	48.8	53.9
9	57.3	54.8	48.7	39.3	27.2	13.4	1.2	15.7	29.1	40.4	48.9	54.0
10	-57.3	-54.8	-48.5	-39.1	-27.0	-13.2	+1.5	+15.0	+29.3	+40.6	+49.0	+54.0
11	57.3	54.7	48.4	38.9	26.8	13.0	1.7	15.2	29.5	40.7	49.1	54.1
12	57.3	54.6	48.3	38.7	26.6	12.7	1.9	15.4	29.7	40.9	49.2	54.1
13	57.3	54.5	48.1	38.5	26.4	12.5	2.2	15.7	29.9	41.0	49.3	54.2
14	57.3	54.5	48.0	38.3	26.2	12.2	2.4	15.9	30.1	41.2	49.5	54.2
15	-57.2	-54.4	-47.9	-38.2	-25.9	-12.0	+2.7	+17.2	+30.3	+41.4	+49.6	+54.3
16	57.2	54.3	47.7	38.0	25.7	11.8	2.9	17.4	30.5	41.5	49.7	54.3
17	57.2	54.2	47.6	37.8	25.5	11.5	3.2	17.6	30.7	41.7	49.8	54.4
18	57.2	54.1	47.4	37.6	25.3	11.3	3.4	17.8	30.9	41.9	49.9	54.4
19	57.2	54.0	47.3	37.4	25.0	11.0	3.7	18.0	31.1	42.0	50.0	54.5
20	-57.1	-54.0	-47.2	-37.2	-24.8	-10.8	+3.9	+18.3	+31.3	+42.2	+50.1	+54.5
21	57.1	53.9	47.0	37.0	24.6	10.6	4.1	18.5	31.5	42.3	50.2	54.5
22	57.1	53.8	46.9	36.9	24.4	10.3	4.4	18.7	31.7	42.5	50.3	54.6
23	57.1	53.7	46.7	36.7	24.1	10.1	4.5	19.0	31.9	42.6	50.4	54.6
24	57.0	53.6	46.6	36.5	23.9	9.8	4.9	19.2	32.1	42.8	50.5	54.7
25	-57.0	-53.5	-46.4	-36.3	-23.7	-9.6	+5.1	+19.4	+32.3	+42.9	+50.6	+54.7
26	57.0	53.4	46.3	36.1	23.5	9.3	5.4	19.7	32.5	43.1	50.7	54.7
27	56.9	53.4	46.2	35.9	23.2	9.1	5.6	19.9	32.7	43.3	50.8	54.8
28	56.9	53.3	46.0	35.7	23.0	8.8	5.9	20.1	32.9	43.4	50.9	54.8
29	56.9	53.2	45.9	35.5	22.8	8.6	6.1	20.3	33.1	43.6	51.0	54.8
30	-56.9	-53.1	-45.7	-35.3	-22.6	-8.4	+6.4	+20.6	+33.3	+43.7	+51.1	+54.9
31	56.8	53.0	45.6	35.1	22.3	8.1	6.6	20.8	33.5	43.9	51.2	54.9
32	56.8	52.9	45.4	34.9	22.1	7.9	6.8	21.0	33.7	44.0	51.3	54.9
33	56.8	52.8	45.3	34.7	21.9	7.6	7.1	21.2	33.9	44.2	51.4	54.9
34	56.7	52.7	45.1	34.5	21.7	7.4	7.3	21.5	34.1	44.3	51.4	55.0
35	-56.7	-52.6	-44.9	-34.3	-21.4	-7.1	+7.6	+21.7	+34.3	+44.4	+51.5	+55.0
36	56.7	52.5	44.8	34.1	21.2	6.9	7.8	21.9	34.5	44.6	51.6	55.0
37	56.6	52.4	44.6	33.9	21.0	6.6	8.1	22.1	34.7	44.7	51.7	55.1
38	56.6	52.3	44.5	33.7	20.7	6.4	8.3	22.4	34.9	44.9	51.8	55.1
39	56.5	52.2	44.3	33.5	20.5	6.1	8.6	22.6	35.0	45.0	51.9	55.1
40	-56.5	-52.1	-44.2	-33.3	-20.3	-5.9	+8.8	+22.8	+35.2	+45.2	+52.0	+55.1
41	56.5	52.0	44.0	33.1	20.0	5.7	9.0	23.0	35.4	45.3	52.0	55.2
42	56.4	51.9	43.9	32.9	19.8	5.4	9.3	23.3	35.6	45.4	52.1	55.2
43	56.4	51.8	43.7	32.7	19.6	5.2	9.5	23.5	35.8	45.6	52.2	55.2
44	56.3	51.7	43.5	32.5	19.4	4.9	9.8	23.7	36.0	45.7	52.3	55.2
45	-56.3	-51.6	-43.4	-32.3	-19.1	-4.7	+10.0	+23.9	+36.2	+45.9	+52.4	+55.2
46	56.2	51.5	43.2	32.1	18.9	4.4	10.2	24.2	36.3	46.0	52.5	55.3
47	56.2	51.3	43.0	31.9	18.7	4.2	10.5	24.4	36.5	46.1	52.5	55.3
48	56.1	51.2	42.9	31.7	18.4	3.9	10.7	24.6	36.7	46.3	52.6	55.3
49	56.1	51.1	42.7	31.5	18.2	3.7	11.0	24.8	36.9	46.4	52.7	55.3
50	-56.0	-51.0	-42.6	-31.3	-18.0	-3.5	+11.2	+25.0	+37.1	+46.5	+52.8	+55.3
51	56.0	50.9	42.4	31.1	17.7	3.2	11.4	25.2	37.3	46.7	52.8	55.3
52	55.9	50.8	42.2	30.9	17.5	3.0	11.7	25.5	37.4	46.8	52.9	55.3
53	55.9	50.6	42.1	30.7	17.3	2.7	11.9	25.7	37.6	46.9	53.0	55.3
54	55.8	50.5	41.9	30.5	17.0	2.5	12.2	25.9	37.8	47.1	53.0	55.3
55	-55.8	-50.4	-41.7	-30.2	-16.8	-2.2	+12.4	+26.1	+38.0	+47.2	+53.1	+55.3
56	55.7	50.3	41.5	30.0	16.5	2.0	12.6	26.3	38.2	47.3	53.2	55.3
57	55.6	50.2	41.4	29.8	16.3	1.7	12.9	26.5	38.3	47.4	53.2	55.4
58	55.6	50.1	41.2	29.6	16.1	1.5	13.1	26.8	38.5	47.6	53.3	55.4
59	55.5	49.9	41.0	29.4	15.8	1.3	13.4	27.0	38.7	47.7	53.4	55.4
60	-55.4	-49.8	-40.9	-29.2	-15.6	-1.0	+13.6	+27.2	+38.9	+47.8	+53.4	+55.4

Fig. 36

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

TABLES FOR FINDING LATITUDE BY OBSERVING POLARIS (1956)

Table (2)

Add always

Alt.					<i>h</i>				(hour angle)				<i>h</i> ₁₂
	<i>h</i> ₀	<i>h</i> ₁	<i>h</i> ₂	<i>h</i> ₃	<i>h</i> ₄	<i>h</i> ₅	<i>h</i> ₆	<i>h</i> ₇	<i>h</i> ₈	<i>h</i> ₉	<i>h</i> ₁₀	<i>h</i> ₁₁	
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0
20	0.0	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.0	0.0
25	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.0
30	0.0	0.0	0.1	0.1	0.2	0.2	0.3	0.3	0.3	0.2	0.1	0.1	0.0
35	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.3	0.3	0.2	0.2	0.1	0.0
40	0.0	0.0	0.1	0.2	0.3	0.4	0.4	0.4	0.4	0.3	0.2	0.1	0.0
45	0.0	0.0	0.1	0.2	0.3	0.4	0.5	0.4	0.4	0.3	0.2	0.1	0.0
50	0.0	0.0	0.1	0.3	0.4	0.5	0.5	0.5	0.5	0.4	0.3	0.1	0.0
55	0.0	0.0	0.2	0.3	0.5	0.6	0.7	0.6	0.6	0.5	0.3	0.2	0.0
60	0.0	0.1	0.2	0.4	0.6	0.7	0.8	0.7	0.7	0.6	0.4	0.2	0.1
65	0.0	0.1	0.2	0.5	0.7	0.9	1.0	0.9	0.9	0.7	0.5	0.2	0.1
70	0.0	0.1	0.3	0.6	1.0	1.2	1.3	1.2	1.2	1.0	0.6	0.3	0.1

Table (3)

Add always

Date M.D.					<i>h</i>				(hour angle)				<i>h</i> ₁₂
	<i>h</i> ₀	<i>h</i> ₁	<i>h</i> ₂	<i>h</i> ₃	<i>h</i> ₄	<i>h</i> ₅	<i>h</i> ₆	<i>h</i> ₇	<i>h</i> ₈	<i>h</i> ₉	<i>h</i> ₁₀	<i>h</i> ₁₁	
1 1	1.3	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.8	0.8	0.7
1 21	1.3	1.3	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.8	0.7	0.7
2 10	1.3	1.3	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.8	0.7	0.7
3 1	1.2	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.8	0.8	0.8
3 21	1.1	1.1	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	0.9	0.9
4 10	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4 30	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.1	1.1	1.1
5 20	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.1	1.1	1.1	1.2
6 9	0.8	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.2	1.2	1.2	1.2
6 29	0.7	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.2	1.2	1.2	1.3
7 19	0.7	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.2	1.2	1.2	1.3
8 8	0.8	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.2	1.2	1.2	1.2
8 28	0.8	0.9	0.9	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.1	1.1	1.2
9 17	0.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.1
10 7	1.1	1.1	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.9	0.9
11 27	1.2	1.2	1.2	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.8	0.8	0.8
12 16	1.3	1.3	1.3	1.2	1.2	1.1	1.0	0.9	0.8	0.8	0.7	0.7	0.7
12 6	1.4	1.4	1.4	1.3	1.2	1.1	1.0	0.9	0.8	0.7	0.6	0.6	0.6
12 26	1.5	1.5	1.4	1.4	1.2	1.1	1.0	0.9	0.8	0.6	0.6	0.5	0.5
46	1.5	1.5	1.5	1.4	1.3	1.1	1.0	0.9	0.7	0.6	0.5	0.5	0.5

Lat. = (Obs. true Alt.)+(Tab.1)+(Tab.2)+(Tab.3)

$$h = U + E* \pm L \text{ in T. } \left(\begin{array}{l} L \rightarrow \text{E. Long.} \rightarrow + \\ \rightarrow \text{W. Long.} \rightarrow - \end{array} \right)$$

Fig. 37

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

TABLES FOR FINDING LATITUDE BY OBSERVING POLARIS (1956)

Table (1)

<i>h</i>	^h 12	^h 13	^h 14	^h 15	^h 16	^h 17	^h 18	^h 19	^h 20	^h 21	^h 22	^h 23
0	+55.4	+53.4	+47.8	+39.9	+27.2	+13.6	- 1.0	-15.6	-29.2	-40.9	-49.0	-55.4
1	55.4	53.4	47.7	39.7	27.0	13.4	1.3	15.0	29.4	41.0	49.9	55.5
2	55.4	53.3	47.6	39.5	26.8	13.1	1.5	16.1	29.6	41.2	50.1	55.6
3	55.4	53.2	47.4	39.3	26.5	12.9	1.7	16.3	29.8	41.4	50.2	55.6
4	55.3	53.2	47.3	39.2	26.3	12.6	2.0	16.5	30.0	41.5	50.3	55.7
5	+55.3	+53.1	+47.2	+39.0	+26.1	+12.4	- 2.2	-16.0	-30.2	-41.7	-50.4	-55.8
6	55.3	53.0	47.1	37.8	25.9	12.2	2.5	17.0	30.5	41.9	50.5	55.8
7	55.3	53.0	46.9	37.6	25.7	11.9	2.7	17.3	30.7	42.1	50.6	55.9
8	55.3	52.9	46.8	37.4	25.5	11.7	3.0	17.5	30.9	42.2	50.8	55.9
9	55.3	52.8	46.7	37.3	25.2	11.4	3.2	17.7	31.1	42.4	50.9	56.0
10	+55.3	+52.8	+46.5	+37.1	+25.0	+11.2	- 3.5	-18.0	-31.3	-42.6	-51.0	-56.0
11	55.3	52.7	46.4	36.9	24.8	11.0	3.7	18.2	31.5	42.7	51.1	56.1
12	55.3	52.6	46.3	36.7	24.6	10.7	3.9	18.4	31.7	42.9	51.2	56.1
13	55.3	52.5	46.1	36.5	24.4	10.5	4.2	18.7	31.9	43.0	51.3	56.2
14	55.3	52.5	46.0	36.3	24.2	10.2	4.4	18.9	32.1	43.2	51.5	56.2
15	+55.2	+52.4	+45.9	+36.2	+23.9	+10.0	- 4.7	-19.1	-32.3	-43.4	-51.6	-56.3
16	55.2	52.3	45.7	36.0	23.7	9.8	4.9	19.4	32.5	43.5	51.7	56.3
17	55.2	52.2	45.6	35.8	23.5	9.5	5.2	19.6	32.7	43.7	51.8	56.4
18	55.2	52.1	45.4	35.6	23.3	9.3	5.4	19.8	32.9	43.9	51.9	56.4
19	55.2	52.0	45.3	35.4	23.0	9.0	5.7	20.0	33.1	44.0	52.0	56.5
20	+55.1	+52.0	+45.2	+35.2	+22.8	+ 8.8	- 5.9	-20.3	-33.3	-44.2	-52.1	-56.5
21	55.1	51.9	45.0	35.0	22.6	8.6	6.1	20.5	33.5	44.3	52.2	56.5
22	55.1	51.8	44.9	34.9	22.4	8.3	6.4	20.7	33.7	44.5	52.3	56.6
23	55.1	51.7	44.7	34.7	22.1	8.1	6.6	21.0	33.9	44.6	52.4	56.6
24	55.0	51.6	44.6	34.5	21.9	7.8	6.9	21.2	34.1	44.8	52.5	56.7
25	+55.0	+51.5	+44.4	+34.3	+21.7	+ 7.6	- 7.1	-21.4	-34.3	-44.9	-52.6	-56.7
26	55.0	51.4	44.3	34.1	21.5	7.3	7.4	21.7	34.5	45.1	52.7	56.7
27	54.9	51.4	44.2	33.9	21.2	7.1	7.6	21.9	34.7	45.3	52.8	56.8
28	54.9	51.3	44.0	33.7	21.0	6.8	7.9	22.1	34.9	45.4	52.9	56.8
29	54.9	51.2	43.9	33.5	20.8	6.6	8.1	22.3	35.1	45.6	53.0	56.8
30	+54.9	+51.1	+43.7	+33.3	+20.6	+ 6.4	- 8.4	-22.6	-35.3	-45.7	-53.1	-56.9
31	54.8	51.0	43.6	33.1	20.3	6.1	8.6	22.8	35.5	45.9	53.2	56.9
32	54.8	50.9	43.4	32.9	20.1	5.9	8.9	23.0	35.7	46.0	53.3	56.9
33	54.8	50.8	43.3	32.7	19.9	5.6	9.1	23.2	35.9	46.2	53.4	56.9
34	54.7	50.7	43.1	32.5	19.7	5.4	9.3	23.5	36.1	46.3	53.4	57.0
35	+54.7	+50.6	+42.9	+32.3	+19.4	+ 5.1	- 9.6	-23.7	-36.3	-46.4	-53.5	-57.0
36	54.7	50.5	42.8	32.1	19.2	4.9	9.8	23.9	36.5	46.6	53.6	57.0
37	54.6	50.4	42.6	31.9	19.0	4.6	10.1	24.1	36.7	46.7	53.7	57.1
38	54.6	50.3	42.5	31.7	18.7	4.4	10.3	24.4	36.9	46.9	53.8	57.1
39	54.5	50.2	42.3	31.5	18.5	4.1	10.6	24.6	37.0	47.0	53.9	57.1
40	+54.5	+50.1	+42.2	+31.3	+18.3	+ 3.9	-10.8	-24.8	-37.2	-47.2	-54.0	-57.1
41	54.5	50.0	42.0	31.1	18.0	3.7	11.0	25.0	37.4	47.3	54.0	57.2
42	54.4	49.9	41.9	30.9	17.8	3.4	11.3	25.3	37.6	47.4	54.1	57.2
43	54.4	49.8	41.7	30.7	17.6	3.2	11.5	25.5	37.8	47.6	54.2	57.2
44	54.3	49.7	41.5	30.5	17.4	2.9	11.8	25.7	38.0	47.7	54.3	57.2
45	+54.3	+49.6	+41.4	+30.3	+17.2	+ 2.7	-12.0	-25.9	-38.2	-47.9	-54.4	-57.2
46	54.2	49.5	41.2	30.1	16.9	2.4	12.2	26.2	38.3	48.0	54.5	57.3
47	54.2	49.3	41.0	29.9	16.7	2.2	12.5	26.4	38.5	48.1	54.5	57.3
48	54.1	49.2	40.9	29.7	16.4	1.9	12.7	26.6	38.7	48.3	54.6	57.3
49	54.1	49.1	40.7	29.5	16.2	1.7	13.0	26.8	38.9	48.4	54.7	57.3
50	+54.0	+49.0	+40.6	+29.3	+16.0	+ 1.5	-13.2	-27.0	-39.1	-48.5	-54.8	-57.3
51	54.0	48.9	40.4	29.1	15.7	1.2	13.4	27.2	39.3	48.7	54.8	57.3
52	53.9	48.8	40.2	28.9	15.5	1.0	13.7	27.5	39.4	48.8	54.9	57.3
53	53.9	48.6	40.1	28.7	15.3	0.7	13.9	27.7	39.6	48.9	55.0	57.3
54	53.8	48.5	39.9	28.5	15.0	0.5	14.2	27.9	39.8	49.1	55.0	57.3
55	+53.8	+48.4	+39.7	+28.2	+14.8	+ 0.2	-14.4	-28.1	-40.0	-49.2	-55.1	-57.3
56	53.7	48.3	39.5	28.0	14.5	0.0	14.6	28.3	40.2	49.3	55.2	57.3
57	53.6	48.2	39.4	27.8	14.3	- 0.3	14.9	28.5	40.3	49.4	55.2	57.4
58	53.6	48.1	39.2	27.6	14.1	0.5	15.1	28.8	40.5	49.6	55.3	57.4
59	53.5	47.9	39.0	27.4	13.8	0.8	15.4	29.0	40.7	49.7	55.4	57.4
60	+53.4	+47.8	+38.9	+27.2	+13.6	- 1.0	-15.6	-29.2	-40.9	-49.8	-55.4	-57.4

Fig. 38

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

TABLES FOR FINDING LATITUDE BY OBSERVING POLARIS (1956)

Table (2)

Add always

Alt.	h														
					h				(hour angle)						
	h	h	h	h	h	h	h	h	h	h	h	h	h	h	h
	12	13	14	15	16	17	18	19	20	21	22	23	24		
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
10	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	
15	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	
20	0.0	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	
25	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.0	0.0	
30	0.0	0.0	0.1	0.1	0.2	0.2	0.3	0.3	0.2	0.2	0.1	0.1	0.0	0.0	
35	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.3	0.3	0.2	0.2	0.1	0.0	0.0	
40	0.0	0.0	0.1	0.2	0.3	0.4	0.4	0.4	0.4	0.3	0.2	0.1	0.0	0.0	
45	0.0	0.0	0.1	0.2	0.3	0.4	0.4	0.4	0.4	0.3	0.2	0.1	0.0	0.0	
50	0.0	0.0	0.1	0.3	0.4	0.5	0.5	0.5	0.5	0.4	0.3	0.1	0.0	0.0	
55	0.0	0.0	0.2	0.3	0.5	0.6	0.7	0.6	0.6	0.5	0.3	0.2	0.0	0.0	
60	0.0	0.1	0.2	0.4	0.6	0.7	0.8	0.7	0.7	0.6	0.4	0.2	0.1	0.0	
65	0.0	0.1	0.2	0.5	0.7	0.9	1.0	0.9	0.9	0.7	0.5	0.2	0.1	0.0	
70	0.0	0.1	0.3	0.6	1.0	1.2	1.3	1.2	1.2	1.0	0.6	0.3	0.1	0.0	

Table (3)

Add always

Date M.D.	h														
					h				(hour angle)						
	h	h	h	h	h	h	h	h	h	h	h	h	h	h	
	12	13	14	15	16	17	18	19	20	21	22	23	24		
1 1	0.7	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.1	1.2	1.2	1.2	1.3	
1 21	0.7	0.7	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.1	1.2	1.2	1.3	1.3	
2 10	0.7	0.7	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.1	1.2	1.2	1.3	1.3	
3 1	0.8	0.8	0.8	0.8	0.9	0.9	1.0	1.1	1.1	1.1	1.2	1.2	1.2	1.2	
3 21	0.9	0.9	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.1	1.1	1.1	1.1	1.1	
4 10	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
4 30	1.1	1.1	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.9	
5 20	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.8	0.8	
6 9	1.2	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.8	
6 29	1.3	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.7	
7 19	1.3	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.7	
8 8	1.2	1.2	1.2	1.2	1.1	1.1	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.8	
8 28	1.2	1.1	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	0.9	0.9	0.8	
9 17	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	
10 7	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.1	1.1	1.1	
11 27	0.8	0.8	0.8	0.9	0.9	1.0	1.0	1.0	1.0	1.1	1.1	1.2	1.2	1.2	
12 16	0.7	0.7	0.7	0.8	0.8	0.9	1.0	1.1	1.1	1.2	1.2	1.3	1.3	1.3	
12 6	0.6	0.6	0.6	0.7	0.8	0.9	1.0	1.1	1.1	1.2	1.3	1.4	1.4	1.4	
12 26	0.5	0.5	0.6	0.6	0.8	0.9	1.0	1.1	1.1	1.2	1.4	1.4	1.5	1.5	
46	0.5	0.5	0.5	0.6	0.7	0.9	1.0	1.1	1.1	1.3	1.4	1.5	1.5	1.5	

Lat. = (Obs. true Alt.) + (Tab. 1) + (Tab. 2) + (Tab. 3)

$h = U + E_* + L$ in T. (L → E. Long. → +
W. Long. → -)

Fig. 39

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

1956

AZIMUTH OF POLARIS

l	h				h				h				h ₁₂
	h ₀	h ₁	h ₂	h ₃	h ₄	h ₅	h ₆	h ₇	h ₈	h ₉	h ₁₀	h ₁₁	
		W	W	W	W	W	W	W	W	W	W	W	
0	0.0	0.2	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.2	0.0
5	0.0	0.2	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.2	0.0
10	0.0	0.2	0.5	0.7	0.8	0.9	1.0	0.9	0.8	0.7	0.5	0.2	0.0
15	0.0	0.3	0.5	0.7	0.8	0.9	1.0	0.9	0.8	0.7	0.5	0.3	0.0
20	0.0	0.3	0.5	0.7	0.9	1.0	1.0	1.0	0.9	0.7	0.5	0.3	0.0
25	0.0	0.3	0.5	0.7	0.9	1.0	1.0	1.0	0.9	0.7	0.5	0.3	0.0
30	0.0	0.3	0.5	0.8	0.9	1.0	1.1	1.0	0.9	0.8	0.5	0.3	0.0
35	0.0	0.3	0.6	0.8	1.0	1.1	1.1	1.1	1.0	0.8	0.6	0.3	0.0
40	0.0	0.3	0.6	0.9	1.1	1.2	1.2	1.2	1.1	0.9	0.6	0.3	0.0
45	0.0	0.3	0.7	0.9	1.2	1.3	1.3	1.3	1.2	0.9	0.7	0.3	0.0
50	0.0	0.4	0.7	1.0	1.3	1.4	1.5	1.4	1.3	1.0	0.7	0.4	0.0
55	0.0	0.4	0.8	1.2	1.4	1.6	1.6	1.6	1.4	1.2	0.8	0.4	0.0
60	0.0	0.5	0.9	1.3	1.6	1.8	1.9	1.8	1.6	1.3	0.9	0.5	0.0
65	0.0	0.6	1.1	1.6	1.9	2.1	2.2	2.1	1.9	1.6	1.1	0.6	0.0
70	0.0	0.7	1.4	1.9	2.4	2.7	2.7	2.7	2.4	1.9	1.4	0.7	0.0

l	h				h				h				h ₂₄
	h ₁₂	h ₁₃	h ₁₄	h ₁₅	h ₁₆	h ₁₇	h ₁₈	h ₁₉	h ₂₀	h ₂₁	h ₂₂	h ₂₃	
		E	E	E	E	E	E	E	E	E	E	E	
0	0.0	0.2	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.2	0.0
5	0.0	0.2	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.2	0.0
10	0.0	0.2	0.5	0.7	0.8	0.9	1.0	0.9	0.8	0.7	0.5	0.2	0.0
15	0.0	0.3	0.5	0.7	0.8	0.9	1.0	0.9	0.8	0.7	0.5	0.3	0.0
20	0.0	0.3	0.5	0.7	0.9	1.0	1.0	1.0	0.9	0.7	0.5	0.3	0.0
25	0.0	0.3	0.5	0.7	0.9	1.0	1.0	1.0	0.9	0.7	0.5	0.3	0.0
30	0.0	0.3	0.5	0.8	0.9	1.0	1.1	1.0	0.9	0.8	0.5	0.3	0.0
35	0.0	0.3	0.6	0.8	1.0	1.1	1.1	1.1	1.0	0.8	0.6	0.3	0.0
40	0.0	0.3	0.6	0.9	1.1	1.2	1.2	1.2	1.1	0.9	0.6	0.3	0.0
45	0.0	0.3	0.7	0.9	1.2	1.3	1.3	1.3	1.2	0.9	0.7	0.3	0.0
50	0.0	0.4	0.7	1.0	1.3	1.4	1.5	1.4	1.3	1.0	0.7	0.4	0.0
55	0.0	0.4	0.8	1.2	1.4	1.6	1.6	1.6	1.4	1.2	0.8	0.4	0.0
60	0.0	0.5	0.9	1.3	1.6	1.8	1.9	1.8	1.6	1.3	0.9	0.5	0.0
65	0.0	0.6	1.1	1.6	1.9	2.1	2.2	2.1	1.9	1.6	1.1	0.6	0.0
70	0.0	0.7	1.4	1.9	2.4	2.7	2.7	2.7	2.4	1.9	1.4	0.7	0.0

$h = utE \pm L \text{ in } T$
E. long $\rightarrow +$
W. long $\rightarrow -$

$0^h < h < 12^h$ suffix \rightarrow W

$12^h < h < 24^h$ suffix \rightarrow E

Prefix is always N

Fig. 39-a

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Problem

At 04^h 35^m on 5 August 1956, a navigator observed the altitude of Polaris as 22°17'0 in D.R.P. 21°13 N, 161°35 W. What was his latitude?

Where : Chronometer time when he observed Polaris was 3^h 14^m 35^s, chronometer error ⊕ 12^m 43^s, index error ⊖ 0.2, height of eye 16 metres, air temperature 23°C, sea water temperature 25°C,

Solution

Ship's Time 5 Aug. 1956	04 ^h 35 ^m 00 ^s	
L. in T. (161°- 35'W)	<u>10 46 00</u>	⊕
G.D. 5 Aug. 1956	15 ^h 21 ^m 00 ^s	
Chro. T.	15 ^h 14 ^m 35 ^s	(3 ^h 14 ^m 35 ^s p.m.)
C.E.	<u>12 43</u>	⊕
U 5 Aug. 1956	15 ^h 27 ^m 18 ^s	(See Fig. 40)
E* (u = 0h)	19 00 04	(From nautical almanac)
P.P. (E*)	<u>2 32</u>	⊕ (From Fig. 27)
	34 29 54	
	<u>24</u>	⊖
hG	10 ^h 29 ^m 54 ^s	
L. in T.	<u>10 46 20</u>	⊖
h.	23 ^h 43 ^m 34 ^s	
Sex Alt.*	22° - 17'0	
I.E.	<u>0.2</u>	⊖
Obs. Alt.	22° - 16'8	
Corr. 1	<u>9.5</u>	⊖
	22° - 07'3	
Corr. 2	<u>0.1</u>	⊕
	22° - 07'4	
Corr. t	<u>0.4</u>	⊖
True Alt.*	22° - 07'0	
	=====	

True Alt.* 22° - 07!0
 Corr. I 57.2 ⊖
 21° - 09!8
 Corr. II 0.0
 21° - 09!8
 Corr. III 8.0 ⊕
 21° - 10!6 N

Ans. Lat. = 21° - 10!6 N

Problem

Solution

Obs Alt. 22° - 07!0
 I.E. 0.5
 Obs. Alt. 22° - 16!8
 Corr. I 9.5
 22° - 07!3
 Corr. II 0.1
 22° - 07!4
 Corr. III 0.4
 22° - 07!0

Ship's Time 5 Aug. 1956
 L. in T. (10!0 - 32!W)
 G.D. 5 Aug. 1956
 Chron. T.
 C.E.
 U
 5 Aug. 1956
 E* (u = 0n)
 P.P. (R*)
 L. in T.
 Sex Alt.*
 I.E.
 Obs. Alt.
 Corr. I
 Corr. II
 Corr. III
 True Alt.*

Longitude by equal altitude of a celestial body

If a ship is proceeding with a constant course and at a constant speed, the value of variation of celestial body's altitude should be zero (nil) at the time of observation of its apparent maximum altitude. The variation of celestial body's altitude should be the same value and contrary name when the navigator observes this celestial body in accurate time interval before its transit and after its transit to the time of apparent maximum altitude.

In this particular case, a celestial body's altitude before transit and after transit must be equal, so if the navigator observes the altitude of the celestial body some minutes before its transit and records the time observed (= T₁), and its equal altitude after transit by the same sextant and at the same height of eye, and records the time observed (=T₂), the mean time (T) of T₁, and T₂ is given as shown below,

$$T = \frac{1}{2}(T_1 + T_2)$$

By using the arithmetic mean time (T), it is possible for navigators to obtain longitude. In other words, very accurate time (T) of a celestial body's transit in apparent maximum altitude can show navigator's longitude using some calculations.

Hour angle "h" at the time of transit can be given as follows,

$$h = - 15^s.28 (\tan \ell \mp \tan d)(\Delta \ell \mp \Delta d) \left(1 - \frac{\Delta E}{3,600} \mp \frac{\Delta L}{900}\right)$$

ℓ = latitude, d = declination, $\Delta \ell$ = value of variant of ℓ for one hour, Δd = value of variant of d for ten or some minutes (obtainable from the nautical almanac), ΔE = value of variant of E for one hour { $E = R - R.A. + (24h)$, $R = R.A.M.S. - 12h + (24h)$ }

Note

Name of the above mentioned, values when each value is increasing, name should be positive + when each value is decreasing, name should be negative-.

In the formula

$$h = 15^{\text{S}}.28 (\tan \ell \mp \tan d) (\Delta\ell \mp d) \left(1 - \frac{\Delta E}{3600} \mp \frac{\Delta Z}{900}\right)$$

$$\begin{aligned} \text{when } \ell \text{ has same name as } d, & \rightarrow \ominus \} \rightarrow (\tan \ell \mp \tan d) \\ \ell \text{ has contrary name to } d, & \rightarrow \oplus \} \rightarrow (\Delta\ell \pm \Delta) \end{aligned}$$

$$\begin{aligned} \text{Longitude is east} & \rightarrow \ominus \} \\ \text{Longitude is west} & \rightarrow \oplus \} \rightarrow \left(1 - \frac{\Delta E}{3600} + \frac{\Delta Z}{900}\right) \end{aligned}$$

Units of $\Delta\ell$, Δd and ΔZ should be 1' (minute)

Units of ΔE should be 1^S (second) and except for observations of the moon value of ΔE can be regarded as zero (nil)

The values of $15.28 \tan L$ and $15.28 \tan d$ are shown in the table (Fig. 41). After calculation according to the formula, if there is negative name of local hour angle (h), subtract it from 24h to convert it into the west local hour angle.

When the value of "h" is given, navigators can calculate the Local Mean Time (L.M.T.) using the following equation

$$\text{L.M.T.} = h - E \quad (E = E^{\odot}, E_{*} \text{ etc.})$$

In comparison with Local Mean Time (L.M.T.) and Universal Time (U.T.), it is possible to obtain the correct Longitude in Time (L. in T.) at the time of celestial body's apparent maximum altitude.

Calculation procedure:

1. when L.M.T. is faster than U.T.
 $L.M.T. - U.T. = L. \text{ in } T.$ (Longitude \rightarrow east)
2. when L.M.T. is slower than U.T.
 $U.T. - L.M.T. = L. \text{ in } T.$ (Longitude \rightarrow west)

To carry out this method to obtain longitude, it is most important for navigators to measure time accurately when they observe equal altitude of a celestial body.

Example

On 16 November 1956, a navigator observed the sun's equal altitude before the time of transit after the time of transit in D.R.P. $04^{\circ} - 06' S$, $41^{\circ} - 28' E$. What was the longitude at arithmetical mean time? (see Fig. 41 and 42)

Where : Ship's true course was 015° , speed 16 knots,

Chronometer error \oplus 4m 13s

Chronometer time of 1st observation was $08^h 21^m 38^s$

Chronometer time of 2nd observation was $09^h 26^m 08^s$

Table for value of 15.28 tan δ or 15.28 tan d

δ	d	δ	d	δ	d	δ	d	δ	d	δ	d	δ	d	δ	d
0° 0'	0.00	10° 0'	2.69	20° 0'	5.56	30° 0'	8.82	40° 0'	12.82	50° 0'	18.21	60° 0'	26.47		
10	0.04	10	2.74	10	5.61	10	8.88	10	12.90	10	18.32	10	26.64		
20	0.09	20	2.79	20	5.66	20	8.94	20	12.97	20	18.43	20	26.83		
30	0.13	30	2.83	30	5.71	30	9.00	30	13.05	30	18.54	30	27.01		
40	0.18	40	2.88	40	5.76	40	9.06	40	13.13	40	18.65	40	27.19		
50	0.22	50	2.92	50	5.81	50	9.12	50	13.20	50	18.76	50	27.38		
1 0	0.27	11 0	2.97	21 0	5.87	31 0	9.18	41 0	12.28	51 0	18.87	61 0	27.57		
10	0.31	10	3.02	10	5.92	10	9.24	10	13.36	10	18.98	10	27.76		
20	0.36	20	3.06	20	5.97	20	9.30	20	13.44	20	19.10	20	27.95		
30	0.40	30	3.11	30	6.02	30	9.36	30	13.52	30	19.21	30	28.14		
40	0.44	40	3.16	40	6.07	40	9.42	40	13.60	40	19.32	40	28.31		
50	0.48	50	3.20	50	6.12	50	9.49	50	13.68	50	19.44	50	28.51		
2 0	0.53	12 0	3.25	22 0	6.17	32 0	9.55	42 0	13.76	52 0	19.56	62 0	28.71		
10	0.58	10	3.29	10	6.23	10	9.61	10	13.84	10	19.68	10	28.91		
20	0.62	20	3.34	20	6.28	20	9.67	20	13.92	20	19.79	20	29.15		
30	0.67	30	3.39	30	6.33	30	9.73	30	14.00	30	19.91	30	29.35		
40	0.71	40	3.43	40	6.38	40	9.80	40	14.08	40	20.03	40	29.56		
50	0.76	50	3.48	50	6.43	50	9.86	50	14.17	50	20.15	50	29.77		
3 0	0.80	13 0	3.53	23 0	6.49	33 0	9.92	43 0	14.25	53 0	20.28	63 0	29.99		
10	0.85	10	3.57	10	6.54	10	9.99	10	14.33	10	20.40	10	30.21		
20	0.89	20	3.62	20	6.59	20	10.05	20	14.42	20	20.52	20	30.42		
30	0.93	30	3.67	30	6.64	30	10.11	30	14.50	30	20.65	30	30.65		
40	0.98	40	3.72	40	6.70	40	10.18	40	14.58	40	20.78	40	30.87		
50	1.02	50	3.76	50	6.75	50	10.24	50	14.67	50	20.90	50	31.10		
4 0	1.07	14 0	3.81	24 0	6.80	34 0	10.31	44 0	14.76	54 0	21.03	64 0	31.33		
10	1.11	10	3.86	10	6.86	10	10.37	10	14.84	10	21.16	10	31.56		
20	1.16	20	3.90	20	6.91	20	10.44	20	14.93	20	21.29	20	31.80		
30	1.20	30	3.95	30	6.96	30	10.50	30	15.02	30	21.42	30	32.04		
40	1.25	40	4.00	40	7.02	40	10.57	40	15.10	40	21.55	40	32.28		
50	1.29	50	4.05	50	7.07	50	10.63	50	15.19	50	21.69	50	32.52		
5 0	1.34	15 0	4.09	25 0	7.13	35 0	10.70	45 0	15.28	55 0	21.82	65 0	32.77		
10	1.38	10	4.14	10	7.18	10	10.77	10	15.37	10	21.96	10	33.02		
20	1.43	20	4.19	20	7.23	20	10.83	20	15.46	20	22.09	20	33.27		
30	1.47	30	4.24	30	7.29	30	10.90	30	15.55	30	22.23	30	33.53		
40	1.52	40	4.29	40	7.34	40	10.97	40	15.64	40	22.37	40	33.79		
50	1.56	50	4.33	50	7.40	50	11.03	50	15.73	50	22.51	50	34.05		
6 0	1.61	16 0	4.38	26 0	7.45	36 0	11.10	46 0	15.82	56 0	22.65	66 0	34.32		
10	1.65	10	4.43	10	7.51	10	11.17	10	15.92	10	22.80	10	34.59		
20	1.70	20	4.48	20	7.56	20	11.24	20	16.01	20	22.94	20	34.86		
30	1.74	30	4.53	30	7.62	30	11.31	30	16.10	30	23.09	30	35.14		
40	1.79	40	4.57	40	7.67	40	11.38	40	16.20	40	23.23	40	35.42		
50	1.83	50	4.62	50	7.73	50	11.44	50	16.29	50	23.38	50	35.71		
7 0	1.88	17 0	4.67	27 0	7.79	37 0	11.51	47 0	16.39	57 0	23.53	67 0	36.00		
10	1.92	10	4.72	10	7.84	10	11.58	10	16.48	10	23.68	10	36.29		
20	1.97	20	4.77	20	7.90	20	11.65	20	16.58	20	23.83	20	36.59		
30	2.01	30	4.82	30	7.95	30	11.72	30	16.68	30	23.98	30	36.89		
40	2.06	40	4.87	40	8.01	40	11.80	40	16.77	40	24.14	40	37.19		
50	2.10	50	4.92	50	8.07	50	11.87	50	16.87	50	24.30	50	37.50		
8 0	2.15	18 0	4.96	28 0	8.12	38 0	11.94	48 0	16.97	58 0	24.45	68 0	37.82		
10	2.19	10	5.01	10	8.18	10	12.01	10	17.07	10	24.61	10	38.14		
20	2.24	20	5.06	20	8.24	20	12.08	20	17.17	20	24.77	20	38.46		
30	2.28	30	5.11	30	8.30	30	12.15	30	17.27	30	24.93	30	38.79		
40	2.33	40	5.16	40	8.35	40	12.23	40	17.37	40	25.10	40	39.12		
50	2.37	50	5.21	50	8.41	50	12.30	50	17.47	50	25.26	50	39.46		
9 0	2.42	19 0	5.26	29 0	8.47	39 0	12.37	49 0	17.58	59 0	25.43	69 0	39.81		
10	2.47	10	5.31	10	8.53	10	12.45	10	17.68	10	25.60	10	40.15		
20	2.51	20	5.36	20	8.59	20	12.52	20	17.79	20	25.77	20	40.51		
30	2.56	30	5.41	30	8.65	30	12.60	30	17.89	30	25.94	30	40.87		
40	2.60	40	5.46	40	8.70	40	12.67	40	18.00	40	26.11	40	41.23		
50	2.65	50	5.51	50	8.76	50	12.75	50	18.10	50	26.29	50	41.60		
10 0	2.69	20 0	5.56	30 0	8.82	40 0	12.82	50 0	18.21	60 0	26.47	70 0	41.98		

Fig. 41

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

☉ Sun				Planet				☾ Moon			
U	E _n	d	P.P. of d	U	E _n	d	P.P.	U	E _t	d	P.P.
h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "
0 12 15	14	5 18	40.8	0 0	0.0			0 2 12	19	N 12	24.5
2	13		42.1	10	1			11	19		29.4
4	12		43.3	20	2			1	10	19	34.3
6	11		44.6	30	3			2	9	19	39.2
8	10		45.0	40	4			3	7	19	44.0
10	10		47.1	50	5			4	6	19	48.9
12 12 15	9	5 18	40.3	1 0	0.6			5	5	18	53.7
14	8		49.6	10	7			6	5	18	58.6
16	7		50.0	20	8			7	4	18	63.4
18	6		52.0	30	9			8	3	18	68.2
20	5		53.3	40	1.0			9	2	17	73.0
22	4		54.5	50	1			10	1	17	77.8
24 12 15	3	5 18	55.7	2 0	1.2						
(H.P. 57.2, S.D. 15 36)											
6 2 0	16	N 13	22.5					6 2 0	16	N 13	22.5
1	15		27.3					7	15		27.3
2	14		32.0					8	14		32.0
3	13		36.7					9	13		36.7
4	12		41.4					10	12		41.4
5	11		46.1					11	11		46.1
6	10		50.8								
7	9		55.4								
8	8		60.1								
9	7		64.7								
10	6		69.3								
11	5		73.9								
12	4		78.5								
13	3		83.1								
14	2		87.7								
15	1		92.3								
16	0		96.9								
17	0		101.5								
18	0		106.1								
19	0		110.7								
20	0		115.3								
21	0		119.9								
22	0		124.5								
23	0		129.1								
24	0		133.7								
(H.P. 57.4, S.D. 15 39)											
12 1 48	1	N 14	18.5					12 1 48	1	N 14	18.5
13	0		23.0					13	0		23.0
14	58		27.6					14	58		27.6
15	56		32.1					15	56		32.1
16	54		36.6					16	54		36.6
17	52		41.1					17	52		41.1
18	50		45.5					18	50		45.5
19	48		50.0					19	48		50.0
20	46		54.4					20	46		54.4
21	44		58.9					21	44		58.9
22	42		63.3					22	42		63.3
23	40		67.7					23	40		67.7
24	38		72.1					24	38		72.1
(H.P. 57.6, S.D. 15 42)											
18 1 35	35	N 15	12.0					18 1 35	35	N 15	12.0
19	34		16.3					19	34		16.3
20	33		20.7					20	33		20.7
21	32		25.0					21	32		25.0
22	31		29.2					22	31		29.2
23	30		33.5					23	30		33.5
24	29		37.8					24	29		37.8
25	28		42.0					25	28		42.0
26	27		46.2					26	27		46.2
27	26		50.4					27	26		50.4
28	25		54.6					28	25		54.6
29	24		58.7					29	24		58.7
30	23		62.9					30	23		62.9
(H.P. 57.8, S.D. 15 46)											
Planet											
R.A. d Mag. H.P. S.D.											
☉	19 10 9	5 29	-3.5	0.1	7						
☽	23 29 6	4 51	-0.8	0.2	7						
♂	11 49 N	2 26	-1.4	0.0	16						
♀	16 9 6	19 17	+0.7	0.0	7						
♃	15 32 8	19 33	-0.8	0.1	2						

Fig. 42

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Solution

Ship's time 16 Nov. 1956	12 ^h 00 ^m 00 ^s
L. in T. (41° - 28'E)	2 45 52 ⊖
G.D.	09 ^h 14 ^m 08 ^s
T ₂	09 ^h 26 ^m 08 ^s
T ₁	08 21 38 ⊖
	01 04 30

2) 01 04 30
0^h 32^m 15^s

Diff.	0 ^h 32 ^m 15 ^s
T ₁	08 ^h 21 ^m 38 ^s
C.E.	04 13 ⊕

U. 16 Nov. 1956	08 ^h 25 ^m 51 ^s
Diff.	0 32 15 ⊕

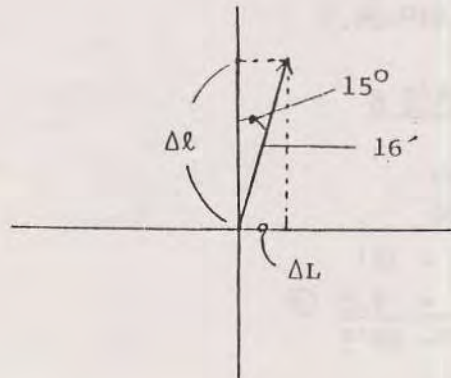
U. 16 Nov. 1956	08 ^h 58 ^m 06 ^s	→ d = 18° - 46.4 S
-----------------	---	--------------------

E ⊕ for 08h 58m 10s = 12 ^h 15 ^m 10 ^s	Δd = ⊕ 0.6 (d of P.P. for one hour)
(from the nautical almanac)	

By the nautical almanac,
U = 8h → d = 18° - 45.8s
P.P. for 58^m 06^s 0.6
d for 08^h 58^m 06^s = 18° - 46.4s

True course 015° = N 15°E	Δℓ = ⊖ 15.5 (for one hour)
speed = 16 knots	Δℓ = ⊕ 4.1 (for one hour)
ℓ = 04° - 06'.s	Δℓ = 16' x cos 15° ≐ 15.5
	ΔL = 16' x sin 15° ≐ 4.1

Feb.

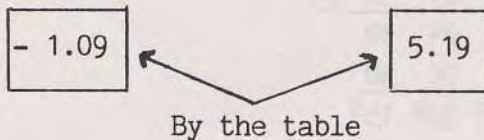


ℓ had the same name as d, celestial body was the sun, longitude was east

$$h = - 15^s.28 (\tan \ell - \tan d)(\Delta \ell - \Delta d) \left(1 - \frac{\Delta \angle}{900}\right)$$

$$= - 15^s.28 \left\{ \tan (04^{\circ}06') - \tan (18^{\circ}46'.4) \right\} (\ominus 15.5 - 0.6) \left\{ 1 - \frac{4.1}{900} \right\}$$

$$= - \left[\underbrace{15^s.28 \left\{ \tan (04^{\circ}06') \right\}}_{-1.09} \right] - \left[\underbrace{15^s.28 \tan (18^{\circ}46'.4)}_{5.19} \right] (\ominus 15.5 - 0.6) \left(1 - \frac{4.1}{900} \right)$$



So,

$$= - (1.09 - 5.19) (- 15.5 - 0.6) \left(1 - \frac{4.1}{900} \right)$$

$$= - (- 4.1) (- 16.1) (0.995)$$

$$= - (66.01) (0.995)$$

$$= - 65^s.67955$$

$$\therefore \ominus 1^m 06^s$$

then,

h	24 ^h 00 ^m 00 ^s	
E _⊙	01 06	⊖
L.M.L. 16 Nov. 1956	23 ^h 58 ^m 54 ^s	
U. 16 Nov. 1956	12 15 10	⊖
L. in T.	11 ^h 43 ^m 44 ^s	
	8 58 06	⊖
	2 45 38	
	↓	
Longitude	41°-24.5	

Ans. long = 41° - 24'.5 E

2 ^h	30°	
- 44 ^m	11°	
- 01 ^m	- 15'	
- 38 ^s ⊕	- 9.5 ⊕	
2 ^h 45 ^m 38 ^s →	41°- 24'.5	

Example

On 22 March 1956, a navigator observed the sun's equal altitude before the time of transit and after the time of transit in D.R.P. $02^{\circ} - 10'N$, $70^{\circ} - 10'E$

What was the longitude at noon of ship's time?

Where: Ship's true course was 325° , speed 18 Knots,
 chronometer error $\ominus 0^m 16^s$
 Chronometer time of 1st observation was $06^h 58^m 53^s$
 Chronometer time of 2nd observation was $07^h 54^m 57^s$
 Time zone was (U + $4^h 36^m$)

Solution (See Figs. 41 and 43)

Ship's T.	22 Mar, 1956	12 ^h 00 ^m 00 ^s		T ₁	07 ^h 54 ^m 57 ^s
L in T		4 41 00	\ominus	T ₂	06 58 53 \ominus
G.D.	22 Mar, 1956	07 19 00			00 56 04
				2)	00 56 04
				Diff.	00 ^h 28 ^m 02 ^s
T ₁		06 ^h 58 ^m 53 ^s			
C.E.		0 16	\ominus		
U ₁	22 Mar, 1956	06 58 37			
Diff.		0 28 02	\oplus		d = $0^{\circ} - 39'6'' N$
U	22 Mar, 1956	07 26 39			$\Delta d = \oplus 1.0$ (d of P.P. for one hour)
E ₀		11 53 01			(From nautical almanac)
True Course	$325^{\circ} = N 35^{\circ}W$				
Speed	= 18.0 knots				
ℓ	= $2^{\circ} - 10'N$				
			}		$\Delta \ell \oplus 14'7''$
					$\Delta L \ominus 10'3''$

ℓ had the same name as d
 celestial body was the sun
 longitude was east

$$\begin{aligned}
 h &= - 15^s.28 (\tan \ell - \tan d) (\Delta \lambda - \Delta d) \left(1 - \frac{\Delta L}{900}\right) \\
 &= - (0.58 - 0.18) (14.7 - 1.0) \left(1 + \frac{10.3}{900}\right) \\
 &= - (0.40 \times 13.7 \times \frac{910.3}{900}) \\
 &= - 6^s
 \end{aligned}$$

	24 ^h 00 ^m 00 ^s	
	06	⊖
h	23 59 54	
E ⊕	11 53 01	⊖
L.M.T.	12 06 53	(22 Mar. 1956)
U	7 26 39	⊖ (22 Mar. 1956)
L. in T.	4 40 14	
Long.	70° 03'5 E ← This longitude was for arithmetic mean time	

So the arithmetic mean time should be converted into ship's time as follows:

U 22 Mar. 1956	07 ^h 26 ^m 39 ^s
L. in T.	04 36 00 ⊕
Ship's T. 22 Mar. 1956	12 02 39

Next, calculate D. long for 02^m 39^s shown as below:

	10!3 W x $\frac{2.65}{60}$ = 0!5 W
then	70° - 03!5 E
	0.5 E ⊕ + Be careful of the sign
Ans.	70° - 04.0 E
	=====

22 March 1956 Lunar Age 9d.4
Nautical Almanac

Table with columns for Sun, Planet (Venus, Mars, Jupiter, Saturn), Moon Tr., and Star. It lists celestial bodies with their right ascension, declination, distance, and magnitude. Includes sub-sections for S.D., U=0h, and Planet R.A. Mag. H.P. S.D.

Fig. 43

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

True Bearing by Amplitude

When the navigator observes direction of a celestial body by ship's compass and knows its true direction by calculation, it is possible to obtain the compass error or its deviation.

If the navigator observes the direction of a celestial body when its true altitude is zero or its center is just on the celestial horizon by his compass, and calculates its true direction, he can obtain compass error or deviation of the compass.

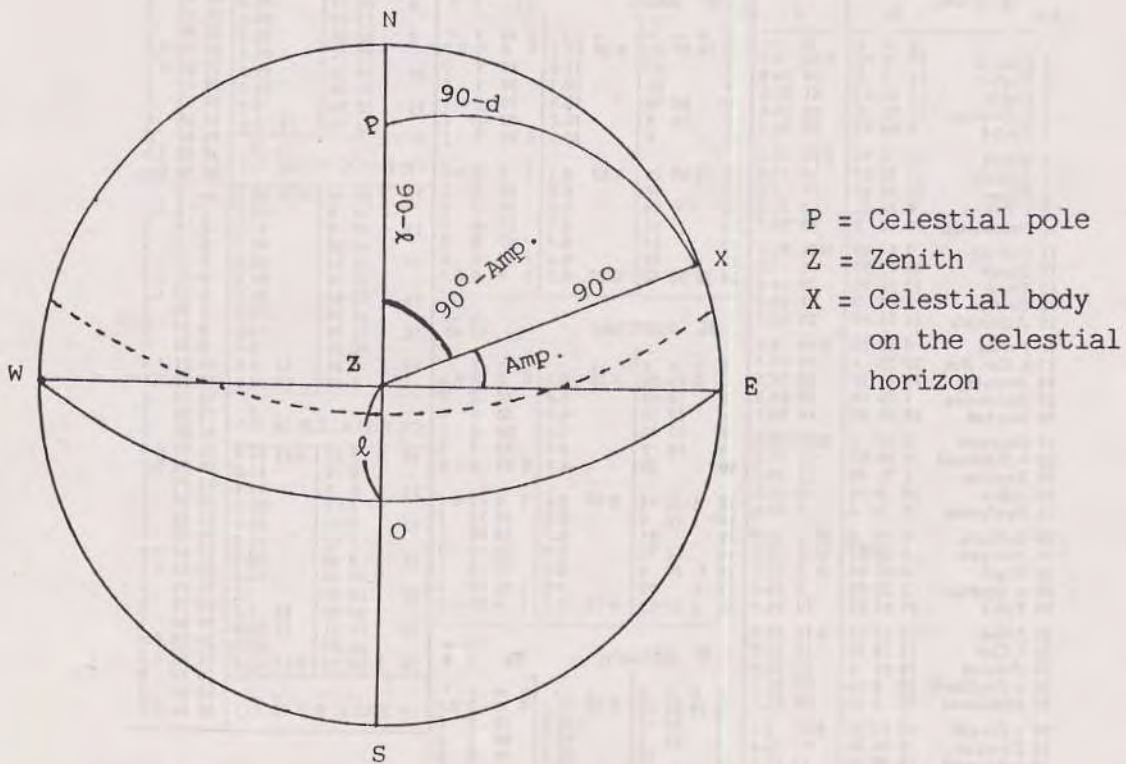


Fig. 44

In Figure 44, $ZX = 90^\circ$, so PZX is quadrantal triangle
 then, $\sin (90^\circ - PX) = \cos (90^\circ - PZ) \cos \angle PZX$

$$PX = 90^\circ - d, PZ = 90^\circ - \ell^\circ$$

↓

$$\sin \{90^\circ - (90^\circ - d^\circ)\} = \cos \{90^\circ - (90^\circ - \ell^\circ)\} \cos \angle PZX$$

$$\sin \{90^\circ - 90^\circ + d^\circ\} = \cos \{90^\circ - 90^\circ + \ell^\circ\} \cos \angle PZX$$

$$\sin d = \cos \ell^\circ \cdot \cos \angle PZX$$

$$\angle PZX = 90^\circ \pm \text{Amp.}$$

$$\sin d = \cos \ell \cdot \cos (90^\circ \pm \text{Amp.})$$

$$= \cos \ell \cdot \sin \text{Amp.}$$

$$\sin \text{Amp.} = \frac{\sin d}{\cos \ell} \sec \ell \cdot \sin d$$

$$\therefore \underline{\sin \text{Amp.} = \sec \ell \cdot \sin d} \text{ or Amp.} = \sin^{-1} (\sec \ell \sin d)$$

Ref.

Formula of trigonometric function

$$\cos (\theta \pm \psi) = \cos \theta \cos \psi \pm \sin \theta \sin \psi$$

$$\text{so, } \cos (90^\circ \pm \text{Amp.}) = \frac{\cos 90^\circ}{\cos 90^\circ} \cos \text{Amp.} \mp \frac{\sin 90^\circ}{\sin 90^\circ} \sin \text{Amp.}$$

↓

↓

$$= \frac{0}{\cos 90^\circ} \cos \text{Amp.} \mp \frac{1}{\sin 90^\circ} \sin \text{Amp.}$$

↓

↓

0

± sin Amp.

$$= \mp \sin \text{Amp.}$$

If the navigator knows the amplitude of a celestial body,
 true bearing can be given as follows,

$$\underline{\text{True bearing} = 90^\circ - \text{true Amp.}}$$

Note 1

Prefix of amplitude should be E or W, and suffix of
 amplitude should be N or S.

At sunrise, prefix of amplitude → E
At sunset, prefix of amplitude → W
Suffix is the same as declination's name

Note 2

When d is zero, that is, the celestial body is located on the celestial equator,

$$\begin{aligned}\sin \text{ Amp.} &= \sec \ell \times \sin d \\ &= \sec \ell \times \sin d 0^\circ \\ &= \sec \ell \times 0 \\ &= 0 \\ \text{Amp.} &= 0\end{aligned}$$

In this case, the celestial body rises in due east (90°) sets in due west (270°)

When ℓ is zero, the navigator is located on the equator.

$$\begin{aligned}\sin \text{ Amp.} &= \sec 0^\circ \times \sin d \\ &= 1 \times \sin d \\ &= \sin d \\ \text{Amp.} &= d\end{aligned}$$

In this case, the value of Amplitude is equal to the value of d .

True bearing by Amplitude of the sun

The sun is the celestial body observed most frequently when obtaining an Amplitude

When the navigator observes the lower limb of the sun, its altitude correction is shown as:

$$\begin{aligned}\text{True Alt. } \ominus &= \text{Obs. Alt.} - \text{Dip-Ref.} + \text{S.D.} + \text{Par} \\ \text{Ref.} &= \text{Refraction. S.D.} = \text{Visible semi-diameter} \\ \text{Par.} &= \text{Parallax}\end{aligned}$$

In the case of observing Amplitude, True. Alt \ominus (true altitude of the sun) should be zero. so.

$$0 = \text{Obs. Alt.} - \text{Dip.} - \text{Ref.} + \text{S.D.} + \text{Par.}$$
$$\therefore \text{Obs. Alt.} = \text{Dip.} + \text{Ref.} - \text{S.D.} - \text{Par.}$$

When sunset or sunrise,

$$\text{Ref.} = 29', \text{S.D.} = 13' \text{ and Par.} = 8'' 95 \doteq 0$$

then Obs. Alt. = Dip. + 29' - 13' - 0' = Dip + 16'

If the observer's height of eye is 15 feet (= 4.6 metres), Dip is about 4', so, Obs. Alt. 4' + 16' = 20'

"Obs. Alt. = 20'" means that when the lower limb of the sun is 20' above the horizon, true altitude of the sun should be zero (sunrise or sunset)

The only time when the navigator should observe the amplitude of the sun is when the sun's lower limb is about 20' (nearly half of semidiameter) above visible horizon.

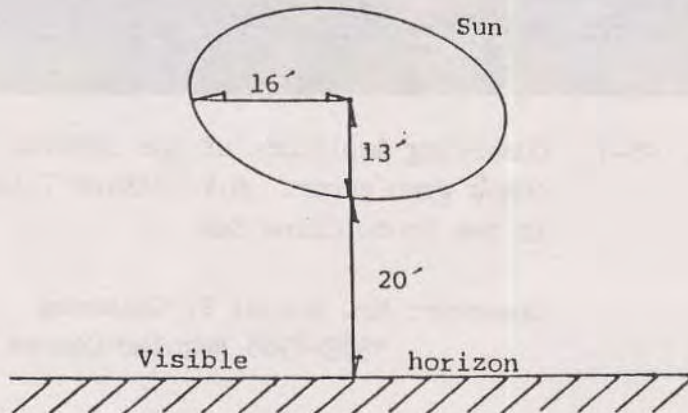


Fig. 45 Amplitude of the sun

Needless to say, when you observe the direction of the sun, you have to observe the center of the sun.



Fig. 45-1 Observing Amplitude of the setting sun to check gyro error. M.V. PAKNAM 7 Aug. 1985, in the South China Sea

Observer: Mr. Roscal P. Galunsag
1983-1985 Regular Course Trainee

Example 10

On 5 August 1956, a navigator observed true amplitude of the rising sun in D.R.P. $32^{\circ}-20'N$, $129^{\circ}-48'E$ by magnetic compass as $N 88^{\circ}.5 E$. What was the deviation of compass? Where: variation $5^{\circ}.2 W$

Solution

(From nautical almanac Fig. 47)

d (5 Aug. 1956, U = 0h)	$17^{\circ} 02'.8 N$	}	$\rightarrow 6^h 45^m$ (from Fig. 50)
λ	$32^{\circ} 20' N$		
	$12^h 00^m 00^s$		
h_o	$06 45 00 \ominus$		
L.A.T. 5 Aug. 1956	$05 15 00$		
L in T.	$08 39 00 \ominus$		
G.A.T. 4 Aug. 1956	$20 36 00$		
	↓		
d (4 Aug. 1956 U = 20h 36m 00s)	$17^{\circ}-05'.9 N$	}	$20^{\circ}.4$ (from Fig. 51)
	$32^{\circ}-20'.0 N$		

Ref.

$$\begin{aligned} \sin \text{ Amp.} &= \sin d \sec \lambda = \sin (17^{\circ} 05'.9) \times \sec (32^{\circ}-20'.0) \\ &= 0.29404 \times 1.18350 = 0.347996 \dots \\ \text{Amp.} &= 20^{\circ}-22' \\ &= 20^{\circ}.4 \end{aligned}$$

True Amp. = $E 20^{\circ}.4 N$ ← Be careful about both prefix and suffix

	<u>$90^{\circ}.0 -$</u>	
True B'g	= $N 69^{\circ}.6 E$	
Comp. B'g	= $N 88^{\circ}.5 E$	
Comp. error	= $18^{\circ}.9 W$	
Var.	= $5^{\circ}.2 W$	
Dev.	= $13^{\circ}.7 W$	<u>Ans. Deviation = $13^{\circ}.7 W$</u>

4 August 1956
Nautical Almanac
Lunar Age 26.8

☉ Sun				Planet				☾ Moon Tr.				
U	E ₀	d	P.P. of d	U	E _p	d	P.P.	U	E _t	d	P.P.	
h h m s	°	'	h m s	h h m s	°	'	h m s	h h m s	°	'	h m s	
0 11 53.59	N17	16.9	0 0 0.0	♀ Venus				0 14 22.31	N20	42.9	1 2 0.1	
2 53 59		17.5	10 1 0.1	h h m s	°	'	h m s	1 21 17		40.6	2 5 2	
4 54 0		18.2	20 2 0.2	0 14 51.12	N18	29.0	0 0 0.0	1 20 3		38.2	3 7 3	
6 0		14.9	30 3 0.3	2 19		29.2	10 1 0.0	1 18 49		35.8	4 10 4	
8 0		13.5	40 4 0.4	4 25		29.5	20 1 1.1	2 17 35		33.4	5 12 5	
10 1		12.2	50 5 0.5	6 32		29.8	30 2 1.1	3 16 20		30.9	6 15 5	
12 11 54.1	N17	10.9	1 0 0.7	8 39		30.1	40 2 1.1	3 15 6		28.4	7 17 6	
14 2		9.5	10 8 0.8	10 45		30.4	50 3 1.1	4 13 52		25.8	8 20 7	
16 2		8.2	20 0.9	12 14 51.52	N18	30.7	1 0 1.0	4 12 38		23.2	9 22 8	
18 3		6.9	30 1.0	14 51.58		30.9	10 4 2.2	5 11 24		20.6	10 25 0.9	
20 3		5.5	40 1 1.1	16 52 5		31.2	20 5 2.2	5 10 10		17.9	11 27 1.0	
22 4		4.2	1 50 2.2	18 11		31.5	30 5 2.2	6 8 56		15.2	12 30 1	
24 11 54.4	N17	2.0	2 0 1.3	20 10		31.8	40 6 3.3	(H.P.60.8, S.D.16 34)				
S.D. 15 48				22 24		32.1	1 50 6.3	6 14 7 42	N20	12.5	13 32 2	
U = Oh				24 14 52 30	N18	32.3	2 0 7 0.9	6 28		9.7	14 35 3	
★ Star				♂ Mars				♁ Jupiter				
No.	E _s	d	U = Oh	h h m s	°	'	h m s	h h m s	°	'	h m s	
1	Polaris	18 56 9	N89	0 21 5 32	S 7	49.6	0 0 0.0	0 10 20 7	N10	27.5	0 0 0.0	
2	Kochab	5 59 20		2 5 50		49.6	10 2 0	2 23		27.1	10 1 0	
3	Dubhe	9 49 6		4 6 7		49.7	20 3 0	4 38		26.7	20 3 1	
4	β Cassiop.	20 43 14		6 25		49.7	30 5 0	6 20 54		26.3	30 4 1	
5	Merak	9 50 55		8 6 43		49.7	40 6 0	8 21 10		26.0	40 5 1	
6	Alioth	7 58 1	N56	10 7 1		49.7	50 11 0	10 26		25.6	50 7 2	
7	Schedir	20 12 4		12 21 7 18	S 7	49.7	1 0 9 0.0	12 10 21 42	N10	25.2	1 0 8 0.2	
8	Mizar	7 27 57		14 36		49.8	10 11 0	14 21 57		24.8	10 9 2	
9	α Persei	17 28 54		16 7 54		49.8	20 12 0	16 22 13		24.4	20 11 3	
10	β Persei	7 4 18		18 8 12		49.8	30 14 0	18 29		24.0	30 12 3	
11	Capella	15 36 39	N45	20 90		49.9	40 15 0	20 22 45		23.7	40 13 3	
12	Deneb	0 10 8		22 8 48		49.9	1 50 17 0	22 23 1		23.3	1 50 15 4	
13	Vega	2 14 38		24 21 9 6	S 7	49.9	2 0 18 0.0	24 10 23 16	N10	22.9	2 0 16 0.4	
14	Castor	13 18 18		♄ Saturn				h h m s	°	'	h m s	
15	Alpheratz	20 43 58		0 5 12 42	S17	20.9	0 0 0.0	0 19 2		21.0	10 2 0	
16	Pollux	13 7 29	N28	2 19 2		21.0	10 2 0	2 7 2		21.0	20 3 0	
17	α Cor. Bor.	5 17 16		4 7 2		21.0	20 3 0	4 19 41		21.0	30 5 0	
18	Arcturus	6 36 26		6 19 41		21.0	30 5 0	6 14 1		21.0	40 7 0	
19	Aldebaran	16 16 42		8 14 1		21.0	40 7 0	8 20		21.1	50 8 0	
20	Markeb	21 47 30		10 20		21.1	0 50 8 0	10 14 40	S17	21.1	1 0 10 0.0	
21	Denebola	9 3 17	N14	12 15 48.9		21.1	10 12 0	12 15 0		21.1	10 12 0	
22	α Ophiuchi	3 17 11		14 21 57		21.2	20 13 0	14 15 0		21.2	20 13 0	
23	Regulus	10 44 4		16 22 13		21.2	30 15 0	16 19		21.2	30 15 0	
24	Altair	1 1 28		18 29		21.2	40 17 0	18 9 9		21.3	1 50 18 0	
25	Betelgeuse	14 57 19		20 22 45		21.2	40 17 0	20 15 58		21.2	40 17 0	
26	Bellatrix	15 27 20	N 6	22 23 1		21.3	1 50 18 0	22 16 18	S17	21.3	2 0 20 0.0	
27	Procyon	13 13 6	N 5	24 10 23 16	N10	22.9	2 0 16 0.4	24 5 16 37	S17	21.3	2 0 20 0.0	
28	Rigel	15 37 41	S 8	Planet				R.A.	d	Mag.	H.P.	S.D.
29	α Hydrae	11 24 41		R.A.				d	Mag.	H.P.	S.D.	
30	Spica	7 27 13		d				Mag.	H.P.	S.D.		
31	Sirius	14 6 54	S16	Mag.				H.P.	S.D.			
32	β Ceti	20 8 42		H.P.				S.D.				
33	Antares	4 23 22		S.D.								
34	α Sagittarii	1 57 31										
35	Fomalhaut	21 54 50										
36	λ Scorpii	3 19 26	S37									
37	Canopus	14 27 10										
38	α Pavonis	0 27 51										
39	α Achernar	19 14 1										
40	β Crucis	8 4 57										
41	β Centauri	6 49 22	S60									
42	α Centauri	6 13 28										
43	α Crucis	9 25 57										
44	α Tri. Aust.	4 6 1										
45	β Carinae	11 37 27	S69									

Fig. 46

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

5 August 1956 Lunar d
Nautical Almanac Age 27.8

☉ Sun				Planet				☾ Moon				
U	E _a	d	P.P. of d	U	E _p	d	P.P.	U	E _t	d	P.P.	
h m s				☿ Venus				h m s				
0 11 54		N17 2.0	0 0 0.0	Tr.				h m s				
2 5 5		1.5	10 1 1	h m s				0 13 23	33	N18 9.3	1 2 0.1	
4 5 5		17 0.1	20 2 2	h m s				1 21 0		10 1.1	2 5 3	
6 5 6		16 59.8	30 4 4	0 11 52	30	N18 32.3	0 0 0.0	2 19 55		17 57.0	4 10 6	
8 5 6		57.1	40 5 5	2 4 37		32.6	10 1 0	4 19 42		52.0	5 12 7	
10 5 7		56.1	0 50 6	4 4 33		32.9	20 1 1	6 17 29		48.6	6 14 0.9	
				6 6 49		33.2	30 2 1	8 16 17		44.4	7 17 1.0	
12 11 51	7	N16 54.7	1 0 0.7	8 52 55		33.5	40 2 1	10 15 4		40.1	8 19 2	
14 8 8		53.3	10 0 0	10 53 2		33.7	0 50 3 1	12 13 52		35.8	9 22 3	
16 8 8		52.0	20 0.9	12 11 53	8	N18 34.0	1 0 3 0.2	14 12 39		31.5	10 24 5	
18 9 9		50.6	30 1.1	14 14		34.3	10 4 2	16 11 27		27.1	11 26 6	
20 9 9		49.2	40 2 2	16 20		34.6	20 4 2	18 10 14		22.7	12 29 8	
22 10 10		47.9	1 50 3	18 26		34.9	30 5 2	(H.P. 61.2, S.D. 16 40)			13 31 1.9	
24 11 54 10		N16 46.5	2 0 1.4	20 32		35.1	40 5 3	6 13 9	2	N17 16.3	14 34 2.1	
S.D. 15 40				22 39		35.4	1 50 6 3	7 7 49		13.8	15 36 2	
				24 14 53	11	N18 35.7	2 0 6 0.3	8 6 37		9.4	16 38 3	
				♂ Mars				9 5 25		4.8	17 41 5	
U=0h				Tr.				10 4 13		17 0.3	18 43 6	
No.	★ Star	E _a	d	h m s				11 3 1		16 55.7	19 46 6	
1	Polaris	19 0 4	N89 3.4	0 21 9	6	57 49.9	0 0 0.0	12 12 54	37	N16 22.8	20 48 2.9	
2	Kochab	6 3 17	74 20.3	2 21		50.0	10 2 0	13 53 26		18.0	21 50 3.1	
3	Dubhe	9 53 2	61 59.2	4 9 42		50.0	20 3 0	14 52 14		13.1	22 53 2	
4	♂ Cassiop.	20 47 11	58 54.6	6 10 0		50.1	30 5 0	15 51 2		8.2	23 55 4	
5	Merak	9 54 52	56 37.0	8 18		50.1	40 6 0	16 49 51		16 3.3	24 58 5	
6	Alioth	0 1 50	N56 11.9	10 36		50.2	0 50 0 0	17 48 39		15 58.4	25 60 3.8	
7	Schedir	20 16 0	56 17.9	12 21 10	54	50.2	1 0 9 0.1	18 47 28		53.4	26 62 5.0	
8	Mizar	7 31 54	55 9.3	14 11 12		50.3	10 11 1	19 46 17		48.5	27 65 4.0	
9	♂ Persei	17 32 51	49 42.3	16 30		50.3	20 12 1	20 45 5		43.4	28 67 1.1	
10	Benetnasch	7 8 15	49 32.0	18 11 48		50.3	30 14 1	21 44 3		38.9	29 70 3	
11	Capella	15 40 35	N45 57.2	20 12 6		50.4	40 15 1	22 43 2		33.3	30 72 4.4	
12	Deneb	0 14 5	45 7.7	22 21		50.5	1 50 17 1	23 42 43		28.2		
13	Vega	2 18 34	38 44.0	24 21 12	43	50.6	2 0 10 0.1	24 41 32		26.2		
14	Castor	13 22 15	31 59.1	♃ Jupiter				h m s				
15	Alphératz	20 47 54	28 51.1	Tr.				13 35				
16	Pollux	13 11 25	N28 7.9	h m s								
17	♂ Cor. Bar.	5 21 13	26 51.8	0 10 23	16	N10 22.9	0 0 0.0					
18	Arcturus	6 40 23	19 24.6	2 32		22.5	10 1 0					
19	Aldebaran	16 20 38	16 25.4	4 23 48		22.1	20 3 1					
20	Markab	21 51 27	14 58.4	6 24 4		21.7	30 4 1					
21	Denebola	9 7 14	N14 48.9	8 20		21.4	40 5 1					
22	♂ Ophiuchi	3 21 8	12 35.6	10 35		21.0	0 50 7 2					
23	Regulus	10 48 1	12 10.0	12 10 24	51	N10 20.6	1 0 8 0.2					
24	Allair	1 5 22	8 45.4	14 25 7		20.2	10 9 2					
25	Bolelgeuse	15 1 15	7 24.0	16 23		19.8	20 11 3					
26	Bellatrix	15 31 16	N 6 18.7	18 39		19.4	30 12 3					
27	Procyon	13 17 3	N 5 20.2	20 25 51		19.1	40 13 3					
28	Rigel	15 41 37	R 8 14.9	22 26 10		18.7	1 50 15 4					
29	♂ Hydrae	11 28 38	8 28.2	24 10 25	26	N10 18.3	2 0 16 0.4					
30	Spica	7 31 10	10 56.2	♄ Saturn				h m s				
31	Sirius	14 10 51	S16 39.3	Tr.								
32	♂ Ceti	20 12 39	18 13.2	h m s								
33	Antares	4 27 18	26 20.3	0 5 16	37	S17 21.3	0 0 0.0					
34	♂ Sagittari	2 1 28	26 21.0	2 16 57		21.3	10 2 0					
35	Fomalhaut	21 58 47	29 50.9	4 17 15		21.3	20 3 0					
36	♂ Scorpii	3 23 23	S37 4.5	6 36		21.4	30 5 0					
37	Canopus	14 31 7	52 40.2	8 17 56		21.4	40 7 0					
38	♂ Pavonis	0 31 47	56 52.4	10 18 15		21.4	0 50 8 0					
39	Achernar	19 17 58	57 27.0	12 5 18	35	S17 21.5	1 0 10 0.0					
40	♂ Crucis	8 8 54	59 27.4	14 18 54		21.5	10 12 0					
41	♂ Centauri	6 53 10	S60 10.2	16 19 14		21.5	20 18 0					
42	♂ Centauri	6 17 25	60 39.0	18 7 3		21.6	30 15 0					
43	♂ Crucis	8 29 54	62 51.8	20 19 53		21.6	40 17 0					
44	♂ Tri. Aust.	4 9 57	80 57.3	22 20 12		21.6	1 50 18 0					
45	♂ Carinae	11 41 23	S69 32.4	24 5 29	32	S17 21.7	2 0 20 0.0					
R ₀ 20 54 4				Planet								
				R.A.				d	Mag.	H.P.	S.D.	
				☿	6 2	N10 32	-4.2	0.3	17			
				♂	23 45	R 7 50	-1.9	0.3	10			
				♃	10 31	N10 23	-1.3	0.0	15			
				♄	15 37	R17 21	+0.7	0.0	8			
				♅	10 5	N13 11	-0.4	0.1	3			

Fig. 47

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

RISING AND SETTING AZIMUTH (True Alt.=0°) (1956)

lat. l	Declination															
	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°
0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0	14.0	15.0	16.0
2	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0	14.0	15.0	16.0
4	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0	14.0	15.0	16.0
6	1.0	2.0	3.0	4.0	5.0	6.0	7.1	8.1	9.1	10.1	11.1	12.1	13.1	14.1	15.1	16.1
8	1.0	2.0	3.0	4.1	5.1	6.1	7.1	8.1	9.1	10.1	11.1	12.1	13.1	14.1	15.1	16.2
10	1.0	2.0	3.1	4.1	5.1	6.1	7.1	8.1	9.2	10.2	11.2	12.2	13.2	14.2	15.3	16.3
12	1.0	2.1	3.1	4.1	5.1	6.1	7.2	8.2	9.2	10.2	11.3	12.3	13.3	14.3	15.4	16.4
14	1.0	2.1	3.1	4.1	5.2	6.2	7.2	8.3	9.3	10.3	11.3	12.4	13.4	14.4	15.5	16.5
15	1.1	2.1	3.1	4.2	5.2	6.2	7.3	8.3	9.4	10.4	11.5	12.5	13.5	14.6	15.6	16.7
19	1.1	2.1	3.2	4.2	5.3	6.3	7.4	8.4	9.5	10.5	11.6	12.6	13.7	14.7	15.8	16.9
20	1.1	2.1	3.2	4.3	5.3	6.4	7.5	8.5	9.6	10.6	11.7	12.8	13.9	14.9	16.0	17.1
21	1.1	2.2	3.2	4.3	5.4	6.4	7.5	8.6	9.7	10.7	11.8	12.9	14.0	15.0	16.1	17.2
22	1.1	2.2	3.2	4.3	5.4	6.5	7.6	8.7	9.8	10.8	11.9	13.0	14.1	15.1	16.2	17.3
23	1.1	2.2	3.3	4.4	5.4	6.5	7.6	8.7	9.8	10.9	12.0	13.1	14.2	15.3	16.3	17.4
24	1.1	2.2	3.3	4.4	5.5	6.6	7.7	8.8	9.9	11.0	12.1	13.2	14.3	15.4	16.5	17.6
25	1.1	2.2	3.3	4.4	5.5	6.6	7.7	8.8	9.9	11.1	12.2	13.3	14.4	15.5	16.6	17.7
26	1.1	2.2	3.4	4.5	5.6	6.7	7.8	8.9	10.0	11.2	12.3	13.4	14.5	15.6	16.8	17.9
27	1.1	2.3	3.4	4.5	5.6	6.7	7.9	9.0	10.1	11.3	12.4	13.5	14.6	15.8	16.9	18.0
28	1.1	2.3	3.4	4.5	5.7	6.8	7.9	9.1	10.2	11.4	12.5	13.6	14.8	15.9	17.1	18.2
29	1.2	2.3	3.4	4.6	5.7	6.9	8.0	9.2	10.3	11.5	12.6	13.8	14.9	16.1	17.2	18.4
30	1.2	2.3	3.5	4.6	5.8	6.9	8.1	9.3	10.4	11.6	12.7	13.9	15.1	16.2	17.4	18.6
31	1.2	2.3	3.5	4.7	5.8	7.0	8.2	9.4	10.5	11.7	12.9	14.0	15.2	16.4	17.6	18.8
32	1.2	2.4	3.6	4.7	5.9	7.1	8.3	9.5	10.6	11.8	13.0	14.2	15.4	16.6	17.8	19.0
33	1.2	2.4	3.6	4.8	6.0	7.2	8.4	9.6	10.8	12.0	13.2	14.4	15.6	16.8	18.0	19.2
34	1.2	2.4	3.6	4.8	6.0	7.3	8.5	9.7	10.9	12.1	13.3	14.5	15.8	17.0	18.2	19.4
35	1.2	2.5	3.7	4.9	6.1	7.3	8.6	9.8	11.0	12.2	13.5	14.7	16.0	17.2	18.4	19.7
36	1.2	2.5	3.7	5.0	6.2	7.4	8.7	9.9	11.2	12.4	13.7	14.9	16.2	17.4	18.7	19.9
37	1.3	2.5	3.8	5.0	6.3	7.5	8.8	10.0	11.3	12.6	13.8	15.1	16.4	17.6	18.9	20.2
38	1.3	2.5	3.8	5.1	6.4	7.6	8.9	10.2	11.4	12.7	14.0	15.3	16.6	17.9	19.2	20.5
39	1.3	2.6	3.9	5.2	6.4	7.7	9.0	10.3	11.6	12.9	14.2	15.5	16.8	18.1	19.5	20.8
40	1.3	2.6	3.9	5.2	6.5	7.9	9.2	10.5	11.8	13.1	14.4	15.8	17.1	18.4	19.8	21.1
41	1.3	2.7	4.0	5.3	6.6	8.0	9.3	10.6	12.0	13.3	14.7	16.0	17.4	18.7	20.1	21.4
42	1.4	2.7	4.0	5.4	6.7	8.1	9.4	10.8	12.2	13.5	14.9	16.3	17.6	19.0	20.4	21.8
43	1.4	2.7	4.1	5.5	6.9	8.2	9.6	11.0	12.4	13.7	15.1	16.5	17.9	19.3	20.7	22.1
44	1.4	2.8	4.2	5.6	7.0	8.4	9.8	11.2	12.6	14.0	15.4	16.8	18.2	19.7	21.1	22.5
45	1.4	2.8	4.3	5.7	7.1	8.5	9.9	11.4	12.8	14.2	15.7	17.1	18.6	20.0	21.5	23.0
46	1.4	2.9	4.3	5.8	7.2	8.7	10.1	11.6	13.0	14.5	16.0	17.4	18.9	20.4	21.9	23.4
47	1.5	2.9	4.4	5.9	7.4	8.8	10.3	11.8	13.3	14.8	16.3	17.8	19.3	20.8	22.3	23.8
48	1.5	3.0	4.5	6.0	7.5	9.0	10.5	12.0	13.5	15.1	16.6	18.1	19.7	21.2	22.8	24.3
49	1.5	3.1	4.6	6.1	7.6	9.2	10.7	12.3	13.8	15.4	16.9	18.5	20.1	21.6	23.2	24.9
50	1.6	3.1	4.7	6.2	7.8	9.4	10.9	12.5	14.1	15.7	17.3	18.9	20.5	22.1	23.8	25.4
51	1.6	3.2	4.8	6.4	8.0	9.6	11.2	12.8	14.4	16.0	17.7	19.3	21.0	22.6	24.3	26.0
52	1.6	3.3	4.9	6.5	8.1	9.8	11.4	13.1	14.7	16.4	18.1	19.7	21.4	23.2	24.9	26.6
53	1.7	3.3	5.0	6.7	8.3	10.0	11.7	13.4	15.1	16.8	18.5	20.2	22.0	23.7	25.5	27.3
54	1.7	3.4	5.1	6.8	8.5	10.3	12.0	13.7	15.4	17.2	19.0	20.7	22.5	24.3	26.1	28.0
55	1.8	3.5	5.2	7.0	8.7	10.5	12.3	14.1	15.8	17.6	19.4	21.2	23.1	25.0	26.8	28.7
56	1.8	3.6	5.4	7.2	9.0	10.8	12.6	14.4	16.3	18.1	20.0	21.8	23.7	25.6	27.6	29.5
57	1.8	3.7	5.5	7.4	9.2	11.1	12.9	14.8	16.7	18.6	20.5	22.4	24.4	26.4	28.4	30.4
58	1.9	3.8	5.7	7.6	9.5	11.4	13.3	15.2	17.2	19.1	21.1	23.1	25.1	27.2	29.2	31.3
59	2.0	3.9	5.8	7.8	9.8	11.7	13.7	15.7	17.7	19.7	21.7	23.8	25.9	28.0	30.2	32.4
60	2.0	4.0	6.0	8.0	10.0	12.1	14.1	16.2	18.2	20.3	22.4	24.6	26.7	28.9	31.2	33.5
61	2.1	4.1	6.2	8.3	10.4	12.5	14.6	16.7	18.8	21.0	23.2	25.4	27.7	29.9	32.3	34.7
62	2.1	4.3	6.4	8.6	10.7	12.9	15.1	17.3	19.5	21.7	24.0	26.3	28.6	31.0	33.5	36.0
63	2.2	4.4	6.6	8.8	11.1	13.3	15.6	17.9	20.2	22.5	24.9	27.3	29.7	32.2	34.8	37.4
64	2.3	4.6	6.9	9.2	11.5	13.8	16.1	18.5	20.9	23.3	25.8	28.3	30.9	33.5	36.2	39.0
65	2.4	4.7	7.1	9.5	11.9	14.3	16.8	19.2	21.7	24.3	26.8	29.5	32.2	34.9	37.8	40.7

Azimuth should be measured from E or W (Prefix)
 Suffix is the same as for declination

Fig. 49

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

RISING AND SETTING HOUR ANGLE (True Alt.=0°) (1956)

lat <i>l</i>	Declination <i>d</i>														
	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°
0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0
2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	5
4	5	5	5	6	6	6	6	7	7	7	8	8	9	9	9
6	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14
8	9	10	10	11	12	12	13	14	14	15	16	16	17	18	19
10	6 12	6 12	6 13	6 14	6 15	6 16	6 16	6 17	6 18	6 19	6 20	6 21	6 22	6 22	6 23
12	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
14	16	17	19	20	21	22	23	24	25	27	28	29	30	32	33
16	19	20	21	23	24	25	27	28	29	31	32	34	35	37	38
18	21	23	24	26	27	29	30	32	33	35	36	38	40	42	43
20	6 24	6 26	6 27	6 29	6 30	6 32	6 34	6 36	6 37	6 39	6 41	6 43	6 45	6 47	6 49
21	25	27	29	30	32	34	36	38	39	41	43	45	47	49	51
22	27	28	30	32	34	36	38	40	41	43	45	48	50	52	54
23	28	30	32	34	36	38	40	42	44	46	48	50	52	54	57
24	29	31	33	35	37	39	41	44	46	48	50	52	55	6 57	7 0
25	6 31	6 33	6 35	6 37	6 39	6 41	6 43	6 46	6 48	6 50	6 53	6 55	6 57	7 0	7 2
26	32	34	36	39	41	43	45	48	50	53	55	6 58	7 0	3	5
27	34	36	38	40	43	45	48	50	52	55	6 58	7 0	3	6	8
28	35	37	40	42	45	47	50	52	55	6 57	7 0	3	6	9	12
29	37	39	42	44	47	49	52	54	6 57	7 0	3	6	9	12	15
30	6 38	6 41	6 43	6 46	6 49	6 51	6 54	6 57	7 0	7 2	7 5	7 8	7 12	7 15	7 18
31	40	42	45	48	51	53	56	6 59	2	5	8	11	15	18	21
32	41	44	47	50	53	56	6 58	7 2	5	8	11	14	18	21	25
33	43	46	49	52	55	6 58	7 1	4	7	11	14	17	21	24	28
34	45	48	51	54	57	7 0	3	7	10	13	17	20	24	28	32
35	6 46	6 49	6 53	6 56	6 59	7 2	7 6	7 9	7 13	7 16	7 20	7 24	7 27	7 31	7 35
36	48	51	55	6 58	7 1	5	8	12	15	19	23	27	31	35	39
37	50	53	57	7 0	4	7	11	15	18	22	26	30	34	39	43
38	52	55	6 59	2	6	10	14	17	21	25	30	34	38	43	47
39	54	57	7 1	5	9	12	16	20	25	29	33	37	42	47	51
40	6 56	6 59	7 3	7 7	7 11	7 15	7 19	7 23	7 28	7 32	7 37	7 41	7 46	7 51	7 56
41	6 58	7 2	6	10	14	18	22	27	31	36	40	45	50	55	6 0
42	7 0	4	8	12	17	21	25	30	35	39	44	49	54	6 0	5
43	2	6	11	15	19	24	29	33	38	43	48	53	59	4	10
44	4	9	13	18	22	27	32	37	42	47	52	58	8 4	9	16
45	7 7	7 11	7 16	7 21	7 25	7 30	7 35	7 40	7 46	7 51	7 57	8 3	8 8	8 15	8 21
46	9	14	19	24	29	34	39	44	50	7 55	8 1	7	14	20	27
47	12	17	22	27	32	37	43	48	54	8 0	6	12	19	26	33
48	14	19	25	30	35	41	47	53	7 59	5	11	18	25	32	40
49	17	22	28	33	39	45	51	7 57	8 3	10	17	24	31	38	46
50	7 20	7 25	7 31	7 37	7 43	7 49	7 55	8 2	8 8	8 15	8 22	8 30	8 37	8 45	8 54
51	23	29	35	41	47	53	8 0	6	13	21	28	36	44	53	9 2
52	26	32	38	45	51	7 58	5	12	19	27	35	43	52	9 1	11
53	29	36	42	49	7 56	8 2	10	17	25	33	41	50	9 0	9	20
54	33	40	46	53	8 0	8	15	23	31	40	49	58	8	19	30
55	7 37	7 44	7 51	7 58	8 5	8 13	8 21	8 29	8 38	8 47	8 57	9 7	9 18	9 29	9 42
56	41	48	7 55	8 3	11	19	27	36	45	8 55	9 5	16	28	41	9 55
57	45	52	8 0	8	16	25	34	43	53	9 4	15	27	40	54	10 11
58	49	7 57	5	14	22	32	41	51	9 2	13	25	38	53	10 10	30
59	54	8 2	11	20	29	39	49	9 0	11	24	37	52	10 9	29	10 56
60	7 59	8 8	8 17	8 26	8 36	8 47	8 58	9 9	9 22	9 35	9 51	10 8	10 28	10 55	12 0
61	8 5	14	24	34	44	55	9 7	20	34	9 49	10 7	27	10 54	12 0	
62	11	20	31	41	53	9 5	18	32	47	10 5	26	10 54	12 0		
63	17	27	38	8 50	9 2	16	30	46	10 4	25	10 53	12 0			
64	24	35	47	9 0	13	28	9 44	10 2	24	10 52	12 0				
65	8 32	8 44	8 57	9 10	9 25	9 42	10 0	10 22	10 51	12 0					

when the name of latitude is the same as declination, use tabulated value; when contrary, use 12h - tabulated value

Fig. 50

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

RIISING AND SETTING AZIMUTH (True Alt.=0°) (1956)

lat.	Declination									d								
	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°			
0	16.0	17.0	18.0	19.0	20.0	21.0	22.0	23.0	24.0	25.0	26.0	27.0	28.0	29.0	30.0			
2	16.0	17.0	18.0	19.0	20.0	21.0	22.0	23.0	24.0	25.0	26.0	27.0	28.0	29.0	30.0			
4	16.0	17.1	18.1	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	29.1	30.1			
6	16.1	17.1	18.1	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.2	27.2	28.2	29.2	30.2			
8	16.2	17.2	18.2	19.2	20.2	21.2	22.2	23.2	24.3	25.3	26.3	27.3	28.3	29.3	30.3			
10	16.3	17.3	18.3	19.3	20.3	21.4	22.4	23.4	24.4	25.4	26.4	27.5	28.5	29.5	30.5			
12	16.4	17.4	18.4	19.4	20.5	21.5	22.5	23.6	24.6	25.6	26.6	27.7	28.7	29.7	30.7			
14	16.5	17.5	18.6	19.6	20.6	21.7	22.7	23.8	24.8	25.8	26.9	27.9	28.9	30.0	31.0			
16	16.7	17.7	18.8	19.8	20.9	21.9	22.9	24.0	25.0	26.1	27.1	28.2	29.2	30.3	31.4			
18	16.9	17.9	19.0	20.0	21.1	22.1	23.2	24.3	25.3	26.4	27.5	28.5	29.6	30.7	31.7			
20	17.1	18.1	19.2	20.3	21.4	22.4	23.5	24.6	25.6	26.7	27.8	28.9	30.0	31.1	32.2			
21	17.2	18.3	19.3	20.4	21.5	22.6	23.7	24.8	25.8	26.9	28.0	29.1	30.2	31.3	32.4			
22	17.3	18.4	19.5	20.6	21.7	22.7	23.8	24.9	26.0	27.1	28.2	29.3	30.4	31.5	32.6			
23	17.4	18.5	19.6	20.7	21.8	22.9	24.0	25.1	26.2	27.3	28.4	29.6	30.7	31.8	32.9			
24	17.6	18.7	19.8	20.9	22.0	23.1	24.2	25.3	26.4	27.6	28.7	29.8	30.9	32.1	33.2			
25	17.7	18.8	19.9	21.1	22.2	23.3	24.4	25.5	26.7	27.8	28.9	30.1	31.2	32.3	33.5			
26	17.9	19.0	20.1	21.2	22.4	23.5	24.6	25.8	26.9	28.0	29.2	30.3	31.5	32.6	33.8			
27	18.0	19.2	20.3	21.4	22.6	23.7	24.9	26.0	27.2	28.3	29.5	30.6	31.8	33.0	34.1			
28	18.2	19.3	20.5	21.6	22.8	24.0	25.1	26.3	27.4	28.6	29.8	30.9	32.1	33.3	34.5			
29	18.4	19.5	20.7	21.9	23.0	24.2	25.4	26.5	27.7	28.9	30.1	31.3	32.5	33.7	34.9			
30	18.6	19.7	20.9	22.1	23.3	24.5	25.6	26.8	28.0	29.2	30.4	31.6	32.8	34.1	35.3			
31	18.8	20.0	21.1	22.3	23.5	24.7	25.9	27.1	28.3	29.5	30.8	32.0	33.2	34.5	35.7			
32	19.0	20.2	21.4	22.6	23.8	25.0	26.2	27.4	28.7	29.9	31.1	32.4	33.6	34.9	36.1			
33	19.2	20.4	21.6	22.9	24.1	25.3	26.5	27.8	29.0	30.3	31.5	32.8	34.0	35.3	36.6			
34	19.4	20.6	21.9	23.1	24.4	25.6	26.9	28.1	29.4	30.7	31.9	33.2	34.5	35.8	37.1			
35	19.7	20.9	22.2	23.4	24.7	26.0	27.2	28.5	29.8	31.1	32.4	33.7	35.0	36.3	37.5			
36	19.9	21.2	22.5	23.7	25.0	26.3	27.6	28.9	30.2	31.5	32.8	34.1	35.5	36.8	38.2			
37	20.2	21.5	22.8	24.1	25.4	26.7	28.0	29.3	30.6	31.9	33.3	34.6	36.0	37.4	38.8			
38	20.5	21.8	23.1	24.4	25.7	27.1	28.4	29.7	31.1	32.4	33.8	35.2	36.6	38.0	39.4			
39	20.8	22.1	23.4	24.8	26.1	27.5	28.8	30.2	31.6	32.9	34.3	35.8	37.2	38.6	40.1			
40	21.1	22.4	23.8	25.2	26.5	27.9	29.3	30.7	32.1	33.5	34.9	36.4	37.8	39.3	40.8			
41	21.4	22.8	24.2	25.6	27.0	28.4	29.8	31.2	32.6	34.1	35.5	37.0	38.5	40.0	41.5			
42	21.8	23.2	24.6	26.0	27.4	28.8	30.3	31.7	33.2	34.7	36.2	37.7	39.2	40.7	42.3			
43	22.1	23.6	25.0	26.4	27.9	29.3	30.8	32.3	33.8	35.3	36.8	38.4	39.9	41.5	43.1			
44	22.5	24.0	25.4	26.9	28.4	29.9	31.4	32.9	34.4	36.0	37.5	39.2	40.7	42.4	44.0			
45	23.0	24.4	25.9	27.4	28.9	30.5	32.0	33.6	35.1	36.7	38.3	39.9	41.6	43.3	45.0			
46	23.4	24.9	26.4	28.0	29.5	31.1	32.6	34.2	35.8	37.5	39.1	40.8	42.5	44.3	46.0			
47	23.8	25.4	27.0	28.5	30.1	31.7	33.3	35.0	36.6	38.3	40.0	41.7	43.5	45.3	47.2			
48	24.3	25.9	27.5	29.1	30.7	32.4	34.1	35.7	37.4	39.2	40.9	42.7	44.5	46.4	48.4			
49	24.9	26.5	28.1	29.8	31.4	33.1	34.8	36.6	38.3	40.1	41.9	43.8	45.7	47.7	49.7			
50	25.4	27.1	28.7	30.4	32.2	33.9	35.6	37.4	39.3	41.1	43.0	44.9	46.9	49.0	51.1			
51	26.0	27.7	29.4	31.2	32.9	34.7	36.5	38.4	40.3	42.2	44.2	46.2	48.2	50.4	52.6			
52	26.6	28.4	30.1	31.9	33.8	35.6	37.5	39.4	41.4	43.4	45.4	47.5	49.7	52.0	54.3			
53	27.3	29.1	30.9	32.8	34.8	36.6	38.5	40.5	42.5	44.6	46.7	49.0	51.3	53.7	56.2			
54	28.0	29.8	31.7	33.6	35.6	37.6	39.6	41.7	43.8	46.0	48.2	50.6	53.0	55.6	58.3			
55	28.7	30.7	32.6	34.6	36.7	38.7	40.8	42.9	45.2	47.5	49.8	52.3	54.9	57.7	60.7			
56	29.5	31.5	33.6	35.6	37.7	39.9	42.1	44.3	46.7	49.1	51.6	54.3	57.1	60.1	63.4			
57	30.4	32.5	34.6	36.7	38.9	41.2	43.5	45.9	48.3	50.9	53.6	56.5	59.6	62.9	66.7			
58	31.3	33.5	35.7	37.9	40.2	42.6	45.0	47.5	50.1	52.9	55.8	58.9	62.4	66.2	70.7			
59	32.4	34.6	36.9	39.2	41.6	44.1	46.7	49.4	52.2	55.1	58.3	61.8	65.7	70.3	76.2			
60	33.5	35.9	38.2	40.6	43.2	45.8	48.5	51.4	54.4	57.7	61.2	65.2	69.9	75.8	90.0			
61	34.7	37.1	39.6	42.2	44.9	47.7	50.6	53.7	57.0	60.6	64.7	69.4	75.5	90.0				
62	36.0	38.5	41.2	43.9	46.8	49.8	52.9	56.3	60.0	64.2	69.0	75.2	90.0					
63	37.4	40.1	42.9	45.8	48.9	52.1	55.6	59.4	63.6	68.6	74.9	90.0						
64	39.0	41.8	44.8	48.0	51.3	54.8	58.7	63.0	68.1	74.6	90.0							
65	40.7	43.8	47.0	50.4	54.0	58.0	62.4	67.6	74.2	90.0								

Azimuth should be measured from E or W (Prefix)
 Suffix is the same as declination name

Fig. 51

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY,
 JAPAN.

Problem

On 14 February 1956, a navigator observed true amplitude of the sun setting in D.R.P. $27^{\circ} - 06'N$, $109^{\circ} - 17'W$ by magnetic compass as $N 87^{\circ}.5 W$. What was the compass deviation?

Where: Variation was $11^{\circ}.0 E$. (Ans. $27^{\circ}.7W$)
 (Ref. True Amp. = $W 14^{\circ}.2 S$, True b'g = $s 75^{\circ}.8 W$)

Direction of Celestial Body by Time-Azimuth

Time-Azimuth method is used for calculating true direction of a celestial body by considering the local hour angle (h), declination (d) and observer's latitude (ℓ).

The time of celestial observation in this method for obtaining direction of a celestial body is not limited, unlike such as the method of True Bearing by Amplitude.

Basically, navigators can utilize this method at any time, but it is desirable and advisable that they observe a celestial body when its altitude is not too high.

For the purpose of obtaining true direction by using h, d, and ℓ , Tables of SDh are given. These tables are derived from the following formulae (see Fig. 52-61).

$$Z = X + Y$$

$\log \tan x$	=	$\log \cos \frac{S}{2}$	+	$\log \operatorname{cosec} \frac{D}{2}$	+	$\log \tan \frac{h}{2}$
$\log \tan y$	=	$\log \sin \frac{S}{2}$	+	$\log \sec \frac{D}{2}$	+	$\log \tan \frac{h}{2}$
↓		↓		↓		↓
Table xy		Table S		Table D		Table h

To obtain true direction (bearing) by making use of these tables, it is necessary to calculate local hour angle (h) and declination by nautical almanac and navigator's dead reckoning position for latitude (ℓ)

Example

At 09^h 20^m a.m. on 10 June 1956, a navigator observed the compass bearing of the sun as S 86°.5 E in D.R.P. 32° - 32' N. 133° - 46' E. What was the deviation of this compass?

Where: Chronometer time was 0^h 43^m 37^s, variation 5°.4 W, and chronometer error ⊖ 16^m 17^s (see Figs. 62 and 52-61)

Solution

1. To obtain d

Ship's T. 10 June 1956	09 ^h 20 ^m 00 ^s	
L. in T. (133°- 46'E)	08 55 04	⊖
G.D. 10 June 1956	00 24 56	(From almanac see Fig. 10)
Chro. T.	00 43 37	
C.E.	16 17	⊖
U 10 June 1956	00 27 20	→ d = 22°- 59'8 N

2. To obtain h

Ref. 1 (U. 10 June 1956	00 ^h 27 ^m 20 ^s	(From almanac see
E _⊙	12 00 47	⊕ ← Fig. 10)
h _G	12 28 07	
h _G	187°- 01'8	

Ref. 2 (L (133° 46'E)	133 - 46.0	⊕
h	320°- 47.8	
d	22°- 59.8 N	
ℓ	32°- 32.0 N	

Ref. 1

$$h_G = U + E \quad h_G \odot = U + E \odot, \quad h_G \ominus = U + E \ominus \quad h_G^P = U + E_P$$

$$h_G^* = U + E^*$$

Ref. 2

$$H = h_G \pm L \text{ (when east longitude } \oplus \text{ and when west longitude } \ominus \text{)}$$

$$h = 320^\circ - 47.8, \quad d = 22^\circ 59.8 \text{ N}, \quad = 32^\circ 32.0 \text{ N}$$

About S. Name of l is same as name of d ,
 $S = l + d = (32^\circ 32') + (22^\circ 59.8') = 55^\circ - 31.8'$

About D. Name of l is same as name of d ,
 $D = l - d = (32^\circ - 32') - (22^\circ - 59.8') = 09^\circ - 32.2'$

About h is given as $320^\circ 47.8'$

So, S.	=	$55^\circ - 31.8'$	X_1	3147	Y_1	2868	
	D	=	$09^\circ - 32.2'$	X_2	1080	Y_2	1
	h	=	$320^\circ - 47.8'$	X_3	2751	Y_3	2751
				X_4	6978	Y_4	5620
				↓		↓	
				$X =$	7502	Y	904

$$x = 7502$$

$$Y = \underline{904} \oplus \leftarrow \text{when } l > d, Z = X + Y$$

$$Z = \underline{S 8406 E} \quad \text{when } h = 12^h \sim 24^h, \text{ suffix should be E}$$

$$h = 320^\circ - 47.8' + 21^h - 23^m - 11^s$$

When $l > d$, measure from pole of contrary name of l . ($l = 32^\circ - 32' \text{ N}$)

True bearing	=	S 8406 E
Comp. bearing	=	<u>S 86.5 E</u> \ominus
Comp. error	=	1.9 E
Var.	=	<u>5.4 W</u> \oplus
Dev.	=	7.3 E

Ans. Deviation = 7.3 E

Azimuth Table-S

same name → $l+d = S$

$l \& d$ { contrary name → $l-d = S$

S	X ₁	Y ₁	S	X ₁	Y ₁	S	X ₁	Y ₁	S	X ₁	Y ₁
0 0	3200	- ∞	6 0	3199	1919	18 0	3195	2394	30 0	3185	2613
5	3200	+ 62	10	3199	1931	10	3195	2398	10	3185	2615
10	3200	363	20	3199	1942	20	3194	2402	20	3185	2618
15	3200	539	30	3199	1954	30	3194	2406	30	3184	2620
20	3200	664	40	3199	1965	40	3194	2410	40	3184	2622
25	3200	761	50	3199	1975	50	3194	2414	50	3184	2625
30	3200	840	7 0	3199	1986	19 0	3194	2418	31 0	3184	2627
35	3200	907	10	3199	1996	10	3194	2421	10	3184	2629
40	3200	965	20	3199	2006	20	3194	2425	20	3184	2631
45	3200	1016	30	3199	2016	30	3194	2429	30	3183	2634
50	3200	1062	40	3199	2025	40	3194	2432	40	3183	2636
55	3200	1103	50	3199	2034	50	3193	2436	50	3183	2638
1 0	3200	1141	8 0	3199	2044	20 0	3193	2440	32 0	3183	2640
5	3200	1176	10	3199	2053	10	3193	2443	10	3183	2643
10	3200	1208	20	3199	2061	20	3193	2447	20	3182	2645
15	3200	1238	30	3199	2070	30	3193	2450	30	3182	2647
20	3200	1266	40	3199	2078	40	3193	2454	40	3182	2649
25	3200	1292	50	3199	2087	50	3193	2457	50	3182	2651
30	3200	1317	9 0	3199	2095	21 0	3193	2461	33 0	3182	2653
35	3200	1340	10	3199	2103	10	3193	2464	10	3182	2655
40	3200	1363	20	3199	2110	20	3192	2467	20	3181	2658
45	3200	1384	30	3199	2118	30	3192	2471	30	3181	2660
50	3200	1404	40	3198	2126	40	3192	2474	40	3181	2662
55	3200	1423	50	3198	2133	50	3192	2477	50	3181	2664
2 0	3200	1442	10 0	3198	2140	22 0	3192	2481	34 0	3181	2666
5	3200	1460	10	3198	2147	10	3192	2484	10	3180	2668
10	3200	1477	20	3198	2154	20	3192	2487	20	3180	2670
15	3200	1493	30	3198	2161	30	3192	2490	30	3180	2672
20	3200	1509	40	3198	2168	40	3191	2493	40	3180	2674
25	3200	1524	50	3198	2175	50	3191	2497	50	3180	2676
30	3200	1539	11 0	3198	2182	23 0	3191	2500	35 0	3179	2678
35	3200	1553	10	3198	2188	10	3191	2503	10	3179	2680
40	3200	1567	20	3198	2194	20	3191	2506	20	3179	2682
45	3200	1580	30	3198	2201	30	3191	2509	30	3179	2684
50	3200	1593	40	3198	2207	40	3191	2512	40	3179	2686
55	3200	1606	50	3198	2213	50	3191	2515	50	3178	2688
3 0	3200	1618	12 0	3198	2219	24 0	3190	2518	36 0	3178	2690
5	3200	1630	10	3198	2225	10	3190	2521	10	3178	2692
10	3200	1641	20	3197	2231	20	3190	2524	20	3178	2694
15	3200	1653	30	3197	2237	30	3190	2527	30	3178	2696
20	3200	1664	40	3197	2243	40	3190	2530	40	3177	2698
25	3200	1674	50	3197	2248	50	3190	2532	50	3177	2700
30	3200	1685	13 0	3197	2254	25 0	3190	2535	37 0	3177	2701
35	3200	1695	10	3197	2259	10	3189	2538	10	3177	2703
40	3200	1705	20	3197	2265	20	3189	2541	20	3177	2705
45	3200	1715	30	3197	2270	30	3189	2544	30	3176	2707
50	3200	1724	40	3197	2275	40	3189	2547	40	3176	2709
55	3200	1734	50	3197	2281	50	3189	2549	50	3176	2711
4 0	3200	1743	14 0	3197	2286	26 0	3189	2552	38 0	3176	2713
5	3200	1752	10	3197	2291	10	3189	2555	10	3175	2714
10	3200	1761	20	3197	2296	20	3188	2558	20	3175	2716
15	3200	1769	30	3197	2301	30	3188	2560	30	3175	2718
20	3200	1778	40	3196	2306	40	3188	2563	40	3175	2720
25	3200	1785	50	3196	2311	50	3188	2566	50	3175	2722
30	3200	1794	15 0	3196	2316	27 0	3188	2568	39 0	3174	2723
35	3200	1802	10	3196	2320	10	3188	2571	10	3174	2725
40	3200	1810	20	3196	2325	20	3188	2573	20	3174	2727
45	3200	1817	30	3196	2330	30	3187	2576	30	3174	2729
50	3200	1825	40	3196	2334	40	3187	2579	40	3173	2731
55	3200	1832	50	3196	2339	50	3187	2581	50	3173	2732
5 0	3200	1840	16 0	3196	2344	28 0	3187	2584	40 0	3173	2734
5	3200	1847	10	3196	2348	10	3187	2586	10	3173	2736
10	3200	1854	20	3196	2352	20	3187	2589	20	3173	2738
15	3200	1861	30	3195	2357	30	3186	2591	30	3172	2739
20	3200	1868	40	3195	2361	40	3186	2594	40	3172	2741
25	3200	1874	50	3195	2365	50	3186	2596	50	3172	2743
30	3199	1881	17 0	3195	2370	29 0	3186	2599	41 0	3172	2744
35	3199	1889	10	3195	2374	10	3186	2601	10	3171	2746
40	3199	1894	20	3195	2378	20	3186	2603	20	3171	2748
45	3199	1900	30	3195	2382	30	3185	2606	30	3171	2749
50	3199	1907	40	3195	2386	40	3185	2608	40	3171	2751
55	3199	1913	50	3195	2390	50	3185	2611	50	3170	2753
6 0	3199	1919	18 0	3195	2394	30 0	3185	2613	42 0	3170	2754

$$X_1 + X_2 + X_3 = X_4 + x \quad Y_1 + Y_2 + Y_3 = Y_4 + y \quad x + y = Z$$

Fig. 52

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-S

$\ell \& d$ { same name + $\ell+d = S$
 contrary name + $\ell-d = S$

$\begin{matrix} S \\ \circ \\ ' \\ '' \end{matrix}$	X_1	Y_1	$\begin{matrix} S \\ \circ \\ ' \\ '' \end{matrix}$	X_1	Y_1	$\begin{matrix} S \\ \circ \\ ' \\ '' \end{matrix}$	X_1	Y_1	$\begin{matrix} S \\ \circ \\ ' \\ '' \end{matrix}$	X_1	Y_1
42 0	3170	2754	54 0	3150	2857	66 0	3124	2936	78 0	3091	2999
10	3170	2756	10	3150	2858	10	3123	2937	10	3090	3000
20	3170	2758	20	3149	2860	20	3123	2938	20	3089	3000
30	3169	2759	30	3149	2861	30	3122	2939	30	3089	3001
40	3169	2761	40	3149	2862	40	3122	2940	40	3088	3002
50	3169	2762	50	3148	2863	50	3122	2941	50	3088	3003
43 0	3169	2764	55 0	3149	2864	67 0	3121	2942	79 0	3087	3004
10	3168	2765	10	3148	2865	10	3121	2943	10	3087	3004
20	3168	2767	20	3147	2867	20	3120	2944	20	3086	3005
30	3168	2769	30	3147	2868	30	3120	2945	30	3086	3006
40	3168	2770	40	3147	2869	40	3119	2946	40	3085	3007
50	3167	2772	50	3146	2870	50	3119	2947	50	3085	3007
44 0	3167	2774	56 0	3146	2872	68 0	3119	2948	80 0	3084	3008
10	3167	2775	10	3146	2873	10	3118	2948	10	3084	3009
20	3167	2777	20	3145	2874	20	3118	2949	20	3083	3010
30	3166	2778	30	3145	2875	30	3117	2950	30	3083	3010
40	3166	2780	40	3145	2876	40	3117	2951	40	3082	3011
50	3166	2781	50	3144	2877	50	3116	2952	50	3082	3012
45 0	3166	2783	57 0	3144	2879	69 0	3116	2953	81 0	3081	3013
10	3165	2784	10	3144	2880	10	3116	2954	10	3081	3013
20	3165	2786	20	3143	2881	20	3115	2955	20	3080	3014
30	3165	2787	30	3143	2882	30	3115	2956	30	3079	3015
40	3165	2789	40	3143	2883	40	3114	2957	40	3079	3015
50	3164	2790	50	3142	2884	50	3114	2958	50	3078	3016
46 0	3164	2792	58 0	3142	2886	70 0	3113	2959	82 0	3078	3017
10	3164	2793	10	3141	2887	10	3113	2959	10	3077	3018
20	3163	2795	20	3141	2888	20	3112	2960	20	3077	3018
30	3163	2796	30	3141	2889	30	3112	2961	30	3076	3019
40	3163	2798	40	3140	2890	40	3112	2962	40	3076	3020
50	3163	2799	50	3140	2891	50	3111	2963	50	3075	3021
47 0	3162	2801	59 0	3140	2892	71 0	3111	2964	83 0	3074	3021
10	3162	2802	10	3139	2893	10	3110	2965	10	3074	3022
20	3162	2804	20	3139	2895	20	3110	2966	20	3073	3023
30	3162	2805	30	3139	2896	30	3109	2967	30	3073	3023
40	3161	2806	40	3138	2897	40	3109	2967	40	3072	3024
50	3161	2808	50	3138	2898	50	3108	2968	50	3072	3025
48 0	3161	2809	60 0	3138	2899	72 0	3108	2969	84 0	3071	3026
10	3160	2811	10	3137	2900	10	3107	2970	10	3071	3026
20	3160	2812	20	3137	2901	20	3107	2971	20	3070	3027
30	3160	2814	30	3136	2902	30	3107	2972	30	3069	3028
40	3160	2815	40	3136	2903	40	3106	2973	40	3069	3028
50	3159	2816	50	3136	2904	50	3106	2974	50	3068	3029
49 0	3159	2818	61 0	3135	2905	73 0	3105	2974	85 0	3068	3030
10	3159	2819	10	3135	2907	10	3105	2975	10	3067	3030
20	3158	2820	20	3135	2908	20	3104	2976	20	3066	3031
30	3158	2822	30	3134	2909	30	3104	2977	30	3066	3032
40	3158	2823	40	3134	2910	40	3103	2978	40	3065	3032
50	3158	2825	50	3133	2911	50	3103	2979	50	3065	3033
50 0	3157	2826	62 0	3133	2912	74 0	3102	2979	86 0	3064	3034
10	3157	2827	10	3133	2913	10	3102	2980	10	3064	3034
20	3157	2829	20	3132	2914	20	3101	2981	20	3063	3035
30	3156	2830	30	3132	2915	30	3101	2982	30	3062	3036
40	3156	2831	40	3132	2916	40	3100	2983	40	3062	3036
50	3156	2833	50	3131	2917	50	3100	2984	50	3061	3037
51 0	3155	2834	63 0	3131	2918	75 0	3099	2984	87 0	3061	3038
10	3155	2835	10	3130	2919	10	3099	2985	10	3060	3038
20	3155	2837	20	3130	2920	20	3098	2986	20	3059	3039
30	3155	2838	30	3130	2921	30	3098	2987	30	3059	3040
40	3154	2839	40	3129	2922	40	3098	2988	40	3058	3040
50	3154	2841	50	3129	2923	50	3097	2989	50	3058	3041
52 0	3154	2842	64 0	3128	2924	76 0	3097	2989	88 0	3057	3042
10	3153	2843	10	3128	2925	10	3096	2990	10	3056	3042
20	3153	2844	20	3128	2926	20	3096	2991	20	3056	3043
30	3153	2846	30	3127	2927	30	3095	2992	30	3055	3044
40	3152	2847	40	3127	2928	40	3095	2993	40	3054	3044
50	3152	2848	50	3126	2929	50	3094	2993	50	3054	3045
53 0	3152	2850	65 0	3126	2930	77 0	3094	2994	89 0	3053	3046
10	3151	2851	10	3126	2931	10	3093	2995	10	3053	3046
20	3151	2852	20	3125	2932	20	3093	2996	20	3052	3047
30	3151	2853	30	3125	2933	30	3092	2997	30	3051	3048
40	3151	2855	40	3124	2934	40	3092	2997	40	3051	3048
50	3150	2856	50	3124	2935	50	3091	2998	50	3050	3049
54 0	3150	2857	66 0	3124	2936	78 0	3091	2999	90 0	3049	3049

$$X_1 + X_2 + X_3 = X_4 \rightarrow x \quad Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y \quad x \pm y = Z$$

Fig. 53

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-D

ℓ&d { same name + ℓ-d = D
 contrary name + ℓ+d = D

D	X ₁	Y ₁		D	X ₁	Y ₁		D	X ₁	Y ₁		D	X ₁	Y ₁	
0 0	+∞	0	180 0	6 0	1281	1	174 0	0 0	806	5	162 0	30 0	587	15	150 0
0 5	3138	0	55	6 5	1269	1	50	0 5	802	5	50	10	585	15	50
10	2837	0	50	10	1258	1	40	10	798	6	40	20	582	15	40
15	2661	0	45	15	1246	1	30	15	794	6	30	30	580	16	30
20	2536	0	40	20	1235	1	20	20	790	6	20	40	578	16	20
25	2439	0	35	25	1225	1	10	25	786	6	10	50	575	18	10
30	2360	0	30	30	1214	1	0	30	782	6	0	60	573	18	0
35	2293	0	25	35	1204	1	50	35	779	6	50	10	571	18	50
40	2235	0	20	40	1194	1	40	40	775	6	40	20	569	18	40
45	2184	0	15	45	1184	1	30	45	771	6	30	30	566	17	30
50	2138	0	10	50	1175	1	20	50	768	6	20	40	564	17	20
55	2097	0	5	55	1166	1	10	55	764	7	10	50	562	17	10
1 0	2059	0	179 0	8 0	1156	1	172 0	20 0	760	7	160 0	32 0	560	17	148 0
1 5	2024	0	55	10	1147	1	50	10	757	7	50	10	557	17	50
10	1992	0	50	15	1139	1	40	15	753	7	40	20	555	18	40
15	1962	0	45	20	1130	1	30	20	750	7	30	30	553	18	30
20	1934	0	40	25	1122	1	20	25	747	7	20	40	551	18	20
25	1908	0	35	30	1113	1	10	30	743	7	10	50	549	18	10
30	1883	0	30	35	1105	1	0	35	739	7	0	60	547	18	0
35	1860	0	25	40	1097	1	50	40	736	7	50	10	545	18	50
40	1837	0	20	45	1090	1	40	45	733	8	40	20	542	19	40
45	1816	0	15	50	1082	1	30	50	729	8	30	30	540	19	30
50	1796	0	10	55	1074	2	20	55	726	8	20	40	538	19	20
55	1777	0	5	5	1067	2	10	55	723	8	10	50	536	19	10
2 0	1758	0	178 0	10 0	1059	2	170 0	22 0	719	8	158 0	34 0	534	19	148 0
2 5	1740	0	55	10	1053	2	50	10	716	8	50	10	532	20	50
10	1723	0	50	15	1046	2	40	15	713	8	40	20	530	20	40
15	1707	0	45	20	1039	2	30	20	710	8	30	30	528	20	30
20	1691	0	40	25	1032	2	20	25	707	9	20	40	526	20	20
25	1676	0	35	30	1025	2	10	30	703	9	10	50	524	20	10
30	1661	0	30	35	1018	2	0	35	700	9	0	60	522	21	0
35	1647	0	25	40	1012	2	50	40	697	9	50	10	520	21	50
40	1633	0	20	45	1006	2	40	45	694	9	40	20	518	21	40
45	1620	0	15	50	999	2	30	50	691	9	30	30	516	21	30
50	1607	0	10	55	993	2	20	55	688	9	20	40	514	21	20
55	1594	0	5	5	987	2	10	55	685	9	10	50	512	22	10
3 0	1582	0	177 0	12 0	981	2	168 0	24 0	682	10	156 0	36 0	510	22	144 0
3 5	1570	0	55	10	975	2	50	10	679	10	50	10	508	22	50
10	1559	0	50	15	969	3	40	15	676	10	40	20	506	22	40
15	1547	0	45	20	963	3	30	20	673	10	30	30	504	22	30
20	1536	0	40	25	957	3	20	25	670	10	20	40	502	23	20
25	1526	0	35	30	952	3	10	30	668	10	10	50	500	23	10
30	1515	0	30	35	946	3	0	35	665	10	0	60	499	23	0
35	1505	0	25	40	941	3	50	40	662	11	50	10	497	23	50
40	1495	0	20	45	935	3	40	45	659	11	40	20	495	23	40
45	1485	0	15	50	930	3	30	50	656	11	30	30	493	24	30
50	1476	0	10	55	925	3	20	55	653	11	20	40	491	24	20
55	1466	0	5	5	919	3	10	55	651	11	10	50	489	24	10
4 0	1457	0	176 0	14 0	914	3	166 0	26 0	648	11	154 0	38 0	487	24	142 0
4 5	1448	0	55	10	909	3	50	10	645	11	50	10	486	25	50
10	1439	0	50	15	904	3	40	15	642	12	40	20	484	25	40
15	1431	0	45	20	899	3	30	20	640	12	30	30	482	25	30
20	1422	0	40	25	894	4	20	25	637	12	20	40	480	25	20
25	1414	0	35	30	889	4	10	30	634	12	10	50	478	25	10
30	1406	0	30	35	884	4	0	35	632	12	0	60	477	26	0
35	1398	0	25	40	880	4	50	40	629	12	50	10	475	26	50
40	1390	0	20	45	875	4	40	45	627	12	40	20	473	26	40
45	1383	0	15	50	870	4	30	50	624	13	30	30	471	26	30
50	1375	0	10	55	866	4	20	55	621	13	20	40	469	27	20
55	1368	0	5	5	861	4	10	55	619	13	10	50	468	27	10
5 0	1350	0	176 0	16 0	856	4	164 0	28 0	616	13	152 0	40 0	466	27	140 0
5 5	1353	0	55	10	852	4	50	10	614	13	50	10	464	27	50
10	1346	0	50	15	848	4	40	15	611	13	40	20	462	27	40
15	1339	0	45	20	843	5	30	20	609	14	30	30	461	28	30
20	1332	0	40	25	839	5	20	25	606	14	20	40	459	28	20
25	1326	0	35	30	835	5	10	30	604	14	10	50	457	28	10
30	1319	1	30	35	830	5	0	35	601	14	0	60	456	28	0
35	1312	1	25	40	826	5	50	40	599	14	50	10	454	29	50
40	1306	1	20	45	822	5	40	45	597	14	40	20	452	29	40
45	1300	1	15	50	818	5	30	50	594	15	30	30	451	29	30
50	1293	1	10	55	814	5	20	55	592	15	20	40	449	29	20
55	1287	1	5	5	810	5	10	55	589	15	10	50	447	30	10
6 0	1281	1	174 0	18 0	806	5	162 0	30 0	587	15	150 0	42 0	448	30	138 0
	Y ₁	X ₁	D		Y ₁	X ₁	D		Y ₁	X ₁	D		Y ₁	X ₁	D

$X_1 + X_2 + X_3 = X_4 \rightarrow x$ $Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y$ $x \pm y = Z$

Fig. 54

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-D

ℓ&d { same name + ℓ+d = D
contrary name + ℓ+d = D

D	X ₁	Y ₁		D	X ₁	Y ₁		D	X ₁	Y ₁		D	X ₂	Y ₂	
42 0	440	30	138 0	54 0	343	50	128 0	68 0	264	70	114 0	78 0	201	109	102 0
10	444	30	60	10	342	50	60	10	263	77	50	10	200	110	50
20	442	30	40	20	340	51	40	20	262	77	40	20	200	111	40
30	441	31	30	30	339	51	30	30	261	78	30	30	199	111	30
40	439	31	20	40	338	51	20	40	260	78	20	40	198	112	20
50	438	31	10	50	337	52	10	50	259	78	10	50	197	112	10
43 0	438	31	137 0	55 0	338	52	125 0	67 0	258	79	113 0	79 0	190	113	101 0
10	434	32	60	10	334	52	60	10	257	79	60	10	198	113	60
20	433	32	40	20	333	53	40	20	256	80	40	20	195	114	40
30	431	32	30	30	332	53	30	30	255	80	30	30	194	114	30
40	430	32	20	40	331	53	20	40	254	81	20	40	193	115	20
50	428	33	10	50	330	54	10	50	253	81	10	50	193	115	10
44 0	428	33	136 0	56 0	328	54	124 0	68 0	252	81	112 0	80 0	192	116	100 0
10	425	33	60	10	327	54	60	10	252	82	60	10	191	116	60
20	423	33	40	20	326	55	40	20	251	82	40	20	190	117	40
30	422	34	30	30	325	55	30	30	250	83	30	30	190	117	30
40	420	34	20	40	324	55	20	40	249	83	20	40	189	118	20
50	419	34	10	50	323	56	10	50	248	84	10	50	188	118	10
45 0	417	34	135 0	57 0	321	56	123 0	69 0	247	84	111 0	81 0	187	119	99 0
10	416	35	60	10	320	56	60	10	246	84	60	10	187	119	60
20	414	35	40	20	319	57	40	20	245	85	40	20	188	120	40
30	413	35	30	30	318	57	30	30	244	85	30	30	185	121	30
40	411	35	20	40	317	57	20	40	243	86	20	40	185	121	20
50	410	36	10	50	316	58	10	50	242	86	10	50	184	122	10
46 0	408	36	134 0	58 0	314	58	122 0	70 0	241	87	110 0	82 0	183	122	98 0
10	407	36	60	10	313	59	60	10	241	87	60	10	182	123	60
20	405	37	40	20	312	59	40	20	240	88	40	20	182	123	40
30	404	37	30	30	311	59	30	30	239	88	30	30	181	124	30
40	402	37	20	40	310	60	20	40	238	88	20	40	180	124	20
50	401	37	10	50	309	60	10	50	237	89	10	50	179	125	10
47 0	399	38	133 0	59 0	308	60	121 0	71 0	236	89	109 0	83 0	179	126	97 0
10	398	38	60	10	307	61	60	10	235	90	60	10	178	126	60
20	396	38	40	20	305	61	40	20	234	90	40	20	177	127	40
30	395	39	30	30	304	61	30	30	233	91	30	30	177	127	30
40	394	39	20	40	303	62	20	40	233	91	20	40	176	128	20
50	392	39	10	50	302	62	10	50	232	92	10	50	175	128	10
48 0	391	39	132 0	60 0	301	62	120 0	72 0	231	92	108 0	84 0	174	129	96 0
10	389	40	60	10	300	63	60	10	230	93	60	10	174	129	60
20	388	40	40	20	299	63	40	20	229	93	40	20	173	130	40
30	386	40	30	30	298	64	30	30	228	93	30	30	172	131	30
40	385	40	20	40	297	64	20	40	227	94	20	40	172	131	20
50	384	41	10	50	296	64	10	50	226	94	10	50	171	132	10
49 0	382	41	131 0	61 0	295	65	119 0	73 0	226	95	107 0	85 0	170	132	95 0
10	381	41	60	10	293	65	60	10	225	95	60	10	170	133	60
20	380	42	40	20	292	65	40	20	224	96	40	20	169	134	40
30	378	42	30	30	291	66	30	30	223	96	30	30	168	134	30
40	377	42	20	40	290	66	20	40	222	97	20	40	168	135	20
50	375	42	10	50	289	67	10	50	221	97	10	50	167	135	10
50 0	374	43	130 0	62 0	288	67	118 0	74 0	221	98	106 0	86 0	166	136	94 0
10	373	43	60	10	287	67	60	10	220	98	60	10	166	136	60
20	371	43	40	20	286	68	40	20	219	99	40	20	165	137	40
30	370	44	30	30	285	68	30	30	218	99	30	30	164	138	30
40	369	44	20	40	284	68	20	40	217	100	20	40	164	138	20
50	367	44	10	50	283	69	10	50	216	100	10	50	163	139	10
51 0	366	45	129 0	63 0	282	69	117 0	75 0	216	101	105 0	87 0	162	139	93 0
10	365	45	60	10	281	70	60	10	215	101	60	10	162	140	60
20	363	45	40	20	280	70	40	20	214	102	40	20	161	141	40
30	362	45	30	30	279	70	30	30	213	102	30	30	160	141	30
40	361	46	20	40	278	71	20	40	212	102	20	40	160	142	20
50	359	46	10	50	277	71	10	50	211	103	10	50	159	142	10
52 0	358	46	128 0	64 0	276	72	116 0	76 0	211	103	104 0	88 0	158	143	92 0
10	357	47	60	10	275	72	60	10	210	104	60	10	158	144	60
20	356	47	40	20	274	72	40	20	209	104	40	20	157	144	40
30	354	47	30	30	273	73	30	30	208	105	30	30	156	145	30
40	353	48	20	40	272	73	20	40	207	105	20	40	156	146	20
50	352	48	10	50	271	74	10	50	207	106	10	50	155	146	10
53 0	350	48	127 0	65 0	270	74	115 0	77 0	206	106	103 0	89 0	154	147	91 0
10	349	49	60	10	269	74	60	10	205	107	60	10	154	147	60
20	348	49	40	20	268	75	40	20	204	107	40	20	153	148	40
30	347	49	30	30	267	75	30	30	203	108	30	30	152	149	30
40	345	49	20	40	266	76	20	40	203	108	20	40	152	149	20
50	344	50	10	50	265	76	10	50	202	109	10	50	151	150	10
54 0	343	50	126 0	66 0	264	76	114 0	78 0	201	109	102 0	90 0	151	151	90 0

$X_1 + X_2 + X_3 = X_4 \rightarrow x$ $Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y$ $x \pm y = Z$

Fig. 55

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-h

h	X ₁ Y ₁	h	X ₂ Y ₂	h	X ₃ Y ₃	h	X ₄ Y ₄
0 0	- ∞	6 0	1919	18 0	2400	30 0	2623
5	+ 62	10	1931	10	2404	10	2631
10	363	20	1943	20	2408	20	2633
15	539	30	1954	30	2412	30	2636
20	664	40	1965	40	2416	40	2638
25	761	50	1976	50	2420	50	2641
30	840	35	1996	19 0	2424	10	2643
35	907	25	1997	10	2427	50	2645
40	965	20	2007	20	2431	40	2648
45	1016	15	2017	30	2435	30	2650
50	1062	10	2026	40	2439	20	2653
55	1103	5	2035	50	2443	10	2655
1 0	1141	359 0	8 0	2045	352 0	20 0	2446
5	1176	65	10	2054	60	10	2450
10	1208	50	20	2062	40	20	2454
15	1238	45	30	2071	30	30	2457
20	1266	40	40	2080	20	40	2461
25	1292	35	50	2088	10	50	2464
30	1317	30	9 0	2096	351 0	21 0	2468
35	1340	25	10	2104	50	10	2471
40	1363	20	20	2112	40	20	2475
45	1384	15	30	2120	30	30	2478
50	1404	10	40	2127	20	40	2482
55	1423	5	50	2135	10	50	2485
2 0	1442	358 0	10 0	2142	350 0	22 0	2489
5	1460	55	10	2149	50	10	2492
10	1477	50	20	2156	40	20	2495
15	1493	45	30	2163	30	30	2499
20	1509	40	40	2170	20	40	2502
25	1524	35	50	2177	10	50	2505
30	1539	30	11 0	2184	349 0	23 0	2508
35	1553	25	10	2190	50	10	2512
40	1567	20	20	2197	40	20	2515
45	1580	15	30	2203	30	30	2518
50	1593	10	40	2209	20	40	2521
55	1606	5	50	2216	10	50	2524
3 0	1618	357 0	12 0	2222	348 0	24 0	2527
5	1630	55	10	2228	50	10	2531
10	1642	50	20	2234	40	20	2534
15	1653	45	30	2239	30	30	2537
20	1664	40	40	2245	20	40	2540
25	1675	35	50	2251	10	50	2543
30	1685	30	13 0	2257	347 0	25 0	2546
35	1695	25	10	2262	50	10	2549
40	1705	20	20	2268	40	20	2552
45	1715	15	30	2273	30	30	2555
50	1725	10	40	2279	20	40	2558
55	1734	5	50	2284	10	50	2560
4 0	1743	356 0	14 0	2289	346 0	26 0	2563
5	1752	55	10	2294	50	10	2566
10	1761	50	20	2299	40	20	2569
15	1769	45	30	2305	30	30	2572
20	1778	40	40	2310	20	40	2575
25	1786	35	50	2315	10	50	2578
30	1794	30	15 0	2319	345 0	27 0	2580
35	1802	25	10	2324	50	10	2583
40	1810	20	20	2329	40	20	2586
45	1818	15	30	2334	30	30	2589
50	1825	10	40	2339	20	40	2591
55	1833	5	50	2343	10	50	2594
5 0	1840	355 0	16 0	2348	344 0	28 0	2597
5	1847	55	10	2352	50	10	2599
10	1854	50	20	2357	40	20	2602
15	1861	45	30	2361	30	30	2605
20	1868	40	40	2366	20	40	2607
25	1875	35	50	2370	10	50	2610
30	1882	30	17 0	2374	343 0	29 0	2613
35	1888	25	10	2379	50	10	2615
40	1895	20	20	2383	40	20	2618
45	1901	15	30	2387	30	30	2620
50	1907	10	40	2391	20	40	2623
55	1913	5	50	2396	10	50	2626
6 0	1919	354 0	18 0	2400	342 0	30 0	2628
	X ₁ Y ₁	h	X ₂ Y ₂	h	X ₃ Y ₃	h	X ₄ Y ₄

$$X_1 + X_2 + X_3 = X_4 \rightarrow x \quad Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y \quad x + y = Z$$

Fig. 56

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-h

h	X_1	Y_2	h	X_2	Y_3	h	X_3	Y_4	h	X_4	Y_5
42 0	2784	318 0	54 0	2907	306 0	66 0	3013	294 0	78 0	3108	282 0
10	2786	50	10	2909	50	10	3014	50	10	3110	50
20	2788	40	20	2910	40	20	3015	40	20	3111	40
30	2790	30	30	2912	30	30	3017	30	30	3112	30
40	2792	20	40	2913	20	40	3018	20	40	3114	20
50	2794	10	50	2915	10	50	3019	10	50	3115	10
43 0	2795	317 0	55 0	2916	305 0	67 0	3021	293 0	79 0	3116	281 0
10	2797	50	10	2918	50	10	3022	50	10	3117	50
20	2799	40	20	2920	40	20	3024	40	20	3119	40
30	2801	30	30	2921	30	30	3025	30	30	3120	30
40	2803	20	40	2923	20	40	3026	20	40	3121	20
50	2805	10	50	2924	10	50	3028	10	50	3123	10
44 0	2806	316 0	56 0	2926	304 0	68 0	3029	292 0	80 0	3124	280 0
10	2808	50	10	2927	50	10	3030	50	10	3125	50
20	2810	40	20	2929	40	20	3032	40	20	3126	40
30	2812	30	30	2930	30	30	3033	30	30	3128	30
40	2814	20	40	2932	20	40	3034	20	40	3129	20
50	2815	10	50	2933	10	50	3036	10	50	3130	10
45 0	2817	315 0	57 0	2935	303 0	69 0	3037	291 0	81 0	3131	279 0
10	2819	50	10	2936	50	10	3038	50	10	3133	50
20	2821	40	20	2938	40	20	3040	40	20	3134	40
30	2823	30	30	2939	30	30	3041	30	30	3135	30
40	2824	20	40	2941	20	40	3043	20	40	3137	20
50	2826	10	50	2942	10	50	3044	10	50	3138	10
46 0	2828	314 0	58 0	2944	302 0	70 0	3045	290 0	82 0	3139	278 0
10	2830	50	10	2945	50	10	3047	50	10	3140	50
20	2831	40	20	2947	40	20	3048	40	20	3142	40
30	2833	30	30	2948	30	30	3049	30	30	3143	30
40	2835	20	40	2950	20	40	3051	20	40	3144	20
50	2837	10	50	2951	10	50	3052	10	50	3146	10
47 0	2838	313 0	59 0	2953	301 0	71 0	3053	289 0	83 0	3147	277 0
10	2840	50	10	2954	50	10	3055	50	10	3148	50
20	2842	40	20	2956	40	20	3056	40	20	3149	40
30	2843	30	30	2957	30	30	3057	30	30	3151	30
40	2845	20	40	2959	20	40	3059	20	40	3152	20
50	2847	10	50	2960	10	50	3060	10	50	3153	10
48 0	2849	312 0	60 0	2961	300 0	72 0	3061	288 0	84 0	3154	276 0
10	2850	50	10	2963	50	10	3063	50	10	3156	50
20	2852	40	20	2964	40	20	3064	40	20	3157	40
30	2854	30	30	2966	30	30	3065	30	30	3158	30
40	2855	20	40	2967	20	40	3067	20	40	3160	20
50	2857	10	50	2969	10	50	3068	10	50	3161	10
49 0	2859	311 0	61 0	2970	299 0	73 0	3069	287 0	85 0	3162	275 0
10	2860	50	10	2972	50	10	3071	50	10	3163	50
20	2862	40	20	2973	40	20	3072	40	20	3165	40
30	2864	30	30	2974	30	30	3073	30	30	3166	30
40	2865	20	40	2976	20	40	3074	20	40	3167	20
50	2867	10	50	2977	10	50	3076	10	50	3168	10
50 0	2869	310 0	62 0	2979	298 0	74 0	3077	286 0	86 0	3170	274 0
10	2870	50	10	2980	50	10	3078	50	10	3171	50
20	2872	40	20	2982	40	20	3080	40	20	3172	40
30	2874	30	30	2983	30	30	3081	30	30	3173	30
40	2875	20	40	2984	20	40	3082	20	40	3175	20
50	2877	10	50	2986	10	50	3084	10	50	3176	10
51 0	2878	309 0	63 0	2987	297 0	75 0	3085	285 0	87 0	3177	273 0
10	2880	50	10	2989	50	10	3086	50	10	3179	50
20	2882	40	20	2990	40	20	3088	40	20	3180	40
30	2883	30	30	2992	30	30	3089	30	30	3181	30
40	2885	20	40	2993	20	40	3090	20	40	3182	20
50	2887	10	50	2994	10	50	3092	10	50	3184	10
52 0	2888	308 0	64 0	2996	296 0	76 0	3093	284 0	88 0	3185	272 0
10	2890	50	10	2997	50	10	3094	50	10	3186	50
20	2891	40	20	2999	40	20	3095	40	20	3187	40
30	2893	30	30	3000	30	30	3097	30	30	3189	30
40	2895	20	40	3001	20	40	3098	20	40	3190	20
50	2896	10	50	3003	10	50	3099	10	50	3191	10
53 0	2898	307 0	65 0	3004	295 0	77 0	3101	283 0	89 0	3192	271 0
10	2899	50	10	3006	50	10	3102	50	10	3194	50
20	2901	40	20	3007	40	20	3103	40	20	3195	40
30	2902	30	30	3008	30	30	3104	30	30	3196	30
40	2904	20	40	3010	20	40	3106	20	40	3197	20
50	2906	10	50	3011	10	50	3107	10	50	3199	10
54 0	2907	306 0	66 0	3013	294 0	78 0	3108	282 0	90 0	3200	270 0
X_1	Y_1	h	X_2	Y_2	h	X_3	Y_3	h	X_4	Y_4	h

$$X_1 + X_2 + X_3 = X_4 \rightarrow x \quad Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y \quad x \pm y = Z$$

Fig. 57

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-h

h	X_2, Y_2	h	X_2, Y_2	h	X_2, Y_2	h	X_2, Y_2
90 0	3200 270 0	102 0	3292 258 0	114 0	3387 246 0	126 0	3493 234 0
10	3201 50	10	3293 50	10	3389 50	10	3494 50
20	3203 40	20	3294 40	20	3390 40	20	3496 40
30	3204 30	30	3296 30	30	3392 30	30	3498 30
40	3205 20	40	3297 20	40	3393 20	40	3499 20
50	3206 10	50	3298 10	50	3394 10	50	3501 10
81 0	3208 269 0	103 0	3299 257 0	115 0	3396 245 0	127 0	3502 233 0
10	3209 50	10	3301 50	10	3397 50	10	3504 50
20	3210 40	20	3302 40	20	3399 40	20	3505 40
30	3211 30	30	3303 30	30	3400 30	30	3507 30
40	3213 20	40	3305 20	40	3401 20	40	3509 20
50	3214 10	50	3306 10	50	3403 10	50	3510 10
92 0	3215 268 0	104 0	3307 256 0	116 0	3404 244 0	128 0	3512 232 0
10	3216 50	10	3308 50	10	3406 50	10	3513 50
20	3218 40	20	3310 40	20	3407 40	20	3515 40
30	3219 30	30	3311 30	30	3408 30	30	3517 30
40	3220 20	40	3312 20	40	3410 20	40	3518 20
50	3221 10	50	3314 10	50	3411 10	50	3520 10
93 0	3223 267 0	105 0	3315 255 0	117 0	3413 243 0	129 0	3522 231 0
10	3224 50	10	3316 50	10	3414 50	10	3523 50
20	3225 40	20	3318 40	20	3416 40	20	3525 40
30	3227 30	30	3319 30	30	3417 30	30	3526 30
40	3228 20	40	3320 20	40	3418 20	40	3528 20
50	3229 10	50	3322 10	50	3420 10	50	3530 10
94 0	3230 266 0	106 0	3323 254 0	118 0	3421 242 0	130 0	3531 230 0
10	3232 50	10	3324 50	10	3423 50	10	3533 50
20	3233 40	20	3326 40	20	3424 40	20	3535 40
30	3234 30	30	3327 30	30	3426 30	30	3536 30
40	3235 20	40	3328 20	40	3427 20	40	3538 20
50	3237 10	50	3329 10	50	3428 10	50	3540 10
95 0	3238 265 0	107 0	3331 253 0	119 0	3430 241 0	131 0	3541 229 0
10	3239 50	10	3332 50	10	3431 50	10	3543 50
20	3240 40	20	3333 40	20	3433 40	20	3545 40
30	3242 30	30	3335 30	30	3434 30	30	3546 30
40	3243 20	40	3336 20	40	3436 20	40	3548 20
50	3244 10	50	3337 10	50	3437 10	50	3550 10
96 0	3246 264 0	108 0	3339 252 0	120 0	3439 240 0	132 0	3551 228 0
10	3247 50	10	3340 50	10	3440 50	10	3553 50
20	3248 40	20	3341 40	20	3441 40	20	3555 40
30	3249 30	30	3343 30	30	3443 30	30	3557 30
40	3251 20	40	3344 20	40	3444 20	40	3558 20
50	3252 10	50	3345 10	50	3446 10	50	3560 10
97 0	3253 263 0	109 0	3347 251 0	121 0	3447 239 0	133 0	3562 227 0
10	3254 50	10	3348 50	10	3449 50	10	3563 50
20	3256 40	20	3349 40	20	3450 40	20	3565 40
30	3257 30	30	3351 30	30	3452 30	30	3567 30
40	3258 20	40	3352 20	40	3453 20	40	3569 20
50	3260 10	50	3353 10	50	3455 10	50	3570 10
98 0	3261 262 0	110 0	3355 250 0	122 0	3456 238 0	134 0	3572 226 0
10	3262 50	10	3356 50	10	3458 50	10	3574 50
20	3263 40	20	3357 40	20	3459 40	20	3576 40
30	3265 30	30	3359 30	30	3461 30	30	3577 30
40	3266 20	40	3360 20	40	3462 20	40	3579 20
50	3267 10	50	3362 10	50	3464 10	50	3581 10
99 0	3269 261 0	111 0	3363 249 0	123 0	3465 237 0	135 0	3583 225 0
10	3270 50	10	3364 50	10	3467 50	10	3585 50
20	3271 40	20	3366 40	20	3468 40	20	3586 40
30	3272 30	30	3367 30	30	3470 30	30	3588 30
40	3274 20	40	3368 20	40	3471 20	40	3590 20
50	3275 10	50	3370 10	50	3473 10	50	3592 10
100 0	3276 260 0	112 0	3371 248 0	124 0	3474 236 0	136 0	3594 224 0
10	3277 50	10	3372 50	10	3476 50	10	3595 50
20	3279 40	20	3374 40	20	3477 40	20	3597 40
30	3280 30	30	3375 30	30	3479 30	30	3599 30
40	3281 20	40	3376 20	40	3480 20	40	3601 20
50	3283 10	50	3378 10	50	3482 10	50	3603 10
101 0	3284 259 0	113 0	3379 247 0	125 0	3484 235 0	137 0	3605 223 0
10	3285 50	10	3381 50	10	3485 50	10	3606 50
20	3286 40	20	3382 40	20	3487 40	20	3608 40
30	3288 30	30	3383 30	30	3488 30	30	3610 30
40	3289 20	40	3385 20	40	3490 20	40	3612 20
50	3290 10	50	3386 10	50	3491 10	50	3614 10
102 0	3292 258 0	114 0	3387 246 0	126 0	3493 234 0	138 0	3616 222 0
	X_2, Y_2		X_2, Y_2		X_2, Y_2		X_2, Y_2

$$X_1 + X_2 + X_3 = X_4 \rightarrow x \quad Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y \quad x \pm y = Z$$

Fig. 58

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-h

h	X ₁ Y ₁	h	X ₂ Y ₂	h	X ₃ Y ₃	h	X ₄ Y ₄
138 0	3616	222 0	3772	210 0	4000	198 0	4181
10	3618	50	3774	50	4004	50	4486
20	3620	40	3777	40	4009	40	4493
30	3622	30	3780	30	4013	30	4499
40	3623	20	3782	20	4017	20	4505
50	3625	10	3785	10	4021	10	4512
139 0	3627	221 0	3787	209 0	4026	197 0	4518
10	3629	50	3790	50	4030	50	4525
20	3631	40	3793	40	4034	40	4532
30	3633	30	3795	30	4039	30	4539
40	3635	20	3798	20	4043	20	4546
50	3637	10	3801	10	4048	10	4553
140 0	3639	220 0	3803	208 0	4052	196 0	4560
10	3641	50	3806	50	4057	50	4567
20	3643	40	3809	40	4061	40	4575
30	3645	30	3811	30	4066	30	4583
40	3647	20	3814	20	4071	20	4590
50	3649	10	3817	10	4076	10	4598
141 0	3651	219 0	3820	207 0	4081	195 0	4606
10	3653	50	3822	50	4085	50	4614
20	3655	40	3825	40	4090	40	4622
30	3657	30	3828	30	4095	30	4631
40	3659	20	3831	20	4101	20	4639
50	3661	10	3834	10	4106	10	4648
142 0	3663	218 0	3837	206 0	4111	194 0	4657
10	3665	50	3840	50	4116	50	4666
20	3667	40	3842	40	4121	40	4675
30	3669	30	3845	30	4127	30	4685
40	3671	20	3848	20	4132	20	4695
50	3673	10	3851	10	4138	10	4705
143 0	3675	217 0	3854	205 0	4143	193 0	4715
10	3678	50	3857	50	4149	50	4725
20	3680	40	3860	40	4155	40	4736
30	3682	30	3863	30	4161	30	4747
40	3684	20	3866	20	4168	20	4758
50	3688	10	3869	10	4172	10	4770
144 0	3688	216 0	3873	204 0	4178	192 0	4782
10	3690	50	3876	50	4184	50	4794
20	3693	40	3879	40	4191	40	4807
30	3695	30	3882	30	4197	30	4820
40	3697	20	3885	20	4203	20	4833
50	3699	10	3888	10	4210	10	4847
145 0	3701	215 0	3892	203 0	4216	191 0	4861
10	3703	50	3895	50	4223	50	4876
20	3706	40	3898	40	4230	40	4891
30	3708	30	3901	30	4237	30	4907
40	3710	20	3905	20	4244	20	4923
50	3712	10	3908	10	4251	10	4940
146 0	3715	214 0	3911	202 0	4258	190 0	4958
10	3717	50	3915	50	4265	50	4977
20	3719	40	3918	40	4273	40	4996
30	3721	30	3922	30	4280	30	5016
40	3724	20	3925	20	4288	20	5037
50	3726	10	3929	10	4296	10	5060
147 0	3728	213 0	3933	201 0	4304	189 0	5083
10	3731	50	3936	50	4312	50	5103
20	3733	40	3939	40	4320	40	5134
30	3735	30	3943	30	4329	30	5162
40	3738	20	3946	20	4338	20	5192
50	3740	10	3950	10	4346	10	5224
148 0	3743	212 0	3954	200 0	4355	188 0	5259
10	3745	50	3957	50	4365	50	5297
20	3747	40	3961	40	4374	40	5338
30	3750	30	3965	30	4383	30	5384
40	3752	20	3969	20	4393	20	5435
50	3755	10	3973	10	4403	10	5493
149 0	3757	211 0	3976	199 0	4414	187 0	5560
10	3759	50	3980	50	4424	50	5640
20	3762	40	3984	40	4435	40	5736
30	3764	30	3988	30	4446	30	5862
40	3767	20	3992	20	4457	20	6037
50	3769	10	3996	10	4469	10	6347
150 0	3772	210 0	4000	198 0	4481	186 0	∞
	X ₁ Y ₁	h	X ₂ Y ₂	h	X ₃ Y ₃	h	X ₄ Y ₄

$X_1 + X_2 + X_3 = X_4 \rightarrow x$ $Y_1 + Y_2 + Y_3 = Y_4 \rightarrow y$ $x \pm y = Z$

Fig. 59

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Azimuth Table-x.y

#	X_4	x	X_3	x	X_2	x	X_1	x	X_0	x	X_0	x	X_1	x	X_2	x	X_3	x	X_4		
$\frac{1}{2}$	Y_4	Y_3	Y_2	Y_1	Y_0	Y_0	Y_1	Y_2	Y_3	Y_4	Y_4	Y_3	Y_2	Y_1	Y_0	Y_0	Y_1	Y_2	Y_3	Y_4	
0.0	- 00	3.0	8119	8.0	5600	16.0	5928	21.0	5984	27.0	6107	33.0	6213	39.0	6308						
1	13341	8134	5605	5931	5986	6109	6214	6310	6381	6436	6491	6546	6601	6656	6711	6766	6821	6876	6931	6986	7041
2	3642	8147	5609	5934	5989	6112	6217	6313	6384	6439	6494	6549	6604	6659	6714	6769	6824	6879	6934	6989	7044
3	3816	8161	5614	5938	5993	6115	6220	6316	6387	6442	6497	6552	6607	6662	6717	6772	6827	6882	6937	6992	7047
4	3943	8174	5619	5942	5997	6118	6223	6319	6390	6445	6500	6555	6610	6665	6720	6775	6830	6885	6940	6995	7050
5	4040	8188	5624	5946	6001	6121	6226	6322	6393	6448	6503	6558	6613	6668	6723	6778	6833	6888	6943	6998	7053
6	4117	8199	5628	5950	6005	6124	6229	6325	6396	6451	6506	6561	6616	6671	6726	6781	6836	6891	6946	7001	7056
7	4186	8211	5633	5954	6009	6126	6231	6327	6398	6453	6508	6563	6618	6673	6728	6783	6838	6893	6948	7003	7058
8	4244	8222	5637	5958	6013	6129	6234	6330	6401	6456	6511	6566	6621	6676	6731	6786	6841	6896	6951	7006	7061
9	4296	8234	5642	5962	6017	6132	6237	6333	6404	6459	6514	6569	6624	6679	6734	6789	6844	6899	6954	7009	7064
10	4341	8245	5646	5966	6021	6135	6240	6336	6407	6462	6517	6572	6627	6682	6737	6792	6847	6902	6957	7012	7067
11	4382	8255	5651	5970	6025	6138	6243	6339	6410	6465	6520	6575	6630	6685	6740	6795	6850	6905	6960	7015	7070
12	4420	8266	5655	5974	6029	6141	6246	6342	6413	6468	6523	6578	6633	6688	6743	6798	6853	6908	6963	7018	7073
13	4455	8278	5659	5978	6033	6143	6249	6345	6420	6475	6530	6585	6640	6695	6750	6805	6860	6915	6970	7025	7080
14	4487	8290	5664	5982	6037	6145	6251	6347	6422	6477	6532	6587	6642	6697	6752	6807	6862	6917	6972	7027	7082
15	4517	8299	5669	5986	6041	6146	6252	6348	6423	6478	6533	6588	6643	6698	6753	6808	6863	6918	6973	7028	7083
16	4545	8308	5672	5989	6044	6147	6253	6349	6424	6479	6534	6589	6644	6699	6754	6809	6864	6919	6974	7029	7084
17	4571	8315	5676	5993	6047	6148	6254	6350	6425	6480	6535	6590	6645	6700	6755	6810	6865	6920	6975	7030	7085
18	4596	8324	5680	5996	6050	6149	6255	6351	6426	6481	6536	6591	6646	6701	6756	6811	6866	6921	6976	7031	7086
19	4620	8333	5685	5999	6053	6150	6256	6352	6427	6482	6537	6592	6647	6702	6757	6812	6867	6922	6977	7032	7087
20	4642	8341	5689	6002	6056	6151	6257	6353	6428	6483	6538	6593	6648	6703	6758	6813	6868	6923	6978	7033	7088
21	4663	8351	5693	6005	6059	6152	6258	6354	6429	6484	6539	6594	6649	6704	6759	6814	6869	6924	6979	7034	7089
22	4683	8359	5697	6008	6062	6153	6259	6355	6430	6485	6540	6595	6650	6705	6760	6815	6870	6925	6980	7035	7090
23	4703	8367	5701	6011	6064	6154	6260	6356	6431	6486	6541	6596	6651	6706	6761	6816	6871	6926	6981	7036	7091
24	4721	8376	5705	6014	6067	6155	6261	6357	6432	6487	6542	6597	6652	6707	6762	6817	6872	6927	6982	7037	7092
25	4739	8384	5708	6017	6070	6156	6262	6358	6433	6488	6543	6598	6653	6708	6763	6818	6873	6928	6983	7038	7093
26	4756	8391	5712	6020	6073	6157	6263	6359	6434	6489	6544	6599	6654	6709	6764	6819	6874	6929	6984	7039	7094
27	4772	8399	5716	6023	6076	6158	6264	6360	6435	6490	6545	6600	6655	6710	6765	6820	6875	6930	6985	7040	7095
28	4788	8407	5720	6026	6079	6159	6265	6361	6436	6491	6546	6601	6656	6711	6766	6821	6876	6931	6986	7041	7096
29	4803	8414	5724	6029	6082	6160	6266	6362	6437	6492	6547	6602	6657	6712	6767	6822	6877	6932	6987	7042	7097
30	4818	8422	5727	6032	6085	6161	6267	6363	6438	6493	6548	6603	6658	6713	6768	6823	6878	6933	6988	7043	7100
31	4832	8429	5731	6035	6088	6162	6268	6364	6439	6494	6549	6604	6659	6714	6769	6824	6879	6934	6989	7044	7101
32	4846	8436	5735	6038	6091	6163	6269	6365	6440	6495	6550	6605	6660	6715	6770	6825	6880	6935	6990	7045	7102
33	4859	8443	5739	6041	6094	6164	6270	6366	6441	6496	6551	6606	6661	6716	6771	6826	6881	6936	6991	7046	7103
34	4872	8450	5742	6044	6097	6165	6271	6367	6442	6497	6552	6607	6662	6717	6772	6827	6882	6937	6992	7047	7104
35	4885	8457	5746	6047	6100	6166	6272	6368	6443	6498	6553	6608	6663	6718	6773	6828	6883	6938	6993	7048	7105
36	4897	8463	5749	6050	6103	6167	6273	6369	6444	6499	6554	6609	6664	6719	6774	6829	6884	6939	6994	7049	7106
37	4909	8470	5753	6053	6106	6168	6274	6370	6445	6500	6555	6610	6665	6720	6775	6830	6885	6940	6995	7050	7107
38	4921	8476	5756	6056	6109	6169	6275	6371	6446	6501	6556	6611	6666	6721	6776	6831	6886	6941	6996	7051	7108
39	4932	8483	5760	6059	6112	6170	6276	6372	6447	6502	6557	6612	6667	6722	6777	6832	6887	6942	6997	7052	7109
40	4943	8489	5763	6062	6115	6171	6277	6373	6448	6503	6558	6613	6668	6723	6778	6833	6888	6943	6998	7053	7110
41	4954	8495	5767	6065	6118	6172	6278	6374	6449	6504	6559	6614	6669	6724	6779	6834	6889	6944	6999	7054	7111
42	4964	8502	5770	6068	6121	6173	6279	6375	6450	6505	6560	6615	6670	6725	6780	6835	6890	6945	7000	7055	7112
43	4975	8508	5774	6071	6124	6174	6280	6376	6451	6506	6561	6616	6671	6726	6781	6836	6891	6946	7001	7056	7113
44	4985	8514	5777	6074	6127	6175	6281	6377	6452	6507	6562	6617	6672	6727	6782	6837	6892	6947	7002	7057	7114
45	4994	8519	5780	6077	6130	6176	6282	6378	6453	6508	6563	6618	6673	6728	6783	6838	6893	6948	7003	7058	7115
46	5004	8525	5784	6080	6133	6177	6283	6379	6454	6509	6564	6619	6674	6729	6784	6839	6894	6949	7004	7059	7116
47	5013	8531	5787	6083	6136	6178	6284	6380	6455	6510	6565	6620	6675	6730	6785	6840	6895	6950	7005	7060	7117
48	5022	8537	5790	6086	6139	6179	6285	6381	6456	6511	6566	6621	6676	6731	6786	6841	6896	6951	7006	7061	7118
49	5031	8542	5794	6089	6142	6180	6286	6382	6457	6512	6567	6622	6677	6732	6787	6842	6897	6952	7007	7062	7119
50	5040	8548	5797	6092	6145	6181	6287	6383	6458	6513	6568	6623	6678	6733	6788	6843	6898	6953	7008	7063	7120
51	5049	8553	5800	6095	6148	6182	6288	6384	6459	6514	6569	6624	6679	6734	6789	6844	6899	6954	7009	7064	7121
52	5057	8559	5803	6098	6151	6183	6289	6385	6460	6515	6570	6625	6680	6735	6790	6845	6900	6955	7010	7065	7122
53	5066	8564	5806	6101	6154	6184	6290	6386	6461	6516	6571	6626	6681	6736	6791	6846	6901	6956	7011	7066	7123
54	5074	8569	5810	6104	6157	6185	6291	6387	6462	6517	6572	6627	6682	6737	6792	6847	6902	6957	7012	7067	7124
55	5082	8574	5813	6107	6160	6186	6292	6388	6463	6518	6573	6628	6683	6738	6793	6848	6903	6958	7013	7068	7125
56	5089	8579	5816	6110	6163	6187	6293	6389	6464	6519	6574	6629	6684	6739	6794	6849	6904	6959	7014	7069	7126
57	5097	8585	5819	6113	6166	6188	6294	6390	6465	6520	6575	6630	6685	6740	6795	6850	6905	6960	7015	7070	7127
58	5105	8590	5822	6116	6169	6189	6295	6391	6466	6521	6576	6631	6686	6741	6796	6851	6906</				

Azimuth Table-x.y

#	X ₁	#	X ₁	#	X ₁	#	X ₁	#	X ₁	#	X ₁	#	X ₁	#	X ₁	#	X ₁
y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁	y	Y ₁
45 0	6100	81 0	6192	57 0	6537	63 0	6933	69 0	7316	75 0	7692	81 0	7200	87 0	7681		
1	6102		6193		6539		6935		7318		7694		7202		7683		
2	6103		6194		6540		6936		7319		7695		7203		7684		
3	6104		6195		6541		6937		7320		7696		7204		7685		
4	6105		6196		6542		6938		7321		7697		7205		7686		
5	6106		6197		6543		6939		7322		7698		7206		7687		
6	6107		6198		6544		6940		7323		7699		7207		7688		
7	6108		6199		6545		6941		7324		7700		7208		7689		
8	6109		6200		6546		6942		7325				7209		7690		
9	6110		6201		6547		6943		7326				7210		7691		
0	6111		6202		6548		6944		7327				7211		7692		
1	6112		6203		6549		6945		7328				7212		7693		
2	6113		6204		6550		6946		7329				7213		7694		
3	6114		6205		6551		6947		7330				7214		7695		
4	6115		6206		6552		6948		7331				7215		7696		
5	6116		6207		6553		6949		7332				7216		7697		
6	6117		6208		6554		6950		7333				7217		7698		
7	6118		6209		6555		6951		7334				7218		7699		
8	6119		6210		6556		6952		7335				7219		7700		
9	6120		6211		6557		6953		7336				7220				
0	6121		6212		6558		6954		7337				7221				
1	6122		6213		6559		6955		7338				7222				
2	6123		6214		6560		6956		7339				7223				
3	6124		6215		6561		6957		7340				7224				
4	6125		6216		6562		6958		7341				7225				
5	6126		6217		6563		6959		7342				7226				
6	6127		6218		6564		6960		7343				7227				
7	6128		6219		6565		6961		7344				7228				
8	6129		6220		6566		6962		7345				7229				
9	6130		6221		6567		6963		7346				7230				
0	6131		6222		6568		6964		7347				7231				
1	6132		6223		6569		6965		7348				7232				
2	6133		6224		6570		6966		7349				7233				
3	6134		6225		6571		6967		7350				7234				
4	6135		6226		6572		6968		7351				7235				
5	6136		6227		6573		6969		7352				7236				
6	6137		6228		6574		6970		7353				7237				
7	6138		6229		6575		6971		7354				7238				
8	6139		6230		6576		6972		7355				7239				
9	6140		6231		6577		6973		7356				7240				
0	6141		6232		6578		6974		7357				7241				
1	6142		6233		6579		6975		7358				7242				
2	6143		6234		6580		6976		7359				7243				
3	6144		6235		6581		6977		7360				7244				
4	6145		6236		6582		6978		7361				7245				
5	6146		6237		6583		6979		7362				7246				
6	6147		6238		6584		6980		7363				7247				
7	6148		6239		6585		6981		7364				7248				
8	6149		6240		6586		6982		7365				7249				
9	6150		6241		6587		6983		7366				7250				
0	6151		6242		6588		6984		7367				7251				
1	6152		6243		6589		6985		7368				7252				
2	6153		6244		6590		6986		7369				7253				
3	6154		6245		6591		6987		7370				7254				
4	6155		6246		6592		6988		7371				7255				
5	6156		6247		6593		6989		7372				7256				
6	6157		6248		6594		6990		7373				7257				
7	6158		6249		6595		6991		7374				7258				
8	6159		6250		6596		6992		7375				7259				
9	6160		6251		6597		6993		7376				7260				
0	6161		6252		6598		6994		7377				7261				
1	6162		6253		6599		6995		7378				7262				
2	6163		6254		6600		6996		7379				7263				
3	6164		6255		6601		6997		7380				7264				
4	6165		6256		6602		6998		7381				7265				
5	6166		6257		6603		6999		7382				7266				
6	6167		6258		6604		7000		7383				7267				
7	6168		6259		6605				7384				7268				
8	6169		6260		6606				7385				7269				
9	6170		6261		6607				7386				7270				
0	6171		6262		6608				7387				7271				
1	6172		6263		6609				7388				7272				
2	6173		6264		6610				7389				7273				
3	6174		6265		6611				7390				7274				
4	6175		6266		6612				7391				7275				
5	6176		6267		6613				7392				7276				
6	6177		6268		6614				7393				7277				
7	6178		6269		6615				7394				7278				
8	6179		6270		6616				7395				7279				
9	6180		6271		6617				7396				7280				
0	6181		6272		6618				7397				7281				
1	6182		6273		6619				7398				7282				
2	6183		6274		6620				7399				7283				
3	6184		6275		6621				7400				7284				
4	6185		6276		6622								7285				
5	6186		6277		6623								7286				
6	6187		6278		6624								7287				
7	6188		6279		6625								7288				
8	6189		6280		6626								7289				
9	6190		6281		6627								7290				
0	6191		6282		6628								7291				
1	6192		6283		6629								7292				
2	6193		6284		6630								7293				
3	6194		6285		6631								7294				
4	6195		6286		6632								7295				
5	6196		6287		6633								7296				
6	6197		6288		6634								7297				
7	6198		6289		6635								7298				
8	6199		6290		6636								7299				
9	6200		6291		6637								7300				
0	6201		6292		6638								7301				
1	6202		6293		6639								7302				
2	6203		6294		6640								7303				
3	6204		6295		6641								7304				
4	6205		6296		6642								7305				
5	6206		6297		6643								7306				
6	6207		6298		6644								7307				
7	6208		6299		6645								7308				
8	6209		6300		6646								7309				
9	6210		6301		6647								7310				
0	6211		6302		6648								7311				
1	6212																

10 June 1956
Nautical Almanac

Lunar Age 1.1

☉ Sun				Planet				☾ Moon				
U	E _s	d	P.P. of d	U	E _r	d	P.P.	U	E _t	Tr.	13 40	P.P.
h m s	° ' "	h m s	h m s	h m s	° ' "	h m s	h m s	h m s	° ' "	h m s	h m s	h m s
0 12 0 47	N22 59.7	0 0 0.0	0 0 0.0	♁ Venus	Tr. 13 16	0 10 53 43	N21 0.8	0 10 53 43	N21 0.8	20 58.6	1 3 0.1	2 5 2
2 36	23 0.1	10 0	1 1	h m s	h m s	h m s	h m s	1 51 13	56.3	49 58	3 8 3	4 10 3
4 45	0.5	20 1	1 1	2 41 40	N23 55.2	10 2 1	54.3	2 49 43	54.0	47 28	5 13 4	6 15 5
6 44	0.9	30 1	1 1	4 42 8	54.3	20 5 2	53.3	3 46 13	47.0	44 58	7 18 6	8 20 7
8 43	1.2	40 1	1 1	6 42 36	52.4	30 7 2	52.4	4 43 43	44.5	42 28	9 23 8	10 25 0.9
10 42	1.6	50 2	2 2	8 43 5	51.4	40 9 3	51.4	5 41 14	37.0	39 59	11 28 1.0	12 30 0
12 12 0 41	N23 2.0	1 0 0.2	1 0 0.2	10 43 33	50.5	50 12 4	50.5	6 37 30	34.4		13 33 1	14 35 2
14 40	2.4	10 2	2 2	12 10 44 1	N23 49.5	1 0 14 0.5	49.5	7 34 15	31.0		15 29 3	16 40 4
16 39	2.7	20 3	3 3	14 29	48.5	10 16 6	48.5	8 31 15	26.4		17 43 5	18 45 6
18 38	3.1	30 3	3 3	16 44 50	47.6	20 19 7	47.6	9 28 49	20.9		19 48 6	20 50 7
20 37	3.5	40 3	3 3	18 45 26	46.6	30 21 7	46.6	10 26 49	15.2		21 51 1.9	22 55 2.0
22 36	3.8	50 4	4 4	20 45 55	45.6	40 23 8	45.6	11 24 34	9.4		23 58 2.1	24 60 1
24 12 0 35	N23 4.2	2 0 0.4	2 0 0.4	22 46 23	44.7	1 50 26 0.9	44.7	12 22 20	6.4		25 65 3	26 68 3
				24 10 46 62	N23 43.7	2 0 28 1.0	43.7	13 19 56	3.4		27 68 3	28 70 4
								14 17 34	2.0		29 73 5	30 75 2.6
								15 15 16	1.5			
								16 14 2	1.2			
								17 11 35	1.0			
								18 10 22	0.8			
								19 8 9	0.7			
								20 7 55	0.6			
								21 6 42	0.5			
								22 5 29	0.4			
								23 4 16	0.3			
								24 3 3	0.2			
								25 2 10	0.1			
								26 1 50	0.0			
								27 0 38	0.0			
								28 0 25	0.0			
								29 0 12	0.0			
								30 0 0	0.0			
								31 0 0	0.0			
								32 0 0	0.0			
								33 0 0	0.0			
								34 0 0	0.0			
								35 0 0	0.0			
								36 0 0	0.0			
								37 0 0	0.0			
								38 0 0	0.0			
								39 0 0	0.0			
								40 0 0	0.0			
								41 0 0	0.0			
								42 0 0	0.0			
								43 0 0	0.0			
								44 0 0	0.0			
								45 0 0	0.0			

Fig. 62

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

14 February 1956
Nautical Almanac

Lunar Age 2.1

☉ Sun					Planet					☾ Moon				
U	E _s	d	P.P. OF d		U	E _p	d	P.P.		U	E _t	d	P.P.	
h m a	' "	' "	h m	' "	h m a	' "	h m a	' "	h m	' "	' "	h m	' "	' "
0 11 45 41	S13	26.0	0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
2 41		24.3	10	1										
4 41		22.6	20	3										
6 42		20.9	30	4										
8 42		19.3	40	6										
10 42		17.6	50	7										
12 11 45 42	S13	15.9	1	0	0.9									
14 42		14.2	10	1.0										
16 42		12.5	20	1										
18 42		10.8	30	3										
20 43		9.1	40	4										
22 43		7.4	50	6										
24 11 45 43	S13	5.7	2	0	1.7									
	S.D. 16 14)													
No.	* Star	E _s	U = 0 ^h		♀ Venus					♁ Mars				
		' "	' "	' "	h m a	' "	h m a	' "	h m a	' "	h m a	' "	h m a	' "
1	Polaris	7 39 13	N 89	3.9	0 16 14 20	S 22	58.0	0 0 0 0.0	0 16 14 20	S 22	58.0	0 0 0 0.0	0 16 14 20	S 22
2	Kochab	18 41 12	74	19.7	2 26		59.1	10 1 0	2 26		59.1	10 1 0	2 26	
3	Dubhe	22 30 55	61	59.0	4 31		59.4	20 1 1	4 31		59.4	20 1 1	4 31	
4	β Cassiop.	9 25 12	58	54.7	6 37		22 59.7	30 2 1	6 37		22 59.7	30 2 1	6 37	
5	Mérah	22 32 45	56	36.8	8 42		23 0.1	40 2 1	8 42		23 0.1	40 2 1	8 42	
6	Alioth	20 39 52	N 56	11.5	10 48		0.4	0 50 3 1	10 48		0.4	0 50 3 1	10 48	
7	Schedir	8 54 0	56	18.1	12 16 14 53	S 23	0.7	1 0 3 0.2	12 16 14 53	S 23	0.7	1 0 3 0.2	12 16 14 53	S 23
8	Mizar	20 9 49	55	8.9	14 14 59		1.0	10 4 2	14 14 59		1.0	10 4 2	14 14 59	
9	α Perseid	6 10 48	49	42.6	16 15 4		1.3	20 4 2	16 15 4		1.3	20 4 2	16 15 4	
10	β Benetnasch	19 46 10	49	31.5	18 10		1.6	30 5 2	18 10		1.6	30 5 2	18 10	
11	Capella	4 18 31	N 45	57.5	20 15		1.9	40 5 3	20 15		1.9	40 5 3	20 15	
12	Deneb	12 52 5	45	7.3	22 21		2.2	1 50 6 3	22 21		2.2	1 50 6 3	22 21	
13	Vega	14 56 34	38	44.3	24 16 15 26	S 23	2.5	2 0 6 0.3	24 16 15 26	S 23	2.5	2 0 6 0.3	24 16 15 26	S 23
14	Castor	2 0 10	31	59.1	♃ Jupiter					♄ Saturn				
15	Alpheratz	9 25 54	28	51.0	h m a	' "	h m a	' "	h m a	' "	h m a	' "	h m a	' "
16	Pollux	1 49 20	N 28	7.9	0 23 34 11	N 13	39.7	0 0 0 0.0	0 23 34 11	N 13	39.7	0 0 0 0.0	0 23 34 11	N 13
17	α Cor. Bor.	17 59 10	26	51.4	2 34		39.9	10 2 0	2 34		39.9	10 2 0	2 34	
18	Arcturus	19 18 20	19	24.3	4 34 56		40.2	20 4 0	4 34 56		40.2	20 4 0	4 34 56	
19	Aldebaran	4 58 35	16	25.3	6 35 18		40.4	30 5 1	6 35 18		40.4	30 5 1	6 35 18	
20	Markab	10 29 26	14	58.2	8 35 40		40.6	40 7 1	8 35 40		40.6	40 7 1	8 35 40	
21	Denebola	21 45 9	N 14	48.8	10 36 3		40.9	0 50 9 1	10 36 3		40.9	0 50 9 1	10 36 3	
22	α Ophiuch	15 59 6	12	35.3	12 23 36 25	N 13	41.1	1 0 11 0.1	12 23 36 25	N 13	41.1	1 0 11 0.1	12 23 36 25	N 13
23	Regulus	23 25 56	8	10.7	14 36 47		41.3	10 13 1	14 36 47		41.3	10 13 1	14 36 47	
24	Alhair	13 43 22	8	45.0	16 37 9		41.6	20 15 1	16 37 9		41.6	20 15 1	16 37 9	
25	Betelgeuse	3 39 11	7	23.9	18 32		41.8	30 17 2	18 32		41.8	30 17 2	18 32	
26	Bellatrix	4 9 12	N 6	18.6	20 37 54		42.0	40 18 2	20 37 54		42.0	40 18 2	20 37 54	
27	Procyon	1 54 58	N 5	20.1	22 38 16		42.3	1 50 20 2	1 54 58		42.3	1 50 20 2	1 54 58	
28	Rigel	4 19 33	9	8 15.2	24 23 38 38	N 13	42.5	2 0 22 0.2	4 19 33		42.5	2 0 22 0.2	4 19 33	
29	α Hydrae	0 6 32	8	28.3	♃ Jupiter					♄ Saturn				
30	Spica	20 9 6	10	56.1	h m a	' "	h m a	' "	h m a	' "	h m a	' "	h m a	' "
31	Sirius	2 48 46	S 16	39.5	0 17 29 51	S 18	35.0	0 0 0 0.0	0 17 29 51	S 18	35.0	0 0 0 0.0	0 17 29 51	S 18
32	β Cell	8 50 37	18	13.7	2 30 10		35.0	10 2 0	2 30 10		35.0	10 2 0	2 30 10	
33	Antares	17 5 17	26	20.2	4 29		35.0	20 3 0	4 29		35.0	20 3 0	4 29	
34	♁ Sagittarii	14 39 28	26	21.1	6 30 47		35.1	30 5 0	6 30 47		35.1	30 5 0	6 30 47	
35	Fomalhaut	10 36 47	29	51.3	8 31 6		35.1	40 6 0	8 31 6		35.1	40 6 0	8 31 6	
36	λ Scorpii	16 1 22	8	37 4.3	10 25		35.1	0 50 8 0	10 25		35.1	0 50 8 0	10 25	
37	Canopus	3 9 0	52	40.6	12 17 31 44	S 18	35.2	1 0 10 0.0	3 9 0		35.2	1 0 10 0.0	3 9 0	
38	α Pavonis	13 9 50	56	52.5	14 32 3		35.2	10 11 0	13 9 50		35.2	10 11 0	13 9 50	
39	Achernar	7 55 56	57	27.0	16 21		35.2	20 13 0	7 55 56		35.2	20 13 0	7 55 56	
40	β Crucis	20 46 49	59	26.9	18 40		35.2	30 14 0	20 46 49		35.2	30 14 0	20 46 49	
41	β Centauri	19 31 15	8	60 9.6	20 32 59		35.3	40 16 0	19 31 15		35.3	40 16 0	19 31 15	
42	α Centauri	18 55 22	60	39.2	22 33 18		35.3	1 50 17 0	18 55 22		35.3	1 50 17 0	18 55 22	
43	α Crucis	21 7 48	62	51.3	24 17 33 37	S 18	35.3	2 0 19 0.0	21 7 48		35.3	2 0 19 0.0	21 7 48	
44	α Tri. Aust.	16 47 59	68	56.8	Planet					Planet				
45	β Carinae	0 19 13	8	69 32.3										
	Ra	h m a	d		R.A.	d	Mag.	H.P.	S.D.	R.A.	d	Mag.	H.P.	S.D.
		9 32 0			0 13 N 0 48	-3.6	0.1	7		17 18 S 22 59	+1.4	0.1	3	
					9 58 N 13 40	-2.1	0.0	21		16 2 S 16 35	+0.7	0.0	7	
					20 4 S 18 52	+0.5	0.2	4						

Fig. 63

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Problem

At 07^h 40^m p.m. on 14 February 1956, a navigator observed the compass bearing of Jupiter as N 72°2 E in D.R.P. 32°16'S, 41°52 E. What was the deviation of this compass?

Where; Chronometer time was 04h 26m 08s, variation 18°8 W, and chronometer error ⊕ 26^m - 32^s

(Ans. Deviation = 14°5 E, Ref. x = 60°8, y = 7°1

Navigation by lines of position

The line of position is one on a point of which the ship can be presumed to be located.

A line of position is a segment of a great circle, but invisible plotting on nautical charts, the segment is so short that it may be plotted as a straight line or rhumb line on a mercator chart.

Geographical position of a celestial body

The position on the earth where a navigator observes a celestial body exactly in the zenith is called its geographical position.

In figure 64, p = north pole, p' = south pole, $\overline{qq'}$ = plane of the equator, C = center of the earth, X = celestial body, x = geographical position of the celestial body x (*) Because strictly speaking the earth is not a perfect sphere, a straight line through X and x does not pass the earth's center C. This straight line intersects the plane of equator $\overline{qq'}$ at C'.

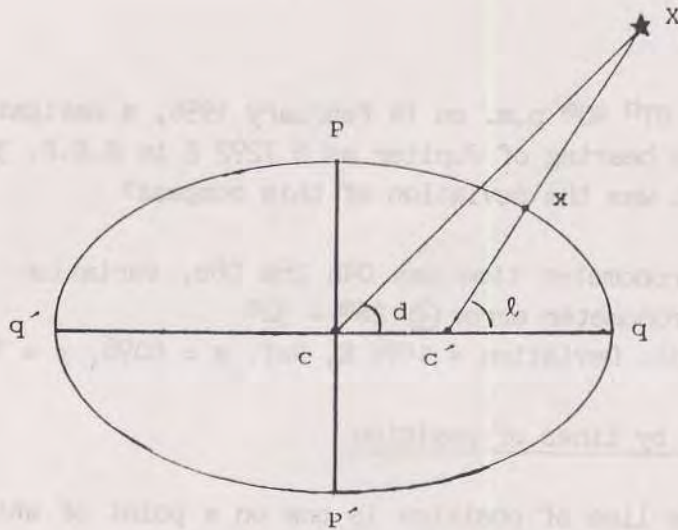


Fig. 64 Geographical Position

So, $\angle XC'_q$ is the latitude of the celestial body's geographical position (x) and the included angle between \overline{XC} and C_q ($\angle XC_q$) is the declination of X .

From Figure 64, $\angle XC'_q = \angle XC_q + \angle CXC'$
 $\angle CXC'$ is negligible (e.g. in the case of the Moon, $\angle CXC' = 0.2'$ only), then $\angle XC'_q = \angle XC_q$

$$\begin{aligned} \angle XC'_q &\rightarrow \text{Latitude of geographical position} + lx, \\ \angle XC_q &\rightarrow \text{Declination} \quad dx \\ \therefore lx &= dx \end{aligned}$$

Thus the intersection obtained by the earth's surface and the straight line connecting the center of the earth (c) with the center of celestial body (X) is the geographical position (x) of the celestial body (X) and the equation $\angle XC'_q = \angle XC_q$ is used with the assumption that the earth as a perfect sphere.

In Figure 65, g = position of Greenwich, $\widehat{pgqp'}$ = prime meridian, $\widehat{PGQP'}$ = hour circle corresponding to $\widehat{pgqp'}$.

$\angle QQ'$ is the Greenwich Hour Angle (G.H.A.) of celestial body X, and $\angle qq'$ on the earth's surface is the longitude of celestial body X at its geographical position (in this case the longitude is westerly).

The western longitude of geographical position (LWx) is equivalent to the Greenwich Hour Angle of celestial body X ($= \text{hgx}$)

$$\text{LWx} = \angle \text{hgx}$$

Therefore if a navigator knows a celestial body's declination (available by nautical almanac) and its Greenwich Hour Angle (available by nautical almanac and astronomical navigation table $h = U + E$), he can decide its geographical position on the earth's surface.

Ref. LWx = West longitude of Geographical Position
hgx = Greenwich Hour Angle

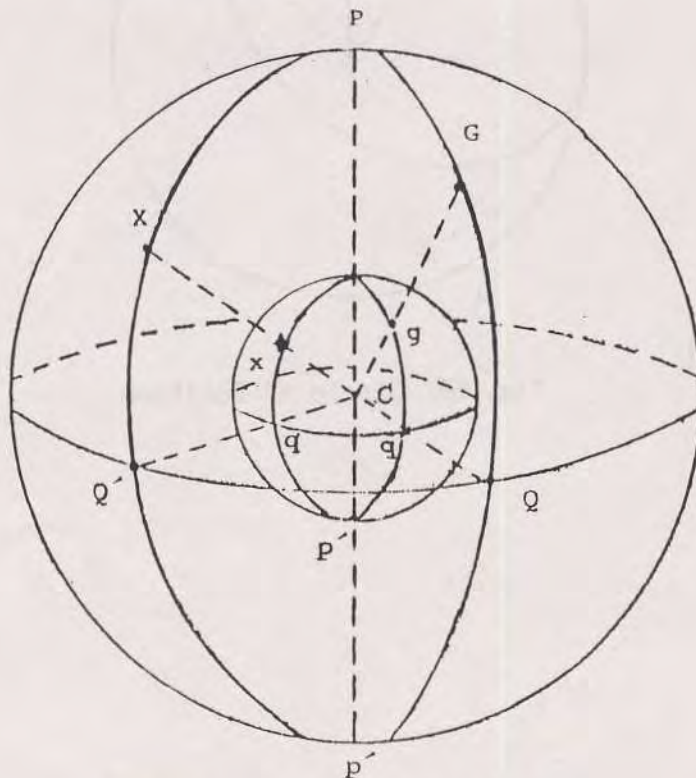


Fig. 65 Geographical Position

Circle of position
In Figure 66,

C = center of the earth, p = north pole, x = geographical position of celestial body X (★), O = observer's position
p' = south pole, X = celestial body, Z = zenith

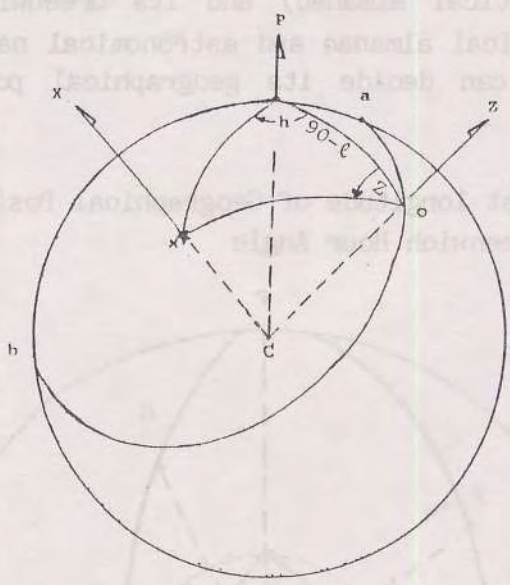


Fig. 66 Circle of Position

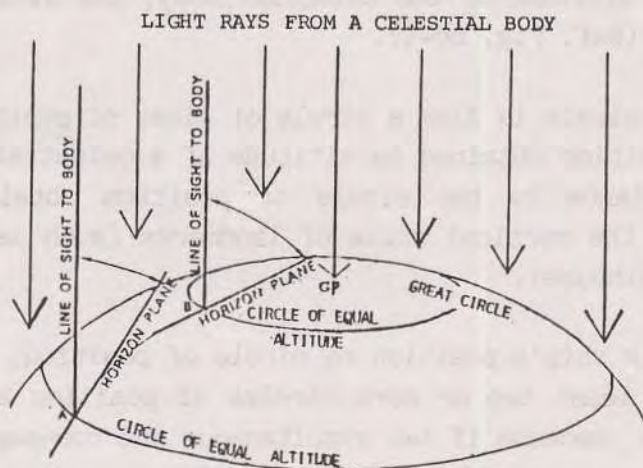


Fig. 66-1 Parallel light rays

Spherical triangle (pxo) on the earth's surface is similar or symmetric to a spherical triangle on the celestial sphere.

- So,
- px = polar distance (p)
 - xo = zenith distance (z) \rightarrow (90° - Alt.)
 - po = co-latitude (90° - ℓ)
 - \angle opx = local hour angle (h)
 - \angle pox = Azimuth (z)

If a navigator observes the altitude of celestial body X, he can obtain the zenith distance z ($= 90^\circ - \text{Alt.}$), and he can have a circle of position given by the celestial body X, with point x as its center and zenith distance z as its radius.

This circle of position of the celestial sphere corresponds to a circle of position on the earth.

In Figure 66, the circle of \widehat{aob} is the circle of position. If a navigator on any point of this circle of position observes the altitude of the celestial body, the altitude should be $(90^\circ - Z)$ (Ref. Fig. 66-1).

This circle is also a circle of lines of position and the circle of position obtained by altitude of a celestial body has a close resemblance to the circle of position obtained by the method using the vertical angle of landmarks (such as a mountain top or a lighthouse).

To fix ship's position by circle of position, a navigator must have at least two or more circles of position available at the same time, because if two simultaneous and non-parallel lines of position are available, the only position that satisfies the requirements of being on both lines at the same time is the intersection of the two lines.

We have two intersections (O and O' in Figure 67) given by two circles of position obtained by observing two celestial bodies (X and X' in Figure 24). But actually the distance between the two positions O and O' is hundreds or thousands of nautical miles and a navigator knows that his dead reckoning position is near true position. Therefore it is not difficult to distinguish true intersection, as his location, from the false one,

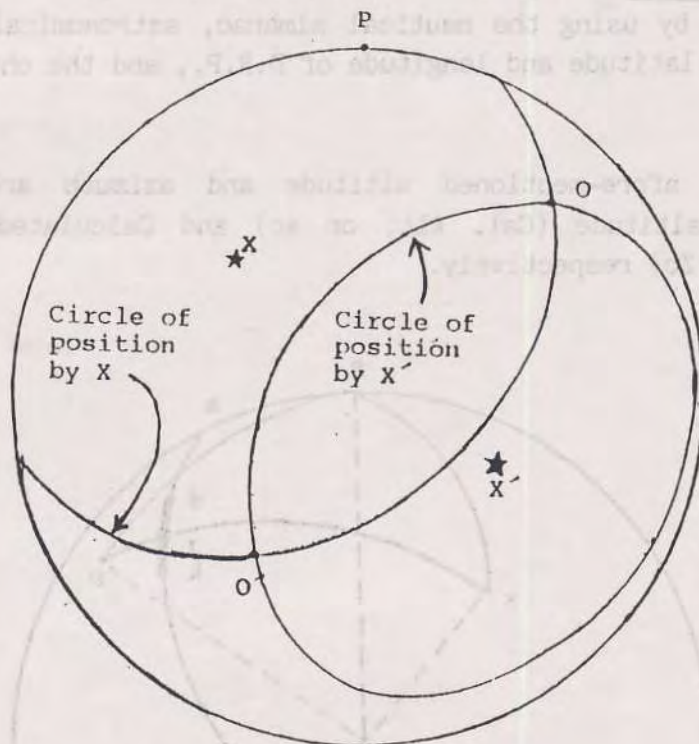


Fig. 67 Two intersections by two circles of position

How to draw lines of position on Mercator chart

In Figure 68,

- p = pole, x = geographical position of celestial body X,
- D = observer's D.R.P. \widehat{ab} = circle of position, \widehat{HJK} = minute particle on circle of position (\widehat{ab}) in the vicinity of D.R.P. (D).

If the navigator's location is in D.R.D. (D) at a particular time, he can calculate a celestial body's altitude and its azimuth by using the nautical almanac, astronomical navigation tables latitude and longitude of D.R.P., and the chronometer time.

The afore-mentioned altitude and azimuth are called Calculated altitude (Cal. Alt. or ac) and Calculated Azimuth (Cal. az or Zc) respectively.

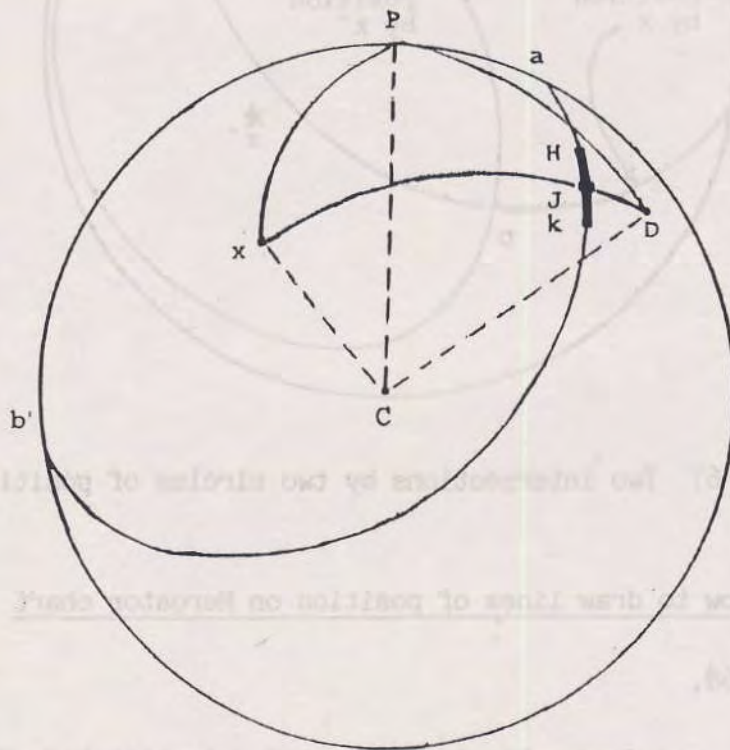


Fig. 68 Line of position

The altitude ($90^\circ - \widehat{xJ}$, in Figure 68) observed by a navigator with altitude corrections is called true altitude (True Alt. or at)

According to Figure 25,

$$\widehat{DJ} = \widehat{xD} - \widehat{xJ} = ac - at$$

\widehat{DJ} is called intercept (Inter, or I) and point J is called Extremity of Intercept. In figure 25, D.R.P. (D) exists outside the circle of position \widehat{aJb} , but in other cases, D can be inside the circle of position \widehat{aJb} .

To distinguish whether D is outside or inside the circle of position \widehat{aJb} , it is very useful to designate intercept plus \oplus or minus \ominus , For this reason we must give the definition of Intercept (I) as follows;

$$I = at - ac$$

In Figure 68,

1. Extremity of Intercept (J) is located on the great circle passing through D.R.P. (D) and geographical position (x), that is, azimuth line from D.R.P. (D) to geographical position (x).

So when I (= at - ac) is plus \oplus , Extremity of Intercept exists towards the celestial body from D.R.P. (D), and

when I (= at - ac) is minus \ominus , Extremity of Intercept is on the opposite side of the celestial body from D.R.P. (D).

2. Angular distance \widehat{DJ} , that is, distance from D.R.P. (D) to extremity is equal to the value of Intercept. Value of Intercept should be expressed in nautical minutes (')

3. \widehat{DJ} and \widehat{HJK} , that is, azimuth line from D.R.P. (D) to geographical position (x) and circle of position (minute particle of circle of position to be exact) intersect at a right angle (90°) at Extremity of Intercept, because geographical position (x) is the center of the circle of position, \widehat{xJ} as its radius.

Therefore navigators can draw lines of position on mercator charts using the following procedure.

1. Draw the azimuth line through D.R.P. (D) by Calculated Azimuth (obtainable from nautical almanac and astronomical calculation tables);
2. To set up Extremity of Intercept,
 - a. When Intercept (I) is positive \oplus , draw a straight line from D.R.P. (D) towards the celestial body (same direction as Calculated Azimuth Z_c), and mark the distance from D.R.P. (D) according to the value of Intercept
 - b. When Intercept (I) is negative \ominus , Draw a straight line from D.R.P. (D) to the opposite side from the celestial body (contrary direction to Calculated Azimuth Z_c), and mark the distance from D.R.P. (D) according to value of Intercept (I) on this straight line to set up the Extremity of Intercept.

3. To draw line of position. The straight line passing through Extremity of Intercept (J) which intersects the azimuth line is the line of position (see Fig. 26).

To fix position, the navigator observes two or more celestial bodies, to obtain lines of position and an intersection at his location. When he measures the altitude of a celestial body by sextant, it is very important to select navigational stars.

It is desirable that the directions of the celestial bodies of which he intends to observe the altitudes intersect at right angles, or at a 30° , 40° , 60° and it is most undesirable that directions of celestial bodies be parallel or nearly parallel.

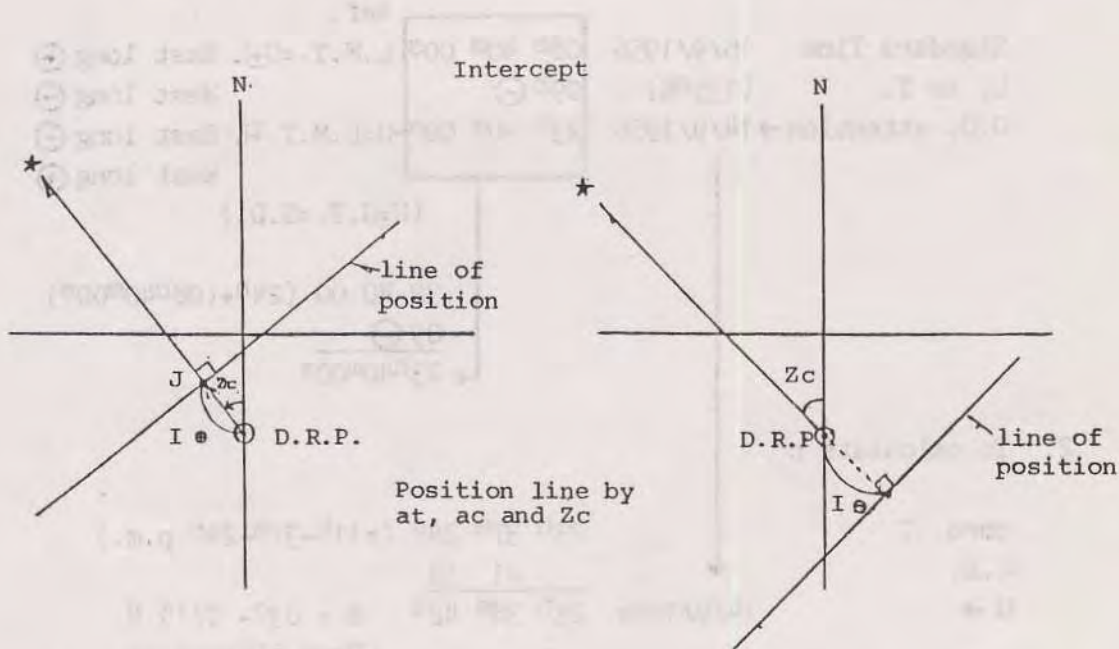


Fig. 69

Example 12

At the standard time 08^h 40^m 00^s (standard time for 135°E) on 15 September 1956, a navigator observed the altitude of the sun's lower limb (\odot) as 39° 07'8 in D.R.P. 34° 45'N, 141° 28'E.

Draw a line of position on the chart.

Where : Chronometer time was 11^h 37^m 24^s, chronometer error \oplus 01^m 18^s, index error \oplus 2.3, height of eye 15 metres, air temperature 22°C, sea water temperature 18°C.

Solution

1. To calculate G.D.

Standard Time	15/9/1956	08h 40m 00s	Ref.
L. in T.	(135°E)	09h \ominus	L.M.T. = U \pm L East long \oplus
G.D. attention \rightarrow	14/9/1956	23h 40m 00s	West long \ominus
			U=L.M.T. \mp L East long \ominus
			West long \oplus
			(U=G.T.=G.D.)
			32 40 00 (24h $+$ (08h40m00s))
			09 \ominus
			\rightarrow 23h40m00s

2. To calculate h

chro. T		23h 37m 24s (=11h-37m-24s p.m.)	
C.E.		01 18	
U \rightarrow	14/9/1956	23h 38m 42s	d = 03°- 07'9 N
			(From almanac on 14/9/1956)
E. (23 38 42 on 14/9/1956)		12 04 40 \oplus	(From almanac)
		35h 43m 22s	
h_G		24 \ominus	
h_C		11 43 21	

h_C $175^\circ - 50:5$
 L ($141^\circ - 28:0$ E) $141^\circ - 28:0$ +
 h $317^\circ - 18:5$

3. To calculate a_c and Z_c by astronomical navigation Table (Altitude-Azimuth Table) corresponding h , d and ℓ .

h $317^\circ - 18:5$ A_1 87780 (see Fig. 29) Z_1 16874
 d $03^\circ - 07:9$ A_2 65 (see Fig. 30) Z_1 $\frac{65}{\oplus}$ ($A_2 = Z_2$)
 $34^\circ - 45:0$ A_3 8531 \oplus (see Fig. 31) 16939
 A_4 96376 \longrightarrow A_5 10871

$\ell - d$ ($34^\circ 45:0$) - ($03^\circ 07:9$) = $31^\circ - 37:1 \rightarrow A_6$ $\frac{7422}{\oplus}$
 a_c $39^\circ - 21:4 \leftarrow A_7$ 18293 $\rightarrow Z_3$ $\frac{11170}{\ominus}$
 Z_4 5769
 Z $61^\circ 07'$
 S $61^\circ 01'$ E

\uparrow
 (see Fig. 34)

4. To calculate true altitude (a_t)

Sex. Alt. \ominus $39^\circ - 07:8$
 I.E. $\frac{02:3}{\oplus}$
 Obs. Alt. \ominus $39^\circ - 10:1$
 Corr. 1 $\frac{07:8}{\oplus}$ (see Fig. 36)
 $39^\circ - 17:9$
 Corr. 2 $\frac{0:2}{\oplus}$ (see Fig. 36)
 $39^\circ - 18:1$
 Corr. 3 $\frac{0:8}{\oplus}$ (air temp. - sea water temp.
 $= 22^\circ C - 18^\circ C = 4^\circ C$)
 a_t $39^\circ - 18:9$

5. To calculate I

a_t \oplus $39^\circ - 18:9$
 a_c $\frac{39^\circ - 21:4}{\ominus}$
 I \ominus 2.5

Ans. Fig. 70

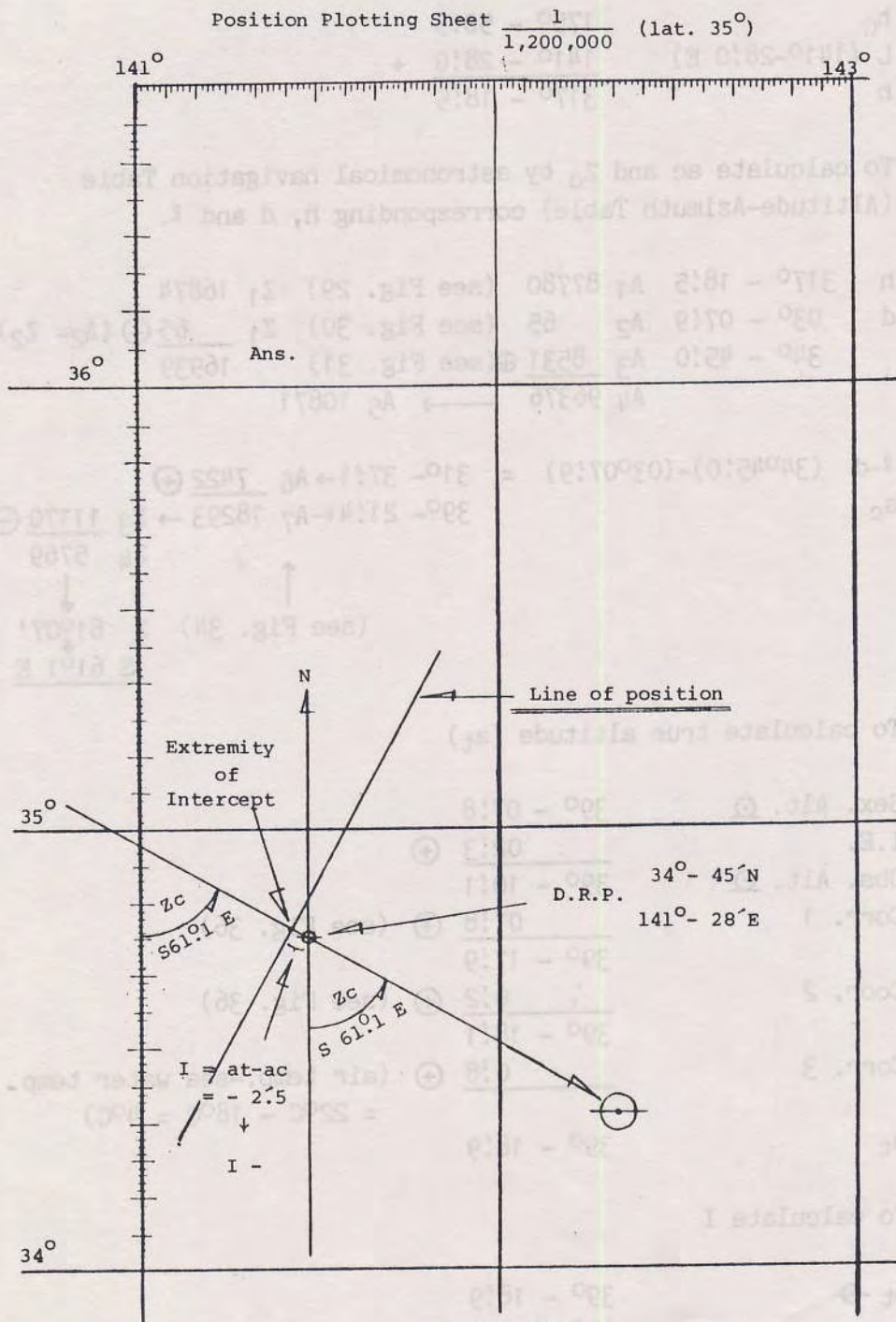


Fig. 70



Fig. 70-1 Meridian Observation

The sun should be observed at local apparent noon as routine work aboard ship.

1983-1985 Regular Course Trainees observing the sun on board M.V. PAKNAM near the Bashi Channel, 7 August 1985.

14 September 1956

Lunar Age 9^d2

Nautical Almanac

☉ Sun				Planet				☾ Moon			
U	E _s	d	P.P. of d	U	E _s	d	P.P.	U	E _t	d	P.P.
h m s	° ' "	h m s	° ' "	♀ Venus	h m s	° ' "	Tr. 0.59	h m s	° ' "	h m s	° ' "
0 12 4	18 N 3	30.6	0 0	0 0 0	0 0 0	0 0	0 0	0 4 36	39 S 19	30.1	1 2 0.1
2	20	28.7	10	2	2	3	3	1	35 42	27.7	2 4 2
4	22	16.8	20	4	4	5	5	2	34 45	25.3	3 6 3
6	24	24.9	30	6	6	6	6	3	33 48	22.9	4 8 3
8	25	22.9	40	8	8	7	7	4	32 51	20.4	5 10 4
10	27	21.0	50	10	10	8	8	5	31 54	17.9	6 11 5
12 12 4	29 N 3	19.1	1 0	12 15 0	40 N 17	9.4	1 0	6	30 57	15.4	7 13 6
14	31	17.2	10	14	38	8.5	10 1	7	30 0	12.9	8 15 7
16	32	15.3	20	16	36	7.7	20 1	8	29 3	10.4	9 17 8
18	34	13.3	30	18	34	6.8	30 2	9	28 7	7.8	10 19 0.9
20	36	11.4	40	20	32	5.9	40 2	10	27 10	5.2	11 21 1.0
22	38	9.5	50	22	30	5.0	50 2	11	26 13	2.6	12 23 0
24 12 4	40 N 3	7.6	2 0	24 15 0	28 N 17	4.1	2 0	12	25 16	0.0	13 25 1
(S.D. 15 56)								(H.P. 54.2, S.D. 14 47)			
U = 0h				♂ Mars				♃ Jupiter			
No.	★ Star	E _t	d	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "
1	Polaris	21 36 59	N 89	0 0 9	22 S 10	19.8	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
2	Kochab	8 41 2	74	2 9	47	20.1	10 2	0	2	0	0
3	Dubhe	12 30 44	61	4	10	12	20.4	20	4	1	1
4	β Cassiop.	23 24 52	58	6	10	37	20.7	30	6	1	1
5	Merah	12 32 34	56	8	11	2	21.0	40	8	1	1
6	Allioth	10 39 40	N 56	10		27	21.2	50	10	1	1
7	Schedir	22 53 41	56	12	0	11	21.5	1	0	12	0.2
8	Mizar	10 9 37	55	14	12	17	21.8	10	15	2	2
9	α Persel	20 10 31	49	16	12	43	22.1	20	17	2	2
10	Benetnasch	9 45 58	49	18	13	8	22.4	30	19	2	2
11	Capella	18 18 16	N 45	20	0	33	22.6	40	21	3	3
12	Deneb	2 51 47	45	22	13	59	22.9	1	50	23	3
13	Vega	4 55 17	38	24	0	14	23.2	2	0	25	0.3
14	Castor	15 59 56	31								
15	Alpheratz	23 25 35	28								
16	Pollux	15 49 6	N 28								
17	α Cor. Bor.	7 58 55	26								
18	Arcturus	9 18 6	19								
19	Aldebaran	18 58 19	16								
20	Markab	0 29 8	14								
21	Denebola	11 44 56	N 14								
22	α Ophiuchi	5 50 50	12								
23	Regulus	13 25 43	12								
24	Altair	3 43 5	8								
25	Betelgeuse	17 35 56	7								
26	Bellatrix	18 8 57	N 6								
27	Procyon	15 54 44	N 5								
28	Rigel	18 19 18	S 8								
29	α Hydrae	14 6 19	8								
30	Spica	10 8 52	10								
31	Sirius	16 48 32	S 16								
32	β Ceti	22 50 20	18								
33	Antares	7 5 1	26								
34	α Sagittarii	4 39 10	26								
35	Fomalhaut	0 36 29	29								
36	λ Scorpii	6 1 5	S 37								
37	Canopus	17 8 47	52								
38	α Pavois	-3 9 30	56								
39	Achernar	21 55 38	57								
40	β Crucis	10 46 37	59								
41	β Centauri	9 31 2	S 60								
42	α Centauri	8 55 8	60								
43	α Crucis	11 7 37	62								
44	α Tri. Aust.	6 47 41	68								
45	β Carinae	14 19 5	S 69								
R _s 23 31 47								(H.P. 54.2, S.D. 14 45)			
Planet											
R.A. d Mag. H.P. S.D.											
♀	8 31	N 17	15	-3.9	0.2	10					
♂	23 22	8 10	20	-2.6	0.4	12					
♃	11 3	N 7	10	-1.2	0.0	14					
♄	15 44	8 17	52	+0.8	0.0	7					
♅	12 38	8 8	29	+1.0	0.2	6					

Fig. 71

Table for Altitude (Ac) and Azimuth (Zc)

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_4$ $A_5 A_6 = A_7$ l & d contrary name $\rightarrow l+d$
 (h) (d) (l) $(L+d)$ (a) l & d same name $\rightarrow l-d$

i	o	317°				47°				316°				46°				i	
		A_1 h	A_4	P.P.	A_5 $(L+d)$	P.P.	Z_1 h	Z_2 Z	P.P.	A_1 h	A_4	P.P.	A_5 $(L+d)$	P.P.	Z_1 h	Z_2 Z	P.P.		
0	↑	89134	0	↓	12843	0	↑	17449	0	↑	87185	0	↓	13432	0	↑	16322	0	80
1		89101	3		12852	1		17435	1		87153	3		13442	1		16308	1	89
2		89068	7		12862	2		17421	2		87121	6		13452	2		16295	2	88
3		89035	10		12872	3		17407	3		87089	10		13462	3		16281	3	87
4		89003	13		12882	4		17393	4		87057	13		13472	4		16268	4	86
5		88970	17		12891	5		17379	5		87025	16		13482	5		16254	5	85
6		88937	20		12901	6		17365	6		86993	19		13492	6		16241	6	84
7		88904	23		12911	7		17351	7		86961	22		13502	7		16227	7	83
8		88871	26		12921	8		17337	8		86929	26		13512	8		16214	8	82
9		88839	30		12930	9		17323	9		86897	29		13522	9		16200	9	81
10		88806	0		12940	0		17309	0		86865	0		13532	0		16487	0	80
11		88773	3		12950	1		17295	1		86833	3		13542	1		16473	1	79
12		88740	7		12960	2		17281	2		86801	6		13552	2		16460	2	78
13		88708	10		12970	3		17267	3		86769	10		13562	3		16446	3	77
14		88675	13		12979	4		17253	4		86737	13		13571	4		16433	4	76
15		88642	17		12989	5		17239	5		86705	16		13581	5		16419	5	75
16		88609	20		12999	6		17225	6		86674	19		13591	6		16406	6	74
17		88577	23		13009	7		17212	7		86642	22		13601	7		16392	7	73
18		88544	26		13018	8		17198	8		86610	26		13611	8		16379	8	72
19		88511	30		13028	9		17184	9		86578	29		13621	9		16366	9	71
20		88479	0		13038	0		17170	0		86546	0		13631	0		16352	0	70
21		88446	3		13048	1		17156	1		86514	3		13641	1		16339	1	69
22		88414	6		13058	2		17142	2		86483	6		13651	2		16326	2	68
23		88381	10		13067	3		17128	3		86451	10		13661	3		16312	3	67
24		88348	13		13077	4		17115	4		86419	13		13671	4		16299	4	66
25		88316	16		13087	5		17101	5		86387	16		13681	5		16285	5	65
26		88283	19		13097	6		17087	6		86356	19		13691	6		16272	6	64
27		88251	22		13107	7		17073	7		86324	22		13701	7		16259	7	63
28		88218	26		13116	8		17059	8		86292	26		13711	8		16245	8	62
29		88186	29		13126	9		17045	9		86261	29		13721	9		16232	9	61
30		88153	0		13136	0		17032	0		86229	0		13731	0		16219	0	60
31		88121	3		13146	1		17018	1		86197	3		13741	1		16205	1	59
32		88088	6		13156	2		17004	2		86166	6		13751	2		16192	2	58
33		88056	10		13166	3		16990	3		86134	9		13761	3		16179	3	57
34		88023	13		13176	4		16977	4		86102	12		13771	4		16166	4	56
35		87991	16		13185	5		16963	5		86071	16		13781	5		16152	5	55
36		87959	19		13195	6		16949	6		86039	19		13791	6		16139	6	54
37		87926	22		13205	7		16935	7		86008	22		13801	7		16126	7	53
38		87894	26		13215	8		16922	8		85976	25		13811	8		16113	8	52
39		87861	29		13225	9		16908	9		85944	28		13822	9		16099	9	51
40		87829	0		13235	0		16894	0		85913	0		13832	0		16086	0	50
41		87797	3		13244	1		16880	1		85881	3		13842	1		16073	1	49
42		87764	6		13254	2		16867	2		85850	6		13852	2		16060	2	48
43		87732	10		13264	3		16853	3		85818	10		13862	3		16046	3	47
44		87700	13		13274	4		16839	4		85787	13		13872	4		16033	4	46
45		87668	16		13284	5		16826	5		85755	16		13882	5		16020	5	45
46		87635	19		13294	6		16812	6		85724	19		13892	6		16007	6	44
47		87603	22		13304	7		16798	7		85693	22		13902	7		15994	7	43
48		87571	26		13314	8		16785	8		85661	26		13912	8		15980	8	42
49		87539	29		13323	9		16771	9		85630	29		13922	9		15967	9	41
50		87506	0		13333	0		16758	0		85598	0		13932	0		15954	0	40
51		87474	3		13343	1		16744	1		85567	3		13942	1		15941	1	39
52		87442	7		13353	2		16730	2		85535	6		13952	2		15928	2	38
53		87410	10		13363	3		16717	3		85504	10		13962	3		15915	3	37
54		87378	13		13373	4		16703	4		85473	13		13972	4		15902	4	36
55		87345	17		13383	5		16690	5		85441	16		13983	5		15888	5	35
56		87313	20		13393	6		16676	6		85410	19		13993	6		15875	6	34
57		87281	23		13403	7		16662	7		85379	22		14003	7		15862	7	33
58		87249	26		13412	8		16649	8		85347	26		14013	8		15849	8	32
59		87217	29		13422	9		16635	9		85316	29		14023	9		15836	9	31
60	↑	87185	0	↓	13432	0	↑	16622	0	↑	85285	0	↓	14033	0	↑	15823	0	30

$Z_1 + Z_2 (= A_2) - Z_3 = Z_4$
 $(h) (d) \qquad\qquad\qquad (a) (Z)$

Fig. 72

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$$A_1 + A_2 + A_3 = A_4 + A_5 + A_6 = A_7$$

$$(A) (d) (l) \quad (l \pm d) (a)$$

ℓ & d contrary name → ℓ+d

ℓ & d same name → ℓ-d

°	86°													87°												
	A ₁ h	A ₂	P.P.	A ₃ A ₄ ±d	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₁ h	A ₂	P.P.	A ₃ A ₄ ±d	P.P.	Z ₁ h	Z ₂ Z	P.P.										
0	↑ 33243	0	↓ 46512	0	↑ 106	0	↑ 32438	0	↓ 47383	0	↑ 60	0	0	60	0	0	60									
1	33230	1	46527	1	105	0	32424	1	47388	1	59	0	0	59	0	0	59									
2	33216	3	46541	3	104	0	32411	3	47412	3	58	0	0	58	0	0	58									
3	33203	4	46556	5	103	0	32398	4	47427	4	58	0	0	58	0	0	57									
4	33189	5	46570	6	102	0	32384	5	47441	5	57	0	0	57	0	0	56									
5	33176	7	46585	8	102	0	32371	7	47456	8	56	1	1	56	1	1	55									
6	33162	8	46599	9	101	0	32359	8	47470	9	56	1	1	56	1	1	54									
7	33149	9	46614	11	100	0	32344	9	47485	11	55	1	1	55	1	1	53									
8	33135	10	46628	12	99	0	32331	10	47499	12	54	1	1	54	1	1	52									
9	33122	12	46643	14	98	0	32318	12	47514	14	54	1	1	54	1	1	51									
10	33108	0	46657	0	97	0	32305	0	47528	0	53	0	0	53	0	0	50									
11	33095	1	46672	1	96	0	32291	1	47543	1	52	0	0	52	0	0	49									
12	33081	3	46686	3	96	0	32278	3	47558	3	52	0	0	52	0	0	48									
13	33068	4	46701	5	95	0	32265	4	47572	4	51	0	0	51	0	0	47									
14	33054	5	46715	6	94	0	32252	5	47587	5	51	0	0	51	0	0	46									
15	33041	7	46730	8	93	1	32238	7	47601	7	50	1	1	50	1	1	45									
16	33027	8	46744	9	92	1	32225	8	47616	8	49	1	1	49	1	1	44									
17	33014	9	46759	11	91	1	32212	10	47630	10	49	1	1	49	1	1	43									
18	33000	10	46773	12	91	1	32199	11	47645	11	48	1	1	48	1	1	42									
19	32987	12	46788	14	90	1	32185	12	47659	12	48	1	1	48	1	1	41									
20	32973	0	46802	0	89	0	32172	0	47674	0	47	0	0	47	0	0	40									
21	32960	1	46817	1	88	0	32159	1	47688	1	46	0	0	46	0	0	39									
22	32946	3	46831	3	87	0	32145	3	47703	3	46	0	0	46	0	0	38									
23	32933	4	46846	5	87	0	32132	4	47717	4	45	0	0	45	0	0	37									
24	32919	5	46860	6	86	0	32119	5	47732	5	45	0	0	45	0	0	36									
25	32906	7	46875	8	85	1	32106	7	47746	7	44	1	1	44	1	1	35									
26	32892	8	46890	9	84	1	32093	8	47761	8	44	1	1	44	1	1	34									
27	32879	9	46904	11	83	1	32080	9	47775	10	43	1	1	43	1	1	33									
28	32866	10	46919	12	83	1	32066	10	47790	11	42	1	1	42	1	1	32									
29	32852	12	46933	14	82	1	32053	12	47805	12	42	1	1	42	1	1	31									
30	32839	0	46948	0	81	0	32040	0	47819	0	41	0	0	41	0	0	30									
31	32825	1	46962	1	80	0	32027	1	47834	1	41	0	0	41	0	0	29									
32	32812	3	46977	3	80	0	32014	3	47848	3	40	0	0	40	0	0	28									
33	32798	4	46991	4	79	0	32000	4	47863	4	40	0	0	40	0	0	27									
34	32785	5	47006	6	78	0	31987	5	47877	5	39	0	0	39	0	0	26									
35	32772	7	47020	7	77	1	31974	7	47892	8	39	0	0	39	0	0	25									
36	32758	8	47035	8	77	1	31961	8	47906	9	38	0	0	38	0	0	24									
37	32745	9	47049	10	76	1	31948	9	47921	11	38	0	0	38	0	0	23									
38	32731	10	47064	11	75	1	31934	10	47935	12	37	0	0	37	0	0	22									
39	32718	12	47078	13	74	1	31921	12	47950	14	37	0	0	37	0	0	21									
40	32705	0	47093	0	74	0	31908	0	47964	0	36	0	0	36	0	0	20									
41	32691	1	47107	1	73	0	31895	1	47979	2	36	0	0	36	0	0	19									
42	32678	3	47122	3	72	0	31882	3	47993	3	35	0	0	35	0	0	18									
43	32664	4	47136	4	71	0	31869	4	48008	5	34	0	0	34	0	0	17									
44	32651	5	47151	6	71	0	31856	5	48022	6	34	0	0	34	0	0	16									
45	32638	7	47165	7	70	1	31842	7	48037	8	33	1	1	33	1	1	15									
46	32624	8	47180	8	69	1	31829	8	48052	9	33	1	1	33	1	1	14									
47	32611	9	47194	10	68	1	31816	10	48066	11	33	1	1	33	1	1	13									
48	32598	10	47209	11	68	1	31803	11	48081	12	32	1	1	32	1	1	12									
49	32584	12	47223	13	67	1	31790	12	48095	14	32	1	1	32	1	1	11									
50	32571	0	47238	0	66	0	31777	0	48110	0	31	0	0	31	0	0	10									
51	32557	1	47252	1	66	0	31764	1	48124	1	31	0	0	31	0	0	9									
52	32544	3	47267	3	65	0	31751	3	48139	3	30	0	0	30	0	0	8									
53	32531	4	47282	5	64	0	31737	4	48153	4	30	0	0	30	0	0	7									
54	32517	5	47296	6	64	0	31724	5	48168	6	29	0	0	29	0	0	6									
55	32504	7	47311	8	63	1	31711	7	48182	7	29	0	0	29	0	0	5									
56	32491	8	47325	9	62	1	31698	8	48197	8	28	0	0	28	0	0	4									
57	32478	9	47340	11	62	1	31685	9	48211	10	28	0	0	28	0	0	3									
58	32464	10	47354	12	61	1	31672	10	48226	11	27	0	0	27	0	0	2									
59	32451	12	47369	14	60	1	31659	12	48241	13	27	0	0	27	0	0	1									
60	↑ 32438	↓ 47383	↑ 60	↑ 31646	↓ 48255	↑ 28	0	0	0	0	0	0	0	0	0	0	0									
	A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ l	Z ₁ a	P.P.	A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ l	Z ₁ a	P.P.	°									
	273'		3'		272'		2'																			

$$Z_1 + Z_2 (= A_2) - Z_3 = Z_4$$

$$(h) (d) \quad (a) (Z)$$

Fig. 73

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_4 \rightarrow A_5 + A_6 = A_7$
 $(A) (d) (l) (l \pm d) (a)$

ℓ & d contrary name $\rightarrow \ell + d$
 ℓ & d same name $\rightarrow \ell - d$

L	54°										55°										D
	A ₁ h	A ₂	P.P.	A ₃ l	A ₄ l+d	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₁ h	A ₂	P.P.	A ₃ l	A ₄ l+d	P.P.	Z ₁ h	Z ₂ Z	P.P.			
0	68591	1	0	20611	0	0	9204	0	67119	0	0	21321	0	0	8664	0	0	60			
1	68307	1	0	20623	0	0	9195	0	67095	2	2	21333	1	1	8655	1	1	69			
2	68511	5	0	20634	0	0	9186	2	67070	5	5	21345	3	3	8646	3	3	68			
3	68516	8	0	20646	4	4	9177	3	67046	7	7	21357	4	4	8637	4	4	67			
4	68492	10	0	20658	5	5	9168	4	67022	10	10	21369	5	5	8628	5	5	66			
5	68467	13	0	20670	6	6	9158	5	66998	12	12	21381	6	6	8619	6	6	65			
6	68442	15	0	20681	7	7	9149	6	66973	14	14	21393	7	7	8611	7	7	64			
7	68417	18	0	20693	8	8	9140	7	66949	17	17	21405	8	8	8602	8	8	63			
8	68393	20	0	20705	10	10	9131	8	66925	19	19	21417	10	10	8593	9	9	62			
9	68368	23	0	20717	11	11	9122	9	66901	22	22	21429	11	11	8584	8	8	61			
10	68343	0	0	20729	0	0	9113	0	66877	0	0	21440	0	0	8575	0	0	60			
11	68318	2	0	20740	1	1	9104	1	66852	2	2	21452	1	1	8567	1	1	49			
12	68294	5	0	20752	2	2	9094	2	66829	5	5	21464	2	2	8558	2	2	48			
13	68269	7	0	20764	3	3	9085	3	66804	7	7	21476	3	3	8549	3	3	47			
14	68244	10	0	20776	4	4	9076	4	66780	10	10	21488	4	4	8540	4	4	46			
15	68220	12	0	20788	5	5	9067	5	66756	12	12	21500	5	5	8531	5	5	45			
16	68195	14	0	20799	6	6	9058	6	66732	14	14	21512	6	6	8523	6	6	44			
17	68170	17	0	20811	7	7	9049	7	66708	17	17	21524	7	7	8514	7	7	43			
18	68146	19	0	20823	8	8	9040	8	66683	19	19	21536	8	8	8505	8	8	42			
19	68121	22	0	20835	9	9	9031	9	66659	22	22	21548	9	9	8496	9	9	41			
20	68097	0	0	20847	0	0	9022	0	66635	0	0	21560	0	0	8488	0	0	40			
21	68072	2	0	20858	1	1	9013	1	66611	2	2	21572	1	1	8479	1	1	39			
22	68047	5	0	20870	2	2	9004	2	66587	5	5	21584	2	2	8470	2	2	38			
23	68023	7	0	20882	3	3	8995	3	66563	7	7	21596	3	3	8462	3	3	37			
24	67998	10	0	20894	4	4	8986	4	66539	10	10	21608	4	4	8453	4	4	36			
25	67974	12	0	20906	5	5	8977	5	66515	12	12	21620	5	5	8444	5	5	35			
26	67949	14	0	20918	6	6	8967	6	66491	14	14	21632	6	6	8435	6	6	34			
27	67924	17	0	20929	7	7	8958	7	66467	17	17	21644	7	7	8427	7	7	33			
28	67900	19	0	20941	8	8	8949	8	66443	19	19	21656	8	8	8418	8	8	32			
29	67875	22	0	20953	9	9	8940	9	66419	22	22	21668	9	9	8409	9	9	31			
30	67851	0	0	20965	0	0	8931	0	66395	0	0	21680	0	0	8401	0	0	30			
31	67826	3	0	20977	1	1	8922	1	66371	3	3	21692	1	1	8392	1	1	29			
32	67802	5	0	20989	2	2	8913	2	66347	5	5	21704	2	2	8383	2	2	28			
33	67777	8	0	21000	3	3	8904	3	66323	7	7	21716	3	3	8375	3	3	27			
34	67753	10	0	21012	4	4	8895	4	66299	10	10	21728	4	4	8366	4	4	26			
35	67728	13	0	21024	5	5	8886	5	66275	12	12	21740	5	5	8357	5	5	25			
36	67704	15	0	21036	6	6	8877	6	66251	14	14	21752	6	6	8349	6	6	24			
37	67679	18	0	21048	7	7	8868	7	66227	17	17	21764	7	7	8340	7	7	23			
38	67655	20	0	21060	8	8	8859	8	66203	19	19	21776	8	8	8331	8	8	22			
39	67630	23	0	21072	9	9	8851	9	66179	22	22	21788	9	9	8323	9	9	21			
40	67606	0	0	21083	0	0	8842	0	66155	0	0	21800	0	0	8314	0	0	20			
41	67582	3	0	21095	1	1	8833	1	66131	3	3	21812	1	1	8305	1	1	19			
42	67557	5	0	21107	2	2	8824	2	66107	5	5	21824	2	2	8297	2	2	18			
43	67533	8	0	21119	3	3	8815	3	66083	7	7	21836	3	3	8288	3	3	17			
44	67508	10	0	21131	4	4	8806	4	66059	10	10	21848	4	4	8279	4	4	16			
45	67484	12	0	21143	5	5	8797	5	66035	12	12	21860	5	5	8271	5	5	15			
46	67459	14	0	21155	6	6	8788	6	66012	14	14	21872	6	6	8262	6	6	14			
47	67435	17	0	21167	7	7	8779	7	65988	17	17	21884	7	7	8254	7	7	13			
48	67411	19	0	21178	8	8	8770	8	65964	19	19	21896	8	8	8245	8	8	12			
49	67386	22	0	21190	9	9	8761	9	65940	22	22	21908	9	9	8237	9	9	11			
50	67362	0	0	21202	0	0	8752	0	65916	0	0	21920	0	0	8228	0	0	10			
51	67338	3	0	21214	1	1	8743	1	65892	3	3	21932	1	1	8219	1	1	9			
52	67313	5	0	21226	2	2	8734	2	65868	5	5	21944	2	2	8211	2	2	8			
53	67289	8	0	21238	3	3	8725	3	65845	7	7	21956	3	3	8202	3	3	7			
54	67265	10	0	21250	4	4	8717	4	65821	10	10	21968	4	4	8194	4	4	6			
55	67240	13	0	21262	5	5	8708	5	65797	12	12	21980	5	5	8185	5	5	5			
56	67216	15	0	21274	6	6	8699	6	65773	14	14	21992	6	6	8177	6	6	4			
57	67192	18	0	21285	7	7	8690	7	65749	17	17	22004	7	7	8168	7	7	3			
58	67167	20	0	21297	8	8	8681	8	65725	19	19	22016	8	8	8160	8	8	2			
59	67143	23	0	21309	9	9	8672	9	65702	22	22	22028	9	9	8151	9	9	1			
60	67119	0	0	21321	0	0	8664	0	65678	0	0	22040	0	0	8143	0	0	0			

$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$
 $(A) (d) (l) (l \pm d) (a)$

Fig. 74

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$$A_1 + A_2 + A_3 = A_4 \rightarrow A_5 + A_6 = A_7$$

$$(A) (d) (l) \quad (l \pm d) (a)$$

f & d contrary name \rightarrow l+d
 l & d same name \rightarrow l-d

h	38'									39'									
	A ₁ h	A ₂	P.P.	A ₃	A ₄ l±d	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₁ h	A ₂	P.P.	A ₃	A ₄ l±d	P.P.	Z ₁ h	Z ₂ Z	P.P.	
0	† 97472	0		† 10599	0		† 21066	0		† 95301	0		† 11143	0		† 20113	0		60
1	97435	4		10608	1		21050	2		95265	4		11152	1		20097	2		59
2	97394	7		10617	2		21033	3		95230	7		11161	2		20082	3		58
3	97362	11		10626	3		21017	5		95194	11		11170	3		20066	5		57
4	97325	15		10635	4		21001	6		95158	14		11179	4		20050	6		56
5	97288	19		10644	5		20985	8		95123	18		11189	5		20035	8		55
6	97252	22		10653	5		20969	10		95087	21		11198	6		20019	9		54
7	97215	26		10662	6		20953	11		95052	25		11207	7		20004	11		53
8	97179	30		10671	7		20937	13		95016	28		11216	8		19988	13		52
9	97142	33		10680	8		20921	14		94981	32		11225	9		19973	14		51
10	97106	0		10689	0		20905	0		94945	0		11234	0		19957	0		50
11	97069	4		10698	1		20889	2		94910	4		11244	1		19942	2		49
12	97033	7		10707	2		20872	3		94874	7		11253	2		19926	3		48
13	96996	11		10716	3		20856	5		94839	11		11262	3		19911	5		47
14	96960	15		10725	4		20840	6		94803	14		11271	4		19895	6		46
15	96923	19		10734	5		20824	8		94768	18		11280	5		19880	8		45
16	96887	22		10743	5		20808	10		94732	21		11290	6		19864	9		44
17	96850	26		10752	6		20792	11		94697	25		11299	7		19849	11		43
18	96814	30		10761	7		20776	13		94661	28		11308	8		19834	13		42
19	96778	33		10770	8		20760	14		94626	32		11317	9		19818	14		41
20	96741	0		10779	0		20744	0		94591	0		11326	0		19803	0		40
21	96705	4		10788	1		20728	2		94555	4		11336	1		19787	2		39
22	96669	7		10797	2		20712	3		94520	7		11345	2		19772	3		38
23	96632	11		10806	3		20696	5		94485	11		11354	3		19756	5		37
24	96596	14		10815	4		20681	6		94449	14		11363	4		19741	6		36
25	96560	18		10824	5		20665	8		94414	18		11373	5		19726	8		35
26	96524	22		10833	5		20649	10		94379	21		11382	6		19710	9		34
27	96487	25		10842	6		20633	11		94344	25		11391	7		19695	11		33
28	96451	29		10851	7		20617	13		94308	28		11400	8		19680	13		32
29	96415	32		10861	8		20601	14		94273	32		11410	9		19664	14		31
30	96379	0		10870	0		20585	0		94238	0		11419	0		19649	0		30
31	96343	4		10879	1		20569	2		94203	4		11428	1		19634	2		29
32	96306	7		10888	2		20553	3		94168	7		11437	2		19618	3		28
33	96270	11		10897	3		20537	5		94133	11		11447	3		19603	5		27
34	96234	14		10906	4		20522	6		94097	14		11456	4		19588	6		26
35	96198	18		10915	5		20506	8		94062	18		11465	5		19572	8		25
36	96162	22		10924	5		20490	10		94027	21		11474	6		19557	10		24
37	96126	25		10933	6		20474	11		93992	25		11484	7		19542	11		23
38	96090	29		10942	7		20458	13		93957	28		11493	8		19527	13		22
39	96054	32		10951	8		20442	14		93922	32		11502	9		19511	14		21
40	96018	0		10960	0		20427	0		93887	0		11511	0		19496	0		20
41	95982	4		10969	1		20411	2		93852	4		11521	1		19481	2		19
42	95946	7		10978	2		20395	3		93817	7		11530	2		19466	3		18
43	95910	11		10988	3		20379	5		93782	11		11539	3		19450	5		17
44	95874	14		10997	4		20364	6		93747	14		11549	4		19435	6		16
45	95838	18		11006	5		20348	8		93712	18		11558	5		19420	8		15
46	95802	22		11015	5		20332	10		93677	21		11567	6		19405	9		14
47	95766	25		11024	6		20316	11		93642	25		11577	7		19390	11		13
48	95730	29		11033	7		20301	13		93607	28		11586	8		19375	13		12
49	95694	32		11042	8		20285	14		93572	32		11595	9		19359	14		11
50	95659	0		11051	0		20269	0		93538	0		11604	0		19344	0		10
51	95623	4		11060	1		20254	2		93503	4		11614	1		19329	2		9
52	95587	7		11070	2		20238	3		93468	7		11623	2		19314	3		8
53	95551	11		11079	3		20222	5		93433	11		11632	3		19299	5		7
54	95515	14		11088	4		20207	6		93398	14		11642	4		19284	6		6
55	95480	18		11097	5		20191	8		93363	18		11651	5		19269	8		5
56	95444	21		11106	5		20175	10		93329	21		11660	6		19254	9		4
57	95408	25		11115	6		20160	11		93294	25		11670	7		19238	11		3
58	95372	28		11124	7		20144	13		93259	28		11679	8		19223	13		2
59	95337	32		11134	8		20129	14		93224	32		11688	9		19208	14		1
60	† 95301	0		† 11143	0		† 20113	0		† 93190	0		† 11698	0		† 19193	0		0
A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ l	Z ₁ u	P.P.	A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ l	Z ₂ a	P.P.				
321'				51'				320'				50'							

$$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$$

$$(A) (d) \quad (a) (Z)$$

Fig. 75

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_4 \rightarrow A_5 + A_6 = A_7$
 (A) (d) (l) (t) (l±d) (a)

ℓ & d contrary name → ℓ+d
 ℓ & d same name → ℓ-d

°	30'									31'									
	A_1 h	A_2	P.P.	A_3	A_4 l±d	P.P.	Z_1 h	Z_2 Z	P.P.	A_1 h	A_2	P.P.	A_3	A_4 l±d	P.P.	Z_1 h	Z_2 Z	P.P.	
0	↑ 117401	0	↓	6699	0	↑	30103	0	↑ 114620	0	↓	7142	0	↑	28818	0		60	
1	117354	5		6706	1		30081	2	114575	5		7149	1		28795	3		59	
2	117306	9		6713	1		30059	4	114529	9		7157	1		28774	4		58	
3	117259	14		6721	2		30037	7	114484	14		7164	2		28753	6		57	
4	117212	19		6728	3		30016	9	114438	18		7172	3		28732	8		56	
5	117165	24		6735	4		29994	11	114393	23		7179	4		28711	11		55	
6	117118	28		6742	4		29972	13	114347	27		7187	4		28690	13		54	
7	117071	33		6750	5		29950	15	114302	32		7194	5		28669	15		53	
8	117024	38		6757	5		29928	18	114257	36		7202	6		28648	17		52	
9	116977	42		6764	6		29907	20	114211	41		7209	6		28627	19		51	
10	116931	0		6772	0		29885	0	114166	0		7217	0		28607	0		50	
11	116884	5		6779	1		29863	2	114121	5		7224	1		28586	2		49	
12	116837	9		6786	1		29841	4	114075	9		7232	1		28565	4		48	
13	116790	14		6794	2		29820	7	114030	14		7239	2		28544	6		47	
14	116743	18		6801	3		29798	9	113985	18		7247	3		28523	8		46	
15	116697	23		6808	4		29776	11	113940	23		7254	4		28502	11		45	
16	116650	28		6816	4		29755	13	113895	27		7262	4		28481	13		44	
17	116603	32		6823	5		29733	15	113849	32		7270	5		28461	15		43	
18	116556	37		6830	6		29712	18	113804	36		7277	6		28440	17		42	
19	116510	41		6833	6		29690	20	113759	41		7285	6		28419	19		41	
20	116463	0		6845	0		29668	0	113714	0		7292	0		28398	0		40	
21	116417	5		6852	1		29647	2	113669	5		7300	1		28378	2		39	
22	116370	9		6860	2		29625	4	113624	9		7307	2		28357	4		38	
23	116324	14		6867	2		29604	6	113579	14		7315	2		28336	6		37	
24	116277	18		6874	3		29582	8	113534	18		7322	3		28315	8		36	
25	116231	23		6882	4		29561	11	113489	23		7330	4		28295	10		35	
26	116184	28		6889	5		29539	13	113444	27		7338	5		28274	12		34	
27	116138	32		6896	6		29518	15	113400	32		7345	6		28253	14		33	
28	116091	37		6904	6		29496	17	113355	36		7353	6		28233	16		32	
29	116045	41		6911	7		29475	19	113310	41		7360	7		28212	18		31	
30	115999	0		6919	0		29453	0	113265	0		7368	0		28191	0		30	
31	115952	5		6926	1		29432	2	113220	5		7376	1		28171	2		29	
32	115906	9		6933	2		29410	4	113175	9		7383	2		28150	4		28	
33	115860	14		6941	2		29389	6	113131	14		7391	2		28130	6		27	
34	115813	18		6948	3		29367	8	113086	18		7398	3		28109	8		26	
35	115767	23		6956	4		29346	11	113041	23		7406	4		28089	10		25	
36	115721	28		6963	5		29325	13	112997	27		7414	5		28068	12		24	
37	115675	32		6970	6		29303	15	112952	32		7421	6		28048	14		23	
38	115629	37		6978	6		29282	17	112907	36		7429	6		28027	16		22	
39	115583	41		6985	7		29261	19	112863	41		7437	7		28006	18		21	
40	115536	0		6993	0		29239	0	112818	0		7444	0		27986	0		20	
41	115490	5		7000	1		29218	2	112774	4		7452	1		27966	2		19	
42	115444	9		7007	2		29197	4	112729	9		7459	2		27945	4		18	
43	115398	14		7015	2		29176	6	112685	13		7467	2		27925	6		17	
44	115352	18		7022	3		29154	8	112640	18		7475	3		27904	8		16	
45	115306	23		7030	4		29133	11	112596	22		7482	4		27884	10		15	
46	115260	28		7037	5		29112	13	112552	26		7490	4		27863	12		14	
47	115215	32		7045	6		29091	15	112507	31		7498	5		27843	14		13	
48	115169	37		7052	6		29069	17	112463	35		7505	6		27823	16		12	
49	115123	41		7059	7		29048	19	112418	40		7513	6		27802	18		11	
50	115077	0		7067	0		29027	0	112374	0		7521	0		27782	0		10	
51	115031	5		7074	1		29006	2	112330	4		7528	1		27762	2		9	
52	114985	9		7082	1		28985	4	112286	9		7536	2		27741	4		8	
53	114940	14		7089	2		28964	6	112241	13		7544	2		27721	6		7	
54	114894	18		7097	3		28942	8	112197	18		7551	3		27701	8		6	
55	114848	23		7104	4		28921	11	112153	22		7559	4		27680	10		5	
56	114803	28		7112	4		28900	13	112109	26		7567	5		27660	12		4	
57	114757	32		7119	5		28879	15	112065	31		7574	6		27640	14		3	
58	114711	37		7127	6		28858	17	112020	35		7582	6		27619	16		2	
59	114666	41		7134	6		28837	19	111976	40		7590	7		27599	18		1	
60	↑ 114620		↓	7142		↑	28816		↑ 11932		↓	7598		↓	27579			0	
	A_1 h	P.P.	A_2 d	P.P.	A_3 l	A_4 l	Z_1 h	P.P.	A_1 h	P.P.	A_2 d	P.P.	A_3 l	A_4 l	Z_1 h	P.P.			
	329°				59'				328°					58'					

$Z_1 + Z_2 (= A_2) - Z_3 = Z_4$
 (h) (d) (a) (Z)

Fig. 76

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth l & d contrary name $\rightarrow l+d$
 l & d same name $\rightarrow l-d$
 $A_1 + A_2 + A_3 = A_4$ $A_5 + A_6 = A_7$
 (h) (d) (l) $(l+d)$ (a)

h	50°							51°									
	A ₁ h	A ₂	P.P.	A ₃ l+d	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₅ h	A ₆	P.P.	A ₇ l+d	P.P.	Z ₃ h	Z ₄ Z	P.P.	
0	† 74810	0	↓	17851	0	†	11575	0	†	73203	0	↓	18534	0	†	10950	0
1	74783	3		17872	1		11564	1		73177	1		18545	1		10940	1
2	74756	5		17883	2		11553	2		73150	2		18557	2		10929	2
3	74729	8		17894	3		11543	3		73124	3		18568	3		10919	3
4	74702	11		17905	4		11532	4		73097	4		18579	4		10909	4
5	74675	14		17916	5		11522	5		73071	5		18591	5		10899	5
6	74648	16		17928	6		11511	6		73044	6		18602	6		10888	6
7	74621	19		17939	7		11501	7		73018	7		18613	7		10878	7
8	74594	22		17950	8		11490	8		72992	8		18624	8		10868	8
9	74567	24		17961	10		11479	9		72965	9		18636	10		10858	9
10	74540	0		17972	0		11469	0		72939	0		18647	0		10848	0
11	74513	3		17983	1		11458	1		72912	1		18658	1		10838	1
12	74486	5		17995	2		11448	2		72886	2		18670	2		10827	2
13	74459	8		18006	3		11437	3		72860	3		18681	3		10817	3
14	74432	11		18017	4		11427	4		72833	4		18692	4		10807	4
15	74405	14		18028	5		11416	5		72807	5		18704	5		10797	5
16	74378	16		18039	6		11406	6		72781	6		18715	6		10787	6
17	74351	19		18050	7		11395	7		72754	7		18727	7		10777	7
18	74324	22		18062	8		11385	8		72728	8		18738	8		10767	8
19	74297	24		18073	10		11374	9		72702	9		18749	10		10757	9
20	74271	0		18084	0		11364	0		72675	0		18761	0		10746	0
21	74244	3		18095	1		11353	1		72649	1		18772	1		10736	1
22	74217	5		18106	2		11343	2		72623	2		18783	2		10726	2
23	74190	8		18118	3		11332	3		72597	3		18795	3		10716	3
24	74163	11		18129	4		11322	4		72570	4		18806	4		10706	4
25	74136	14		18140	5		11312	5		72544	5		18817	5		10696	5
26	74109	16		18151	6		11301	6		72518	6		18829	6		10686	6
27	74083	19		18162	7		11291	7		72492	7		18840	7		10677	7
28	74056	22		18174	8		11280	8		72465	8		18852	8		10668	8
29	74029	24		18185	10		11270	9		72439	9		18863	10		10659	9
30	74002	0		18196	0		11259	0		72413	0		18874	0		10648	0
31	73975	3		18207	1		11249	1		72387	1		18886	1		10638	1
32	73949	5		18219	2		11239	2		72361	2		18897	2		10628	2
33	73922	8		18230	3		11228	3		72334	3		18908	3		10618	3
34	73895	11		18241	4		11218	4		72308	4		18920	4		10608	4
35	73868	14		18252	5		11207	5		72282	5		18931	5		10598	5
36	73842	16		18263	6		11197	6		72256	6		18943	6		10588	6
37	73815	19		18275	7		11187	7		72230	7		18954	7		10578	7
38	73788	22		18286	8		11176	8		72204	8		18965	8		10568	8
39	73762	24		18297	10		11166	9		72178	9		18977	10		10558	9
40	73735	0		18308	0		11156	0		72152	0		18988	0		10548	0
41	73708	3		18320	1		11145	1		72125	1		19000	1		10538	1
42	73681	5		18331	2		11135	2		72099	2		19011	2		10528	2
43	73655	8		18342	3		11125	3		72073	3		19022	3		10518	3
44	73628	10		18353	4		11114	4		72047	4		19034	4		10508	4
45	73602	13		18365	5		11104	5		72021	5		19045	5		10498	5
46	73575	16		18376	6		11094	6		71995	6		19057	6		10488	6
47	73548	18		18387	7		11083	7		71969	7		19068	7		10478	7
48	73522	21		18399	8		11073	8		71943	8		19080	8		10468	8
49	73495	23		18410	10		11063	9		71917	9		19091	10		10458	9
50	73468	0		18421	0		11052	0		71891	0		19102	0		10448	0
51	73442	3		18432	1		11042	1		71865	1		19114	1		10438	1
52	73415	5		18444	2		11032	2		71839	2		19125	2		10428	2
53	73389	8		18455	3		11022	3		71813	3		19137	3		10418	3
54	73362	10		18466	4		11011	4		71787	4		19148	4		10408	4
55	73336	13		18478	5		11001	5		71761	5		19160	5		10398	5
56	73309	16		18489	6		10991	6		71735	6		19171	6		10388	6
57	73283	18		18500	7		10980	7		71709	7		19183	7		10378	7
58	73256	21		18511	8		10970	8		71683	8		19194	8		10368	8
59	73230	23		18523	10		10960	9		71658	9		19205	10		10357	9
60	† 73203	0		↓ 18534	0		† 10950	0		† 71632	0		↓ 19217	0		† 10347	0
A ₁ h	P.P.	A ₂ d	P.P.	A ₃ l	A ₄ l+d	Z ₁ h	Z ₂ Z	P.P.	A ₅ h	P.P.	A ₆ d	P.P.	A ₇ l+d	P.P.	Z ₃ h	Z ₄ Z	P.P.
309°				39°					308°				38°				

$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$
 (h) (d) (l) (a) (Z)

Fig. 77

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY
 AGENCY, JAPAN.

Table of Altitude and Azimuth

$$A_1 + A_2 + A_3 = A_4 \quad A_5 + A_6 = A_7$$

(h) (d) (l) (l+d) (a)

ℓ & d contrary name → ℓ+d
ℓ & d same name → ℓ-d

°	60'						61'									
	A_1 h	A_2 h	P.P.	A_3 ±d	A_4 ±d	P.P.	Z_1 h	Z_2 Z	P.P.	A_5 h	A_6 ±d	P.P.	Z_3 h	Z_4 Z	P.P.	
0	60206			25000						58906			25760			60
1	60184			25013						58885			25772			69
2	60162			25025						58863			25785			68
3	60140			25038						58842			25798			67
4	60119			25050						58820			25810			66
5																
6	60097			25063						58799			25823			65
7	60075			25076						58778			25836			64
8	60053			25088						58756			25849			63
9	60031			25101						58735			25861			62
10	60009			25113						58713			25874			61
11																
12	59988			25126						58692			25887			60
13	59966			25139						58671			25900			49
14	59944			25151						58649			25912			48
15	59922			25164						58628			25925			47
16	59900			25177						58607			25938			46
17	59879			25189						58585			25951			45
18	59857			25202						58564			25963			44
19	59835			25214						58543			25976			43
20	59813			25227						58521			25989			42
21	59792			25240						58500			26002			41
22																
23	59770			25252						58479			26014			40
24	59748			25265						58457			26027			39
25	59726			25278						58436			26040			39
26	59705			25290						58415			26053			37
27	59683			25303						58394			26065			36
28	59661			25316						58372			26078			35
29	59640			25328						58351			26091			34
30	59618			25341						58330			26104			33
31	59596			25354						58308			26117			32
32	59575			25366						58287			26129			31
33																
34	59553			25379						58266			26142			30
35	59531			25391						58245			26155			29
36	59510			25404						58224			26168			28
37	59488			25417						58202			26180			27
38	59466			25429						58181			26193			26
39																
40	59445			25442						58160			26206			25
41	59423			25455						58139			26219			24
42	59401			25467						58118			26232			23
43	59380			25480						58096			26244			22
44	59358			25493						58075			26257			21
45																
46	59337			25506						58054			26270			20
47	59315			25518						58033			26283			19
48	59293			25531						58012			26296			18
49	59272			25544						57991			26308			17
50	59250			25556						57969			26321			16
51																
52	59229			25569						57948			26334			15
53	59207			25582						57927			26347			14
54	59186			25594						57906			26360			13
55	59164			25607						57885			26372			12
56	59143			25620						57864			26385			11
57																
58	59121			25632						57843			26398			10
59	59100			25645						57822			26411			9
60	59078			25658						57801			26424			8
1	59057			25671						57779			26437			7
2	59035			25683						57758			26449			6
3																
4	59014			25696						57737			26462			5
5	58992			25709						57716			26475			4
6	58971			25721						57695			26488			3
7	58949			25734						57674			26501			2
8	58928			25747						57653			26514			1
9	58906			25760						57632			26526			0

$$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$$

(h) (d) (a) (Z)

Fig. 78

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Altitude Correction of Sun 6° - 90°

Obs. alt.	Height of Eye (m)																	Obs. alt.
	0	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17		
	(+)																	
6 0	7.5	4.3	3.8	3.4	3.0	2.7	2.4	2.1	2.0	1.7	1.4	1.2	0.9	0.7	0.4	0.2	0.0	6 0
20	7.8	4.7	4.2	3.8	3.4	3.1	2.7	2.4	2.1	1.8	1.6	1.3	1.1	0.8	0.6	0.4	20	
40	8.2	5.1	4.7	4.2	3.8	3.4	3.1	2.8	2.5	2.2	1.9	1.7	1.4	1.2	1.0	0.8	40	
7 0	8.5	5.4	4.9	4.5	4.1	3.8	3.4	3.1	2.8	2.5	2.2	2.0	1.8	1.5	1.3	1.1	7 0	
20	8.8	5.7	5.2	4.8	4.4	4.1	3.7	3.4	3.1	2.9	2.6	2.3	2.1	1.8	1.6	1.4	20	
40	9.1	6.0	5.5	5.1	4.7	4.3	4.0	3.7	3.4	3.1	2.9	2.6	2.4	2.1	1.9	1.7	40	
8 0	9.4	6.3	5.8	5.4	5.0	4.6	4.3	4.0	3.7	3.4	3.1	2.9	2.6	2.4	2.2	2.0	8 0	
20	9.6	6.5	6.0	5.6	5.2	4.9	4.5	4.2	3.9	3.7	3.4	3.1	2.9	2.6	2.4	2.2	20	
40	9.8	6.7	6.2	5.8	5.4	5.1	4.8	4.4	4.1	3.9	3.6	3.4	3.1	2.9	2.7	2.4	40	
9 0	10.0	6.9	6.4	6.0	5.6	5.3	5.0	4.7	4.4	4.1	3.8	3.6	3.3	3.1	2.9	2.6	9 0	
20	10.2	7.1	6.7	6.2	5.8	5.5	5.2	4.9	4.6	4.3	4.0	3.8	3.5	3.3	3.1	2.8	20	
40	10.4	7.3	6.8	6.4	6.0	5.7	5.4	5.0	4.7	4.5	4.2	4.0	3.7	3.5	3.3	3.0	40	
10 0	10.6	7.5	7.0	6.6	6.2	5.9	5.5	5.2	4.9	4.7	4.4	4.1	3.9	3.7	3.4	3.2	10 0	
30	10.8	7.7	7.3	6.8	6.5	6.1	5.8	5.5	5.2	4.9	4.6	4.4	4.1	3.9	3.7	3.5	30	
11 0	11.1	8.0	7.5	7.1	6.7	6.3	6.0	5.7	5.4	5.1	4.9	4.6	4.4	4.1	3.9	3.7	11 0	
30	11.3	8.2	7.7	7.3	6.9	6.5	6.2	5.9	5.6	5.3	5.1	4.8	4.6	4.3	4.1	3.9	30	
12 0	11.5	8.4	7.9	7.5	7.1	6.7	6.4	6.1	5.8	5.5	5.3	5.0	4.8	4.5	4.3	4.1	12 0	
30	11.6	8.5	8.1	7.6	7.3	6.9	6.6	6.3	6.0	5.7	5.4	5.2	4.9	4.7	4.5	4.3	30	
13 0	11.8	8.7	8.2	7.8	7.4	7.1	6.7	6.4	6.1	5.9	5.6	5.4	5.1	4.9	4.7	4.4	13 0	
30	11.9	8.8	8.4	8.0	7.6	7.2	6.8	6.5	6.3	6.0	5.8	5.5	5.3	5.0	4.8	4.6	30	
14 0	12.1	9.0	8.5	8.1	7.7	7.4	7.0	6.7	6.4	6.2	5.9	5.7	5.4	5.2	4.9	4.7	14 0	
30	12.2	9.1	8.7	8.2	7.8	7.5	7.2	6.9	6.6	6.3	6.0	5.8	5.5	5.3	5.1	4.9	30	
15 0	12.3	9.3	8.8	8.4	8.0	7.6	7.3	7.0	6.7	6.4	6.2	5.9	5.7	5.4	5.2	5.0	15 0	
16 0	12.6	9.5	9.0	8.6	8.2	7.8	7.5	7.2	6.9	6.7	6.4	6.1	5.9	5.7	5.4	5.2	16 0	
17 0	12.8	9.7	9.2	8.8	8.4	8.1	7.7	7.4	7.1	6.9	6.6	6.4	6.1	5.9	5.6	5.4	17 0	
18 0	12.9	9.9	9.4	9.0	8.6	8.2	7.9	7.6	7.3	7.0	6.8	6.5	6.3	6.1	5.8	5.6	18 0	
19 0	13.1	10.0	9.6	9.1	8.7	8.4	8.1	7.8	7.5	7.2	6.9	6.7	6.4	6.2	6.0	5.8	19 0	
20 0	13.3	10.2	9.7	9.3	8.9	8.6	8.2	7.9	7.6	7.4	7.1	6.9	6.6	6.4	6.2	5.9	20 0	
22 0	13.5	10.4	10.0	9.5	9.1	8.8	8.5	8.2	7.9	7.6	7.3	7.1	6.8	6.6	6.4	6.2	22 0	
24 0	13.7	10.6	10.2	9.8	9.4	9.0	8.7	8.4	8.1	7.8	7.6	7.3	7.1	6.8	6.6	6.4	24 0	
26 0	13.9	10.8	10.4	9.9	9.6	9.2	8.9	8.6	8.3	8.0	7.8	7.5	7.3	7.0	6.8	6.6	26 0	
28 0	14.1	11.0	10.5	10.1	9.7	9.4	9.0	8.7	8.4	8.2	7.9	7.7	7.4	7.2	7.0	6.7	28 0	
30 0	14.2	11.1	10.7	10.2	9.9	9.5	9.2	8.9	8.6	8.3	8.1	7.9	7.6	7.3	7.1	6.9	30 0	
32 0	14.3	11.2	10.8	10.4	10.0	9.6	9.3	9.0	8.7	8.4	8.2	7.9	7.7	7.4	7.2	7.0	32 0	
34 0	14.4	11.4	10.9	10.5	10.1	9.7	9.4	9.1	8.8	8.5	8.3	8.0	7.8	7.6	7.3	7.1	34 0	
36 0	14.5	11.5	11.0	10.6	10.2	9.8	9.5	9.2	8.9	8.6	8.4	8.1	7.9	7.7	7.4	7.2	36 0	
38 0	14.6	11.5	11.1	10.7	10.3	9.9	9.6	9.3	9.0	8.7	8.5	8.2	8.0	7.7	7.5	7.3	38 0	
40 0	14.7	11.6	11.2	10.7	10.4	10.0	9.7	9.4	9.1	8.8	8.6	8.3	8.1	7.8	7.6	7.4	40 0	
45 0	14.9	11.8	11.3	10.9	10.5	10.2	9.9	9.6	9.3	9.0	8.7	8.5	8.2	8.0	7.8	7.6	45 0	
50 0	15.0	12.0	11.5	11.1	10.7	10.3	10.0	9.7	9.4	9.1	8.9	8.6	8.4	8.2	7.9	7.7	50 0	
55 0	15.2	12.1	11.6	11.2	10.8	10.5	10.1	9.8	9.5	9.3	9.0	8.8	8.5	8.3	8.1	7.8	55 0	
60 0	15.3	12.2	11.7	11.3	10.9	10.6	10.2	9.9	9.6	9.4	9.1	8.9	8.6	8.4	8.2	7.9	60 0	
65 0	15.4	12.3	11.8	11.4	11.0	10.7	10.3	10.0	9.7	9.5	9.2	9.0	8.7	8.5	8.3	8.0	65 0	
70 0	15.4	12.4	11.9	11.5	11.1	10.7	10.4	10.1	9.8	9.6	9.3	9.0	8.8	8.6	8.3	8.1	70 0	
75 0	15.5	12.4	12.0	11.6	11.2	10.8	10.5	10.2	9.9	9.6	9.4	9.1	8.9	8.6	8.4	8.2	75 0	
80 0	15.6	12.5	12.1	11.6	11.3	10.9	10.6	10.3	10.0	9.7	9.5	9.2	9.0	8.7	8.5	8.3	80 0	
85 0	15.7	12.6	12.1	11.7	11.3	11.0	10.7	10.3	10.1	9.8	9.5	9.3	9.0	8.8	8.6	8.4	85 0	
90 0	15.8	12.7	12.2	11.8	11.4	11.0	10.7	10.4	10.1	9.9	9.6	9.3	9.1	8.9	8.6	8.4	90 0	
	0.0	3.1	3.6	4.0	4.4	4.7	5.0	5.3	5.6	5.9	6.2	6.4	6.6	6.9	7.1	7.3		
	0.0	3.6	4.1	4.6	5.1	5.5	5.9	6.2	6.6	6.9	7.2	7.5	7.8	8.0	8.3	8.5		

Corr. for S.D.	Jan.	Feb.	Mar.	Apr.	May.	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.
Lower \odot	+ 0.5	+ 0.5	+ 0.4	+ 0.2	+ 0.1	0.0	0.0	+ 0.1	+ 0.2	+ 0.3	+ 0.5	+ 0.5
Upper \odot	-32.0	-32.0	-31.9	-31.7	-31.6	-31.5	-31.5	-31.6	-31.7	-31.8	-32.0	-32.0

Diff. of temp. between air and sea water	C°	0'	1'	2'	3'	4'	5'	6'	7'	8'	9'	10'	11'	12'	13'	14'	
	Corr.	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	
		when air temp > Sea water temp (+) * Air temp. at height of eye air temp < Sea water temp (-)															

Fig. 79

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Example 13

At 03^h 30^m p.m. on 12 December 1956, a navigator observed the altitude of the sun's upper limb (\odot) as 36°27'2 in D.R.P. 04°06'S, 41°28'E.

What were I and Zc?

Where: Chronometer Time was 0^h 40^m 20^s, chronometer error \ominus 2^m 35^s, index error \ominus 1.7, height of eye 18 meters, air temperature 29°C, and sea water temperature 26°C (see Figs. 80-87).

Solution

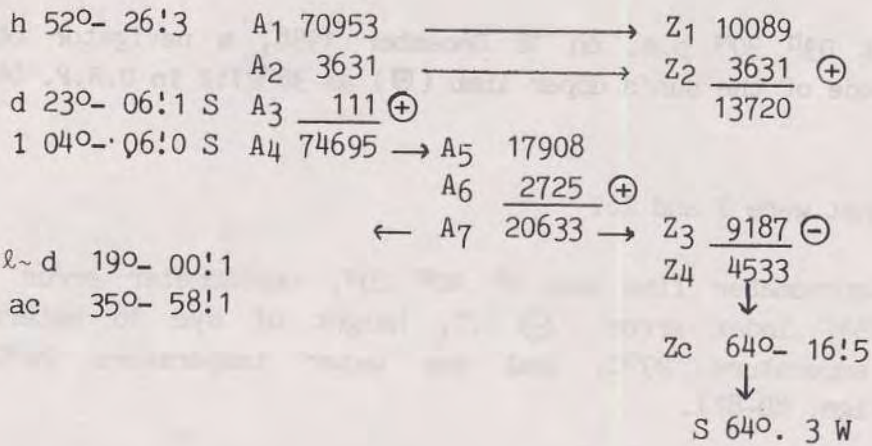
1) To calculate G.D.

Ship's Time 12/12/56	15 ^h 30 ^m 00 ^s (\leftarrow 03 ^h 30 ^m 00 ^s p.m.)	U=L.M.T. \pm L
L. in T. (41°-28'E)	<u>2 45 52</u>	\ominus (41°=2 ^h 44 ^m 28' = 1 ^m 52 ^s)
G.D.	12/12/56 12 ^h 44 ^m 08 ^s	G.D.=Ship's Time+Long in Time

2) To calculate d and h

Chro. T.	12 ^h 40 ^m 20 ^s	(\leftarrow 0 ^h 40 ^m 20 ^s)	
C.E.	<u>2 35</u>	\ominus	
U.	12/12/56 12 37 45	\rightarrow d = 23°- 06.1S	(by almanac)
			$h_G = U + E \odot$
E \odot (by almanac)	<u>12 06 08</u>	\oplus	
h_G	24 43 53		
\downarrow	<u>24</u>	\ominus	
h_C	00 43 53	\rightarrow 40 ^m = 10°, 3 ^m = 45', 52 ^s = 13', 1 ^s = 0!3)	
h_G	10°-58!3		
L (41°28'E)	<u>41°-28!0</u>	\oplus	$h = h_G \pm L$ (East long. \oplus) West long. \ominus)
h_i	<u>52°-26!3</u>		

3) To calculate ac and zc



4) To calculate at and I

Sex. Alt. $\ominus \ 36^{\circ} - 27!2$
 I.E. $\quad \quad \quad \underline{1.7} \ominus$
 Obs. Alt. $\ 36^{\circ} - 25!5$
 Corr. 1 $\quad \quad \quad \underline{7!0} \oplus$
 $\quad \quad \quad \ 36^{\circ} - 32!5$
 Corr. 2 $\quad \quad \quad \underline{32!0} \ominus$
 $\quad \quad \quad \ 36^{\circ} - 00!5$
 Corr. 3 $\quad \quad \quad \underline{0!6} \oplus$
 True Alt. $\oplus \ 36^{\circ} - 01!1 \text{ (at)}$
 ac $\quad \quad \quad \underline{35^{\circ} - 58!1} \ominus$
 I $\quad \quad \quad \oplus \ 3!0$

Ans. $I = \oplus 3!0 \quad Zc = S \ 64^{\circ} . 3 \ W$

12 December 1956

U E			\odot	p.p. of d		
			d			
h	h	m s	'	h	m	'
0	12	6 23	S23 3.8	0	0	0.0
2		21	4.2	10		0
4		19	4.5	20		1
6		16	4.9	30		1
8		14	5.3	40		1
10		12	5.7	0	50	2
12	12	6 9	S23 6.0	1	0	0.2
14		7	8.4	10		2
16		5	6.7	20		3
18		2	7.1	30		3
20		6 0	7.4	40		3
22		5 58	7.8	1	50	4
24	12	5 55	S23 8.1	2	0	0.4

Fig. 80

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_u + A_5 + A_6 = A_7$ & d contrary name $\rightarrow \ell + d$
 & d same name $\rightarrow \ell - d$
 (h) (d) (l) (l+d) (a)

°	5°										53'									
	A_1 h	A_2	P.P.	A_3	A_4 l+d	P.P.	Z_1 h	Z_2 Z	P.P.	A_1 h	A_2	P.P.	A_3	A_4 l+d	P.P.	Z_1 h	Z_2 Z	P.P.		
0	↑ 71632		o	↓ 19217	o	↑ 10347	o	↑ 70094	o	↓ 19909		↑ 9765	o	60						
1	71606		3	19228	1	10337	1	70969	1	19921		9756	1	59						
2	71580		5	19240	2	10327	2	70044	2	19932		9746	2	58						
3	71554		8	19251	3	10317	3	70019	3	19944		9737	3	57						
4	71528		10	19263	4	10307	4	69993	4	19956		9727	4	56						
5	71502		13	19274	6	10298	5	69968	5	19967		9718	5	55						
6	71476		16	19286	7	10288	6	69943	6	19979		9708	6	54						
7	71451		18	19297	8	10278	7	69917	7	19991		9699	7	53						
8	71425		21	19309	9	10268	8	69892	8	20002		9689	8	52						
9	71399		23	19320	10	10258	9	69867	9	20014		9680	9	51						
10	71373		o	19332	o	10248	o	69842	o	20026		9670	o	50						
11	71347		3	19343	1	10239	1	69816	1	20037		9661	1	49						
12	71321		5	19355	2	10229	2	69791	2	20049		9651	2	48						
13	71296		8	19366	3	10219	3	69766	3	20060		9642	3	47						
14	71270		10	19378	4	10209	4	69741	4	20072		9632	4	46						
15	71244		13	19389	6	10199	5	69715	5	20084		9623	5	45						
16	71218		16	19401	7	10190	6	69690	6	20095		9614	6	44						
17	71193		18	19412	8	10180	7	69665	7	20107		9604	7	43						
18	71167		21	19424	9	10170	8	69640	8	20119		9595	8	42						
19	71141		23	19435	10	10160	9	69615	9	20130		9585	9	41						
20	71115		o	19447	o	10151	o	69590	o	20142		9576	o	40						
21	71090		3	19458	1	10141	1	69564	1	20154		9566	1	39						
22	71064		5	19470	2	10131	2	69539	2	20165		9557	2	38						
23	71038		8	19481	3	10121	3	69514	3	20177		9548	3	37						
24	71013		10	19493	4	10112	4	69489	4	20189		9538	4	36						
25	70987		13	19504	6	10102	5	69464	5	20200		9529	5	35						
26	70961		16	19516	7	10092	6	69439	6	20212		9520	6	34						
27	70936		18	19527	8	10082	7	69414	7	20224		9510	7	33						
28	70910		21	19539	9	10073	8	69389	8	20235		9501	8	32						
29	70884		23	19550	10	10063	9	69364	9	20247		9491	9	31						
30	70859		o	19562	o	10053	o	69338	o	20259		9482	o	30						
31	70833		3	19573	1	10044	1	69313	1	20271		9473	1	29						
32	70808		5	19585	2	10034	2	69288	2	20282		9463	2	28						
33	70782		8	19597	3	10024	3	69263	3	20294		9454	3	27						
34	70756		10	19608	4	10015	4	69239	4	20306		9445	4	26						
35	70731		13	19620	6	10005	5	69213	5	20317		9435	5	25						
36	70705		16	19631	7	9995	6	69188	6	20329		9426	6	24						
37	70680		18	19643	8	9986	7	69163	7	20341		9417	7	23						
38	70654		20	19654	9	9976	8	69138	8	20352		9408	8	22						
39	70629		23	19666	10	9966	9	69113	9	20364		9398	9	21						
40	70603		o	19677	o	9957	o	69088	o	20376		9389	o	20						
41	70578		3	19689	1	9947	1	69063	1	20388		9380	1	19						
42	70552		5	19701	2	9937	2	69038	2	20399		9370	2	18						
43	70527		8	19712	3	9928	3	69013	3	20411		9361	3	17						
44	70501		10	19724	4	9918	4	68988	4	20423		9352	4	16						
45	70476		13	19735	6	9909	5	68964	5	20435		9343	5	15						
46	70450		16	19747	7	9899	6	68939	6	20446		9333	6	14						
47	70425		18	19758	8	9889	7	68914	7	20458		9324	7	13						
48	70399		20	19770	9	9880	8	68889	8	20470		9315	8	12						
49	70374		23	19782	10	9870	9	68864	9	20481		9306	9	11						
50	70348		o	19793	o	9861	o	68839	o	20493		9296	o	10						
51	70323		3	19805	1	9851	1	68814	1	20505		9287	1	9						
52	70297		5	19816	2	9841	2	68789	2	20517		9278	2	8						
53	70272		8	19828	3	9832	3	68764	3	20528		9269	3	7						
54	70247		10	19840	4	9822	4	68740	4	20540		9259	4	6						
55	70221		13	19851	6	9813	5	68715	5	20552		9250	5	5						
56	70196		16	19863	7	9803	6	68690	6	20564		9241	6	4						
57	70171		18	19874	8	9794	7	68665	7	20575		9232	7	3						
58	70145		21	19886	9	9784	8	68640	8	20587		9223	8	2						
59	70120		23	19898	10	9775	9	68615	9	20599		9213	9	1						
60	↑ 70094		o	↓ 19909	o	↑ 9765	o	↑ 68591	o	↓ 20511		↑ 9204	o	0						

$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$
 (h) (d) (a) (z)

Fig. 81

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_4 + A_5 + A_6 = A_7$ ℓ & d contrary name $+\ell+d$
 (h) (d) (Z) (L+d) (a) ℓ & d same name $-\ell-d$

°	66						67°										
	A ₁ h	A ₂	P.P.	A ₃ L+d	A ₄	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₁ h	A ₂	P.P.	A ₃ L+d	A ₄	P.P.	Z ₁ h	Z ₂ Z
0	52778	0	29663	0	3927	0	51622	0	30463	0	3597	0	60				
1	52759	2	29676	1	3921	1	51603	2	30477	1	3592	1	59				
2	52739	4	29690	1	3916	1	51584	2	30490	1	3587	1	58				
3	52720	6	29703	4	3910	2	51565	4	30504	4	3581	2	57				
4	52700	8	29716	6	3905	2	51546	6	30517	5	3576	2	56				
5	52681	10	29730	7	3899	3	51527	8	30530	7	3571	3	55				
6	52662	11	29743	8	3894	4	51508	10	30544	8	3566	3	54				
7	52642	13	29756	10	3888	4	51489	11	30557	9	3560	4	53				
8	52623	15	29770	11	3882	5	51470	12	30571	10	3555	4	52				
9	52603	17	29783	13	3877	5	51451	13	30584	12	3549	5	51				
10	52584	0	29796	0	3871	0	51432	0	30597	0	3544	0	50				
11	52565	2	29809	1	3865	1	51413	2	30611	1	3539	1	49				
12	52545	4	29823	3	3860	1	51393	4	30624	3	3533	1	48				
13	52526	6	29836	4	3854	2	51374	6	30638	4	3528	2	47				
14	52507	8	29849	6	3849	2	51355	8	30651	5	3523	2	46				
15	52487	10	29863	7	3843	3	51336	10	30664	7	3517	3	45				
16	52468	12	29876	8	3838	4	51317	11	30678	8	3512	4	44				
17	52448	14	29889	10	3832	4	51298	13	30691	9	3507	4	43				
18	52429	16	29903	11	3826	5	51280	15	30705	10	3502	5	42				
19	52410	18	29916	13	3821	5	51261	17	30718	12	3496	5	41				
20	52390	0	29929	0	3815	0	51242	0	30732	0	3491	0	40				
21	52371	2	29943	1	3810	1	51223	2	30745	1	3486	1	39				
22	52352	4	29956	3	3804	1	51204	4	30758	3	3480	1	38				
23	52332	6	29969	4	3799	2	51185	6	30772	4	3475	2	37				
24	52313	8	29983	5	3793	2	51166	8	30785	6	3470	2	36				
25	52294	10	29996	7	3788	3	51147	10	30799	7	3465	3	35				
26	52275	11	30009	8	3782	3	51128	11	30812	8	3459	3	34				
27	52255	13	30023	9	3777	4	51109	13	30826	10	3454	4	33				
28	52236	15	30036	10	3771	4	51090	15	30839	11	3449	4	32				
29	52217	17	30049	12	3766	5	51071	17	30852	13	3444	5	31				
30	52197	0	30063	0	3760	0	51052	0	30866	0	3438	0	30				
31	52178	2	30076	1	3755	1	51033	2	30879	1	3433	1	29				
32	52159	4	30089	3	3749	1	51014	4	30893	3	3428	1	28				
33	52140	6	30103	4	3744	2	50996	6	30906	4	3423	2	27				
34	52120	8	30116	5	3738	2	50977	8	30920	5	3418	2	26				
35	52101	10	30129	7	3733	3	50958	10	30933	7	3412	3	25				
36	52082	11	30143	8	3727	3	50939	11	30946	8	3407	4	24				
37	52063	13	30156	9	3722	4	50920	13	30959	9	3402	4	23				
38	52043	15	30169	10	3716	4	50901	15	30973	10	3397	5	22				
39	52024	17	30183	12	3711	5	50882	17	30987	12	3392	5	21				
40	52005	0	30196	0	3705	0	50863	0	31000	0	3386	0	20				
41	51986	2	30209	1	3700	1	50844	2	31014	1	3381	1	19				
42	51967	4	30223	3	3695	1	50826	4	31027	3	3376	1	18				
43	51947	6	30236	4	3689	2	50807	6	31041	4	3371	2	17				
44	51928	8	30249	6	3684	2	50788	8	31054	5	3366	2	16				
45	51909	10	30263	7	3678	3	50769	10	31068	7	3360	3	15				
46	51890	11	30276	8	3673	4	50750	11	31081	8	3355	4	14				
47	51871	13	30290	10	3667	4	50732	13	31095	10	3350	4	13				
48	51852	15	30303	11	3662	5	50713	15	31108	11	3345	5	12				
49	51832	17	30316	13	3657	5	50694	17	31121	13	3340	5	11				
50	51813	0	30330	0	3651	0	50675	0	31135	0	3335	0	10				
51	51794	2	30343	1	3646	(1)	50656	2	31148	1	3330	1	9				
52	51775	4	30356	3	3640	1	50638	4	31162	3	3324	1	8				
53	51756	6	30370	4	3635	2	50619	6	31175	4	3319	2	7				
54	51737	8	30383	6	3630	2	50600	8	31189	5	3314	2	6				
55	51718	10	30397	7	3624	3	50581	10	31202	7	3309	3	5				
56	51698	11	30410	8	3619	4	50563	11	31216	8	3304	3	4				
57	51679	13	30423	10	3613	4	50544	13	31229	9	3299	4	3				
58	51660	15	30437	11	3608	5	50525	15	31243	10	3294	4	2				
59	51641	17	30450	13	3603	5	50506	17	31256	12	3289	5	1				
60	51622	0	30463	0	3597	0	50488	0	31270	0	3283	0	0				
	A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ Z ₁ Z ₂ a	P.P.	A ₁ h	P.P.	A ₂ a	P.P.	A ₃ d	A ₄ Z ₁ Z ₂ a	P.P.			
	293'		23'		297'		27'										

$Z_1 + Z_2 (= A_3) - Z_3 = Z_4$
 (A) (d) (a) (Z)

Fig. 82

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth.

$$A_1 + A_2 + A_3 = A_4 + A_5 + A_6 = A_7$$

(h) (d) (L)
(L+d) (a)

ℓ & d contrary name → ℓ+d

ℓ & d same name → ℓ-d

0	84°						85°										
	A ₁ h	A ₂	P.P.	A ₃ L+d	P.P.	Z ₁ h	Z ₂ Z	P.P.	A ₄ h	A ₅	P.P.	A ₆ L+d	P.P.	Z ₃ h	Z ₄ Z	P.P.	
0	↑ 34898	0	0	↓ 44774	0	↑ 239	0	0	↑ 34063	0	0	↓ 45642	0	↑ 106	0	0	60
1	34884	1	1	44789	1	237	0	0	34070	1	1	45657	1	161	0	0	59
2	34870	2	2	44803	2	235	0	0	34076	2	2	45671	2	163	0	0	58
3	34856	3	3	44817	3	233	0	0	34082	3	3	45686	3	162	0	0	57
4	34842	4	4	44831	4	231	0	0	34088	4	4	45700	4	161	0	0	56
5		5	5		5												
6	34828	6	6	44846	6	229	1	1	33994	6	6	45715	6	160	1	1	55
7	34814	7	7	44860	7	227	1	1	33981	7	7	45729	7	159	1	1	54
8	34800	8	8	44875	8	225	1	1	33967	8	8	45744	8	158	1	1	53
9	34786	9	9	44889	9	223	1	1	33953	9	9	45758	9	157	1	1	52
10	34772	10	10	44904	10	221	1	1	33939	10	10	45773	10	156	1	1	51
11		11	11		11												
12	34758	12	12	44918	12	219	0	0	33925	12	12	45787	12	155	0	0	50
13	34744	13	13	44933	13	217	0	0	33912	13	13	45802	13	154	0	0	49
14	34730	14	14	44947	14	215	0	0	33898	14	14	45816	14	153	0	0	48
15	34716	15	15	44962	15	213	0	0	33884	15	15	45831	15	152	0	0	47
16	34702	16	16	44976	16	211	0	0	33871	16	16	45845	16	150	0	0	46
17		17	17		17												
18	34688	18	18	44991	18	209	1	1	33857	18	18	45860	18	149	1	1	45
19	34674	19	19	45005	19	207	1	1	33843	19	19	45874	19	148	1	1	44
20	34660	20	20	45020	20	205	1	1	33830	20	20	45889	20	147	1	1	43
21	34646	21	21	45034	21	203	1	1	33816	21	21	45903	21	146	1	1	42
22	34632	22	22	45048	22	201	1	1	33802	22	22	45918	22	145	1	1	41
23		23	23		23												
24	34618	24	24	45063	24	199	0	0	33788	24	24	45932	24	144	0	0	40
25	34604	25	25	45077	25	197	0	0	33775	25	25	45947	25	143	0	0	39
26	34590	26	26	45092	26	195	0	0	33761	26	26	45961	26	142	0	0	38
27	34576	27	27	45105	27	193	0	0	33747	27	27	45976	27	141	0	0	37
28	34562	28	28	45121	28	191	0	0	33734	28	28	45990	28	140	0	0	36
29		29	29		29												
30	34548	30	30	45135	30	189	1	1	33720	30	30	46005	30	139	1	1	35
31	34534	31	31	45150	31	187	1	1	33706	31	31	46019	31	138	1	1	34
32	34520	32	32	45164	32	185	1	1	33693	32	32	46034	32	137	1	1	33
33	34507	33	33	45179	33	183	1	1	33679	33	33	46048	33	136	1	1	32
34	34493	34	34	45193	34	181	1	1	33665	34	34	46063	34	135	1	1	31
35		35	35		35												
36	34479	36	36	45208	36	179	0	0	33652	36	36	46077	36	134	0	0	30
37	34465	37	37	45222	37	177	0	0	33638	37	37	46092	37	133	0	0	29
38	34451	38	38	45237	38	175	0	0	33624	38	38	46106	38	132	0	0	28
39	34437	39	39	45251	39	173	1	1	33611	39	39	46121	39	131	1	1	27
40	34423	40	40	45265	40	171	1	1	33597	40	40	46135	40	130	1	1	26
41		41	41		41												
42	34409	42	42	45280	42	169	1	1	33583	42	42	46150	42	129	1	1	25
43	34395	43	43	45295	43	167	1	1	33570	43	43	46164	43	128	1	1	24
44	34381	44	44	45309	44	165	1	1	33556	44	44	46179	44	127	1	1	23
45	34368	45	45	45324	45	163	2	2	33542	45	45	46193	45	126	2	2	22
46	34354	46	46	45338	46	161	2	2	33529	46	46	46208	46	125	2	2	21
47		47	47		47												
48	34340	48	48	45353	48	159	0	0	33515	48	48	46222	48	124	0	0	20
49	34326	49	49	45367	49	157	0	0	33501	49	49	46237	49	123	0	0	19
50	34312	50	50	45381	50	155	0	0	33488	50	50	46251	50	122	0	0	18
51	34298	51	51	45396	51	153	0	0	33474	51	51	46266	51	121	0	0	17
52	34284	52	52	45410	52	151	0	0	33461	52	52	46280	52	120	0	0	16
53		53	53		53												
54	34271	54	54	45425	54	149	1	1	33447	54	54	46295	54	119	1	1	15
55	34257	55	55	45439	55	147	1	1	33433	55	55	46309	55	118	1	1	14
56	34243	56	56	45454	56	145	1	1	33420	56	56	46324	56	117	1	1	13
57	34229	57	57	45468	57	143	1	1	33406	57	57	46338	57	116	1	1	12
58	34215	58	58	45483	58	141	1	1	33393	58	58	46353	58	115	1	1	11
59		59	59		59												
60	34201	60	60	45497	60	139	0	0	33379	60	60	46367	60	114	0	0	10
61	34188	61	61	45512	61	137	0	0	33365	61	61	46382	61	113	0	0	9
62	34174	62	62	45526	62	135	0	0	33352	62	62	46396	62	112	0	0	8
63	34160	63	63	45541	63	133	0	0	33338	63	63	46411	63	111	0	0	7
64	34146	64	64	45555	64	131	0	0	33325	64	64	46425	64	110	0	0	6
65		65	65		65												
66	34132	66	66	45570	66	129	1	1	33311	66	66	46440	66	109	1	1	5
67	34119	67	67	45584	67	127	1	1	33298	67	67	46454	67	108	1	1	4
68	34105	68	68	45599	68	125	1	1	33284	68	68	46469	68	107	1	1	3
69	34091	69	69	45613	69	123	1	1	33270	69	69	46483	69	106	1	1	2
70	34077	70	70	45628	70	121	1	1	33257	70	70	46498	70	105	1	1	1
71	↑ 34063	71	71	↓ 45642	71	↑ 119	0	0	↑ 33243	71	71	↓ 46512	71	↑ 106	0	0	0
	A ₁ h	P.P.	A ₇ a	P.P.	A ₂ d	A ₃ L	Z ₁ h	Z ₂ Z	P.P.	A ₄ h	P.P.	A ₅ a	P.P.	A ₆ L+d	Z ₃ h	Z ₄ Z	P.P.
	715°				5°					714°							

$$Z_1 + Z_2 (= A_1) - Z_3 = Z_4$$

(h) (d)
(a) (Z)

Fig. 83

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

Table of Altitude and Azimuth

$A_1 + A_2 + A_3 = A_4, A_5 + A_6 = A_7$
 (h) (d) (l) (l+d) (a)

ℓ & d contrary name → ℓ+d
 ℓ & d same name → ℓ-d

o	18													13'														
	A_1	A_2	P.P.	A_3	A_4	P.P.	A_5	A_6	P.P.	A_1	A_2	P.P.	A_3	A_4	P.P.	A_5	A_6	P.P.	A_1	A_2	P.P.	A_3	A_4	P.P.				
	h	a		d	i	a	d	i	a	h	a		d	i	a	h	a		d	i	a	h	a		d	i	a	
0	161133	0	0	2447	0	0	51002	0	0	156478	0	0	2724	0	0	148736	0	0	43371	0	0	60						
1	161054	8	0	2452	1	0	50963	4	0	156403	8	0	2729	1	0	48699	4	0	43334	4	0	59						
2	160974	16	0	2455	1	0	50921	8	0	156327	15	0	2731	1	0	48662	7	0	43298	7	0	58						
3	160895	24	0	2461	2	0	50885	12	0	156252	23	0	2734	2	0	48626	14	0	43262	14	0	57						
4	160815	32	0	2465	2	0	50847	16	0	156177	30	0	2743	2	0	48589	14	0	43226	15	0	56						
5	160736	40	0	2470	3	0	50808	20	0	156101	38	0	2748	3	0	48553	18	0	43189	19	0	55						
6	160656	47	0	2474	3	0	50769	23	0	156025	46	0	2753	3	0	48516	22	0	43153	22	0	54						
7	160577	55	0	2479	4	0	50731	27	0	155951	53	0	2757	4	0	48480	25	0	43117	25	0	53						
8	160498	63	0	2483	4	0	50692	31	0	155876	61	0	2762	4	0	48443	29	0	43081	30	0	52						
9	160419	71	0	2488	5	0	50653	35	0	155801	68	0	2767	5	0	48407	32	0	43045	32	0	51						
10	160340	0	0	2492	0	0	50615	0	0	155727	0	0	2772	0	0	48371	0	0	43009	0	0	50						
11	160261	8	0	2497	1	0	50576	4	0	155652	8	0	2776	1	0	48334	4	0	42973	4	0	49						
12	160182	16	0	2501	1	0	50538	8	0	155577	15	0	2781	1	0	48298	7	0	42937	7	0	48						
13	160103	24	0	2506	2	0	50500	12	0	155502	23	0	2786	2	0	48262	11	0	42901	11	0	47						
14	160024	32	0	2510	2	0	50461	15	0	155428	30	0	2791	3	0	48226	15	0	42865	15	0	46						
15	159945	40	0	2515	3	0	50423	19	0	155353	38	0	2796	3	0	48189	19	0	42829	19	0	45						
16	159867	47	0	2520	3	0	50385	23	0	155279	45	0	2800	3	0	48153	22	0	42793	22	0	44						
17	159788	55	0	2524	4	0	50346	27	0	155204	53	0	2805	4	0	48117	26	0	42757	26	0	43						
18	159710	63	0	2529	4	0	50308	30	0	155130	60	0	2810	4	0	48081	30	0	42721	30	0	42						
19	159631	71	0	2533	5	0	50270	34	0	155056	68	0	2815	5	0	48045	33	0	42685	33	0	41						
20	159553	0	0	2538	0	0	50232	0	0	154982	0	0	2820	0	0	48009	0	0	42649	0	0	40						
21	159475	8	0	2542	1	0	50194	4	0	154907	7	0	2824	1	0	47973	4	0	42613	4	0	39						
22	159397	15	0	2547	1	0	50156	8	0	154833	15	0	2829	1	0	47937	7	0	42577	7	0	38						
23	159319	23	0	2552	2	0	50118	12	0	154759	22	0	2834	2	0	47901	11	0	42541	11	0	37						
24	159240	31	0	2556	2	0	50080	15	0	154685	29	0	2839	3	0	47865	14	0	42505	14	0	36						
25	159163	39	0	2561	3	0	50042	19	0	154612	37	0	2844	3	0	47829	18	0	42469	18	0	35						
26	159085	47	0	2565	3	0	50004	23	0	154538	44	0	2849	3	0	47793	22	0	42433	22	0	34						
27	159007	54	0	2570	4	0	49966	27	0	154464	51	0	2853	4	0	47757	25	0	42397	25	0	33						
28	158929	62	0	2575	4	0	49928	30	0	154390	58	0	2858	4	0	47721	29	0	42361	29	0	32						
29	158851	69	0	2579	5	0	49890	34	0	154317	66	0	2863	5	0	47685	32	0	42325	32	0	31						
30	158774	0	0	2584	0	0	49852	0	0	154243	0	0	2868	0	0	47649	0	0	42289	0	0	30						
31	158696	8	0	2588	1	0	49815	4	0	154170	7	0	2873	1	0	47613	4	0	42253	4	0	29						
32	158619	15	0	2593	1	0	49777	8	0	154096	15	0	2878	1	0	47577	7	0	42217	7	0	28						
33	158541	23	0	2598	2	0	49739	12	0	154023	22	0	2883	2	0	47541	11	0	42181	11	0	27						
34	158464	31	0	2602	2	0	49702	15	0	153950	29	0	2887	3	0	47505	14	0	42145	14	0	26						
35	158387	39	0	2607	3	0	49664	19	0	153876	37	0	2892	3	0	47469	18	0	42109	18	0	25						
36	158310	47	0	2612	3	0	49626	23	0	153803	44	0	2897	3	0	47433	21	0	42073	21	0	24						
37	158233	54	0	2616	4	0	49589	27	0	153730	52	0	2902	4	0	47397	25	0	42037	25	0	23						
38	158155	62	0	2621	4	0	49551	30	0	153657	59	0	2907	4	0	47361	28	0	42001	28	0	22						
39	158079	69	0	2626	5	0	49514	34	0	153584	67	0	2912	5	0	47325	32	0	41965	32	0	21						
40	158002	0	0	2630	0	0	49477	0	0	153511	0	0	2917	0	0	47289	0	0	41929	0	0	20						
41	157925	8	0	2635	0	0	49439	4	0	153438	7	0	2922	1	0	47253	4	0	41893	4	0	19						
42	157848	15	0	2639	1	0	49402	7	0	153365	14	0	2926	1	0	47217	7	0	41857	7	0	18						
43	157771	23	0	2644	1	0	49365	11	0	153293	22	0	2931	2	0	47181	11	0	41821	11	0	17						
44	157695	31	0	2649	2	0	49327	15	0	153220	29	0	2936	3	0	47145	14	0	41785	14	0	16						
45	157618	39	0	2653	2	0	49290	19	0	153148	36	0	2941	3	0	47109	18	0	41749	18	0	15						
46	157542	46	0	2658	2	0	49253	22	0	153075	43	0	2946	3	0	47073	21	0	41713	21	0	14						
47	157465	54	0	2663	3	0	49216	26	0	153002	50	0	2951	4	0	47037	25	0	41677	25	0	13						
48	157389	62	0	2668	3	0	49179	30	0	152930	58	0	2956	4	0	47001	28	0	41641	28	0	12						
49	157313	69	0	2672	4	0	49142	33	0	152858	65	0	2961	5	0	46965	32	0	41605	32	0	11						

Table of Altitude and Azimuth

A₁ + A₂ + A₃ = A₄ A₅ + A₆ = A₇
(h) (d) (l) (l+d) (a)

ℓ & d contrary name → ℓ+d
ℓ & d same name → ℓ-d

Table with columns for Altitude (A1-A7) and Azimuth (Z1-Z4) for latitudes 64 and 65. Includes a summary row at the bottom with A1, P.P., A2, P.P., A3, A4, Z1, Z2, P.P., A5, P.P., A6, P.P., A7, A4, Z3, P.P.

Z₁ + Z₂ (= A₁) - Z₃ = Z₄
(h) (d) (a) (Z)

Fig. 85

Extracted from ASTRONOMICAL NAVIGATION TABLES, MARITIME SAFETY AGENCY, JAPAN.

How to fix the ship's position on position plotting sheet

To fix the ship's position by lines of position, we have to use specialized sheets as follows:

1. Plotting Sheet for Astronomical Position (Fig. 88)
2. Position plotting sheet (Fig. 89)
3. Nautical chart
4. Diagram of concentric circles in quadrates (Fig. 90)

Lines of position are drawn in a very small and limited area on the chart which corresponds to the earth, so we can apply the theory of the mid-latitude sailing ($D\text{-long} = \frac{\text{Dep}}{\cos \ell}$) to fix position on the chart.

One method for the applications of the mid-latitude sailing is to use a diagram of concentric circles in quadrates (Fig. 90).

This diagram consists of latitudinal line (\overline{EW}), longitudinal line (\overline{NS}), concentric circles and quadrates. In Figure 90, Point D is Dead Reckoning Position, the line \overline{NDS} is its longitude, \overline{EDW} is its latitude and each interval of circles and straight line is one nautical mile.

Example 14 (use Fig. 90)

A navigator observed the stars A and B at the same time and obtained $Zc = N 80^{\circ}W$, $I = + 5'.0$ by the star A and $Zc = S 30^{\circ}W$, $I = + 7'.0$ by the star B, in D.R.P. $30^{\circ}00'.0$ N, $150^{\circ}50'.0$ E.

Draw lines of position, fix ship's position, current set and current drift.

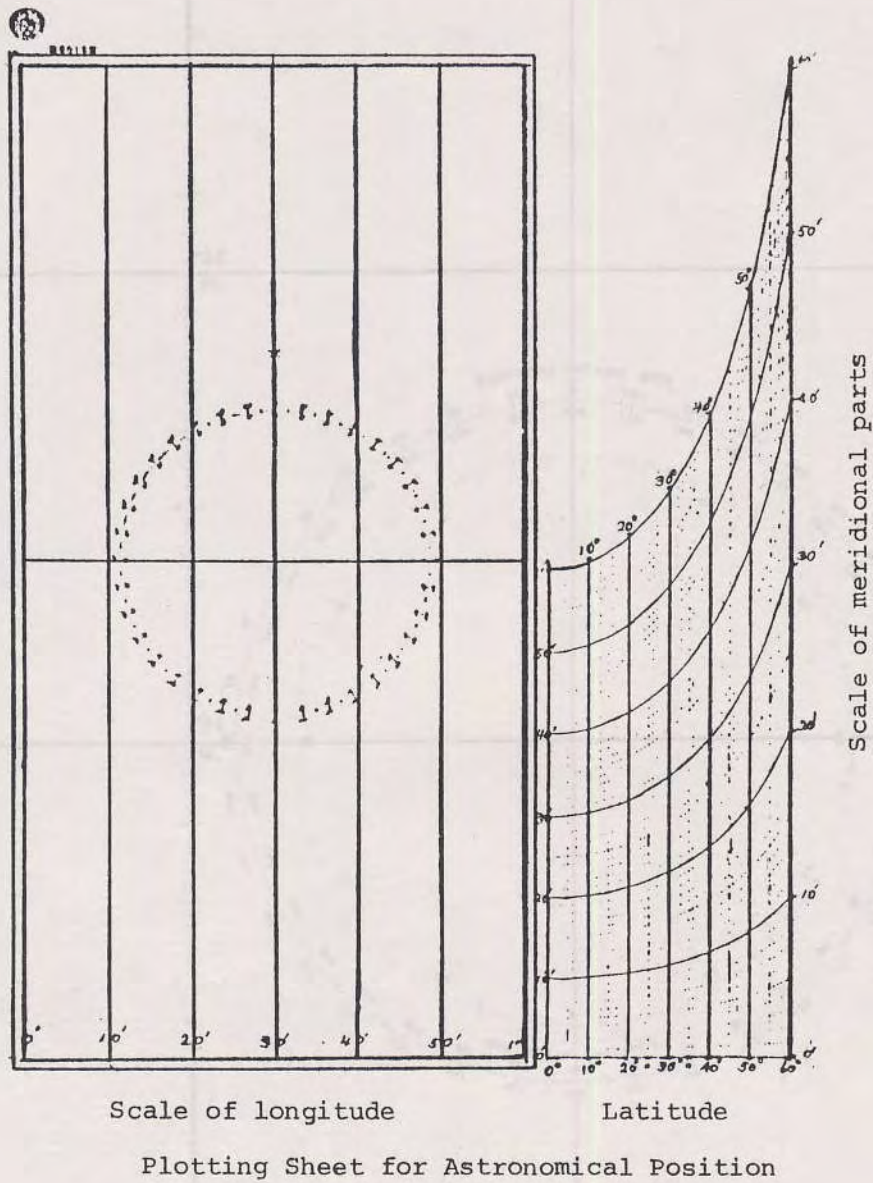


Fig. 88

Position Plotting Sheet

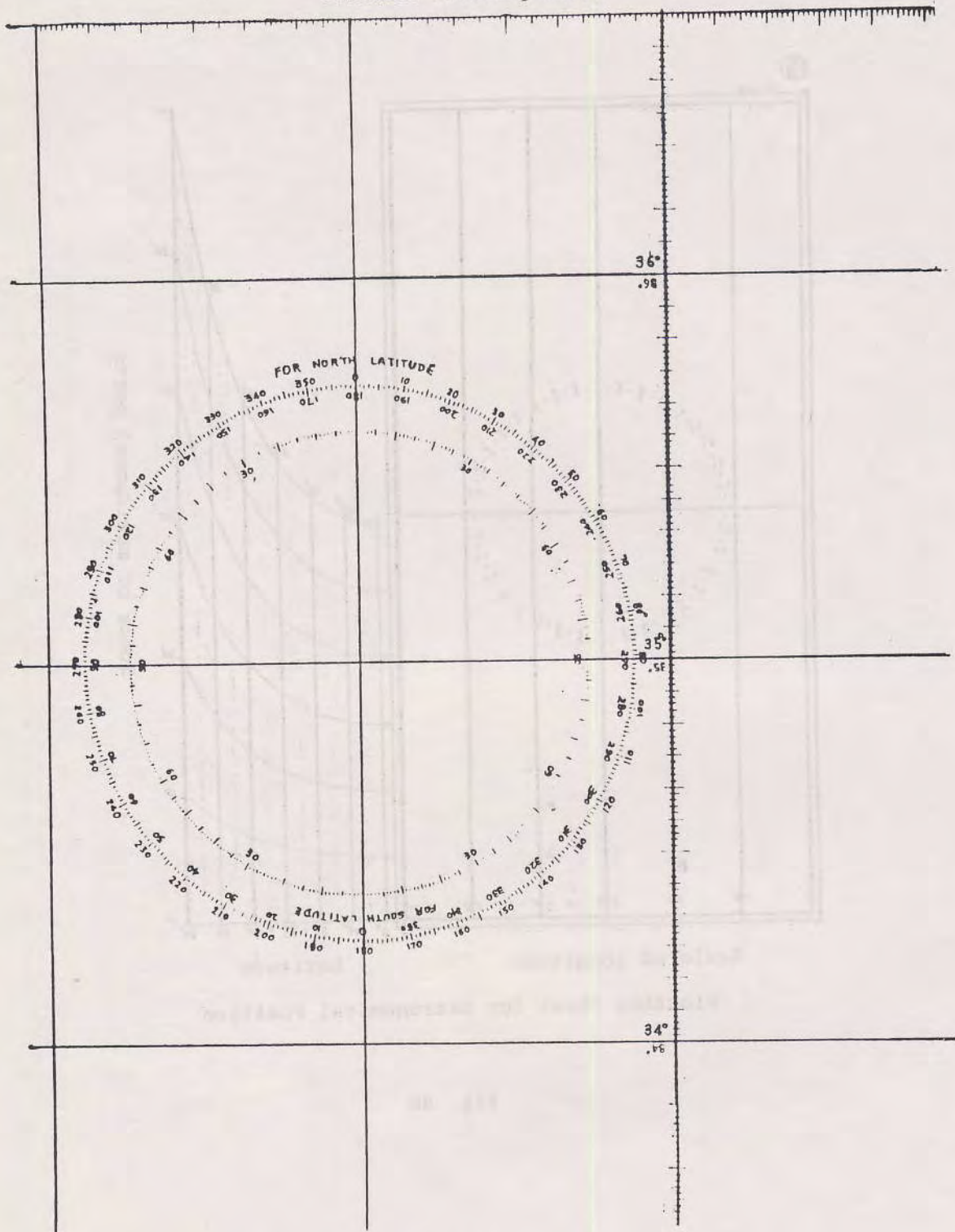


Fig. 89

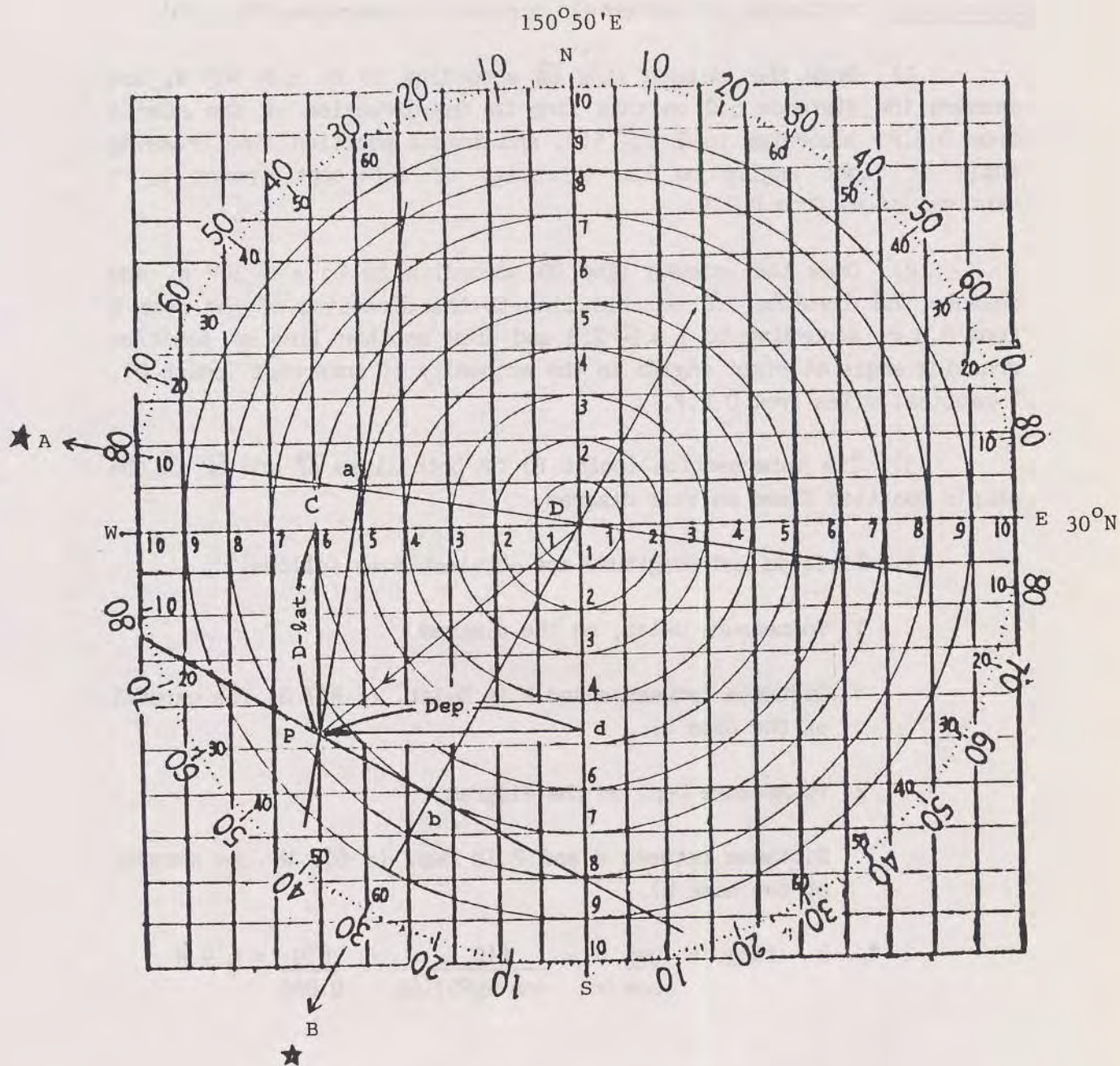


Fig. 90 Diagram of concentric circles in quadrates

Solution A by diagram of concentric circles in quadrates (Fig. 90)

1) Draw the azimuth line \vec{DA} according to $Zc = N 80^\circ W$, and measure the distance 5'.0 on this line to the direction of the star A from D.R.P. according to $I = \oplus 5'.0$, and draw a position line crossing angle at right angles on the extremity of intercept (point a) 5 nautical miles from D.R.P.

2) Draw the azimuth line \vec{DB} according to $Zc = S 30^\circ W$, and measure the distance 7'.0 on this line to the direction of the star B from D.R.P. according to $I = \oplus 7'.0$ and draw another line of position crossing angle at right angles in the extremity of intercept (point b), 7 nautical miles from D.R.P.

3) The intersection (point P) of both lines \vec{aP} and \vec{bP} is the ship's position fixed on this diagram.

4) Latitude and longitude are obtainable as follows,

1 To measure D-lat, on the diagram

Distance between c and P is D-lat. (= 4'.7 S...be careful of the name S).

2 To measure Dep. on the diagram

Distance between d and P is Dep. (= 6'.0 W...be careful of the name W).

$$* \quad D - \text{long.} = \frac{\text{Dep}}{\cos \ell_m} = \frac{6'.0}{\cos 29^\circ 57'.65} = \frac{6'.0}{0.866} = 6'.9 \text{ W}$$

* See page 3 of the textbook "COASTAL NAVIGATION" TD/TRB/37 Rev.2

So. D.R.P. Lat. $30^{\circ} - 00'0''$ N D.R.P. long. $150^{\circ} - 50'0''$ E
D - Lat. $\underline{4'7''}$ S \ominus D - long. $\underline{6'9''}$ W \ominus
 $29^{\circ} - 55'3''$ N $150^{\circ} - 43'1''$ E

Then fixed position \oplus { $29^{\circ} - 55'3''$ N
 $150^{\circ} - 43'1''$ E

5) Current set is \overrightarrow{DP} (= S 52° W) and current drift is the distance between point D and P (= 7'6).

Ans. Fixed position $29^{\circ} - 55'3''$ N, $150^{\circ} - 43'1''$ E
 Current set S 52° W
 Current drift 7'6 nautical miles

Solution B by a triangle ruler (Figs. 91-96)

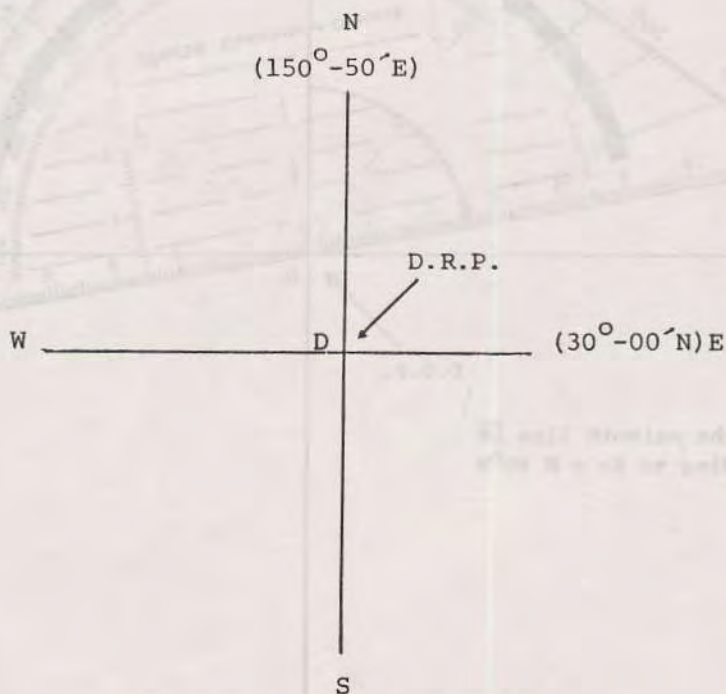


Fig. 91 Latitude and Longitude

- 1) Draw the latitude and longitude lines in your note book as shown in Figure 91. Intersection of these two lines in D.R.P.

2) About the star A (see Figs. 92, 93).

Draw the azimuth line \overline{DA} by a triangle ruler according to $Z_c = N 80^\circ W$ (see Fig. 92), and measure the distance 5'.0 on this line to the direction of star A from D.R.P. according to $I = \oplus 5'.0$, and draw a line of position crossing angle at right angles on the extremity of intercept (point a), 5 nautical miles from D.R.P. (see Fig. 93).

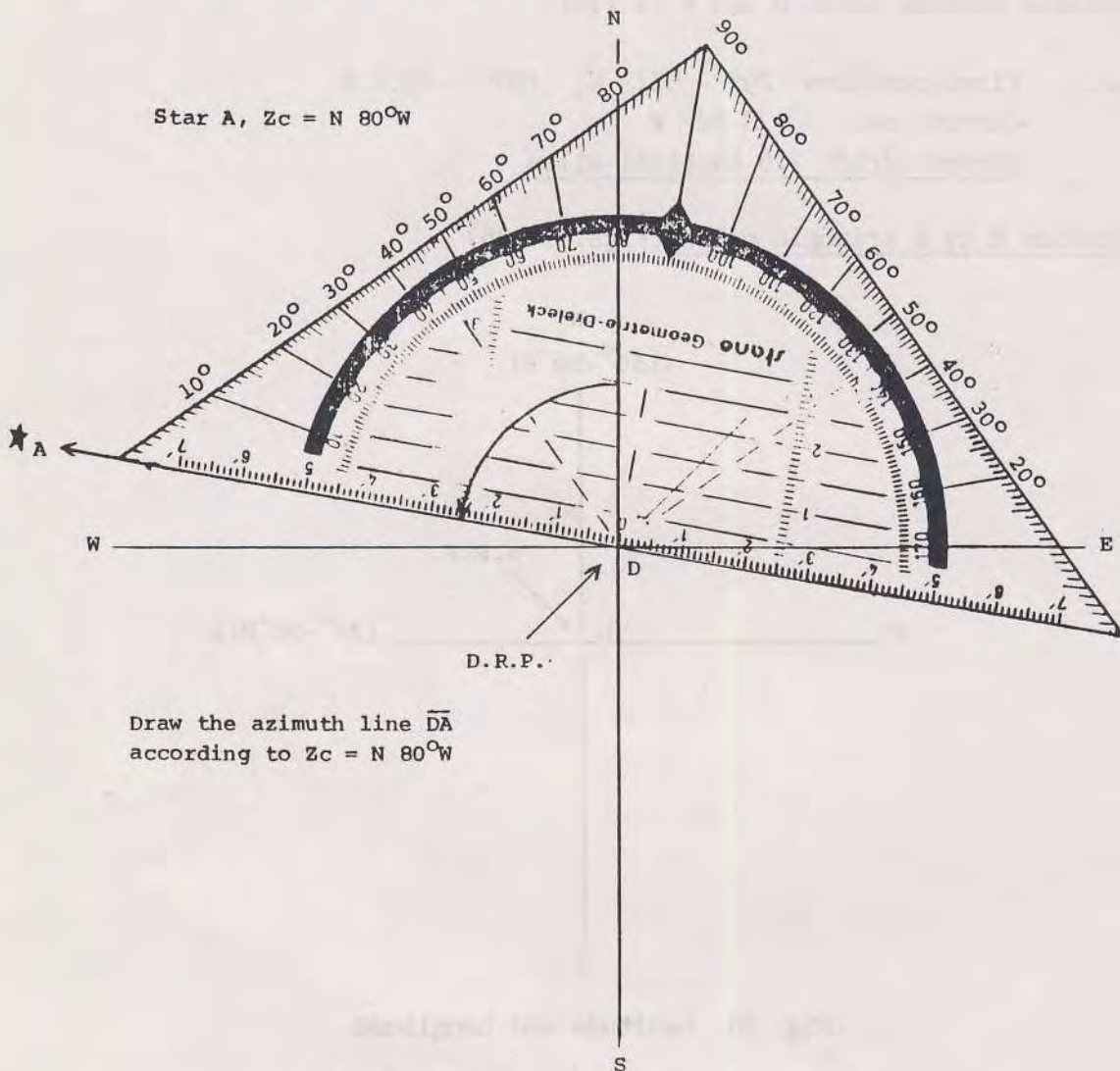
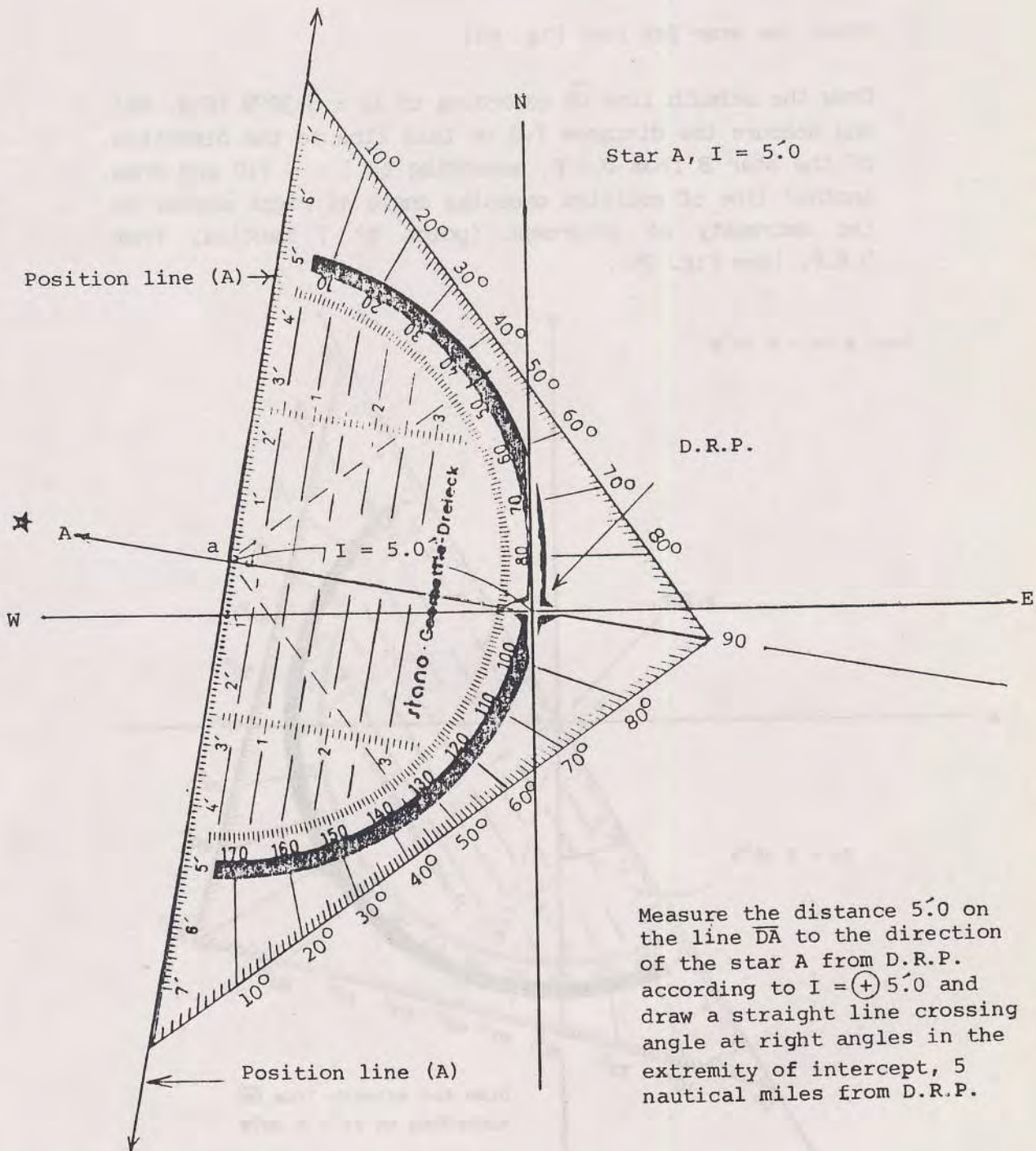


Fig. 92 How to draw line of position



Measure the distance 5.0 on the line \overline{DA} to the direction of the star A from D.R.P. according to $I = \oplus 5.0$ and draw a straight line crossing angle at right angles in the extremity of intercept, 5 nautical miles from D.R.P.

Fig. 93 How to draw line of position

3) About the star Bar (see Fig. 94)

Draw the azimuth line \overline{DB} according to $Z_c = S 30^\circ W$ (Fig. 94) and measure the distance 7.0 on this line to the direction of the star B from D.R.P. according to $I = + 7!0$ and draw another line of position crossing angle at right angles on the extremity of intercept (point b) 7 nautical from D.R.P. (see Fig. 95).

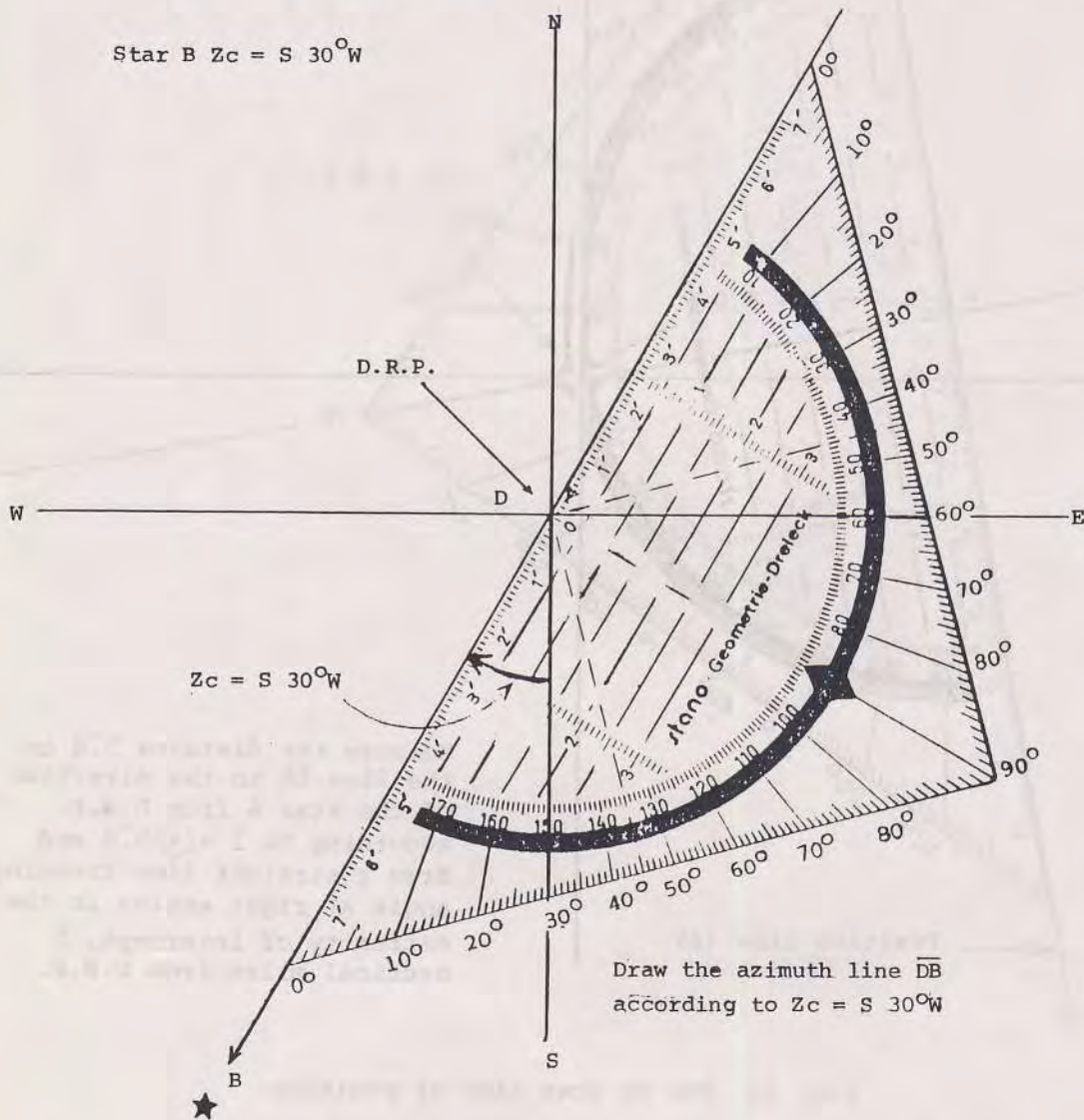


Fig. 94 How to draw line of Position

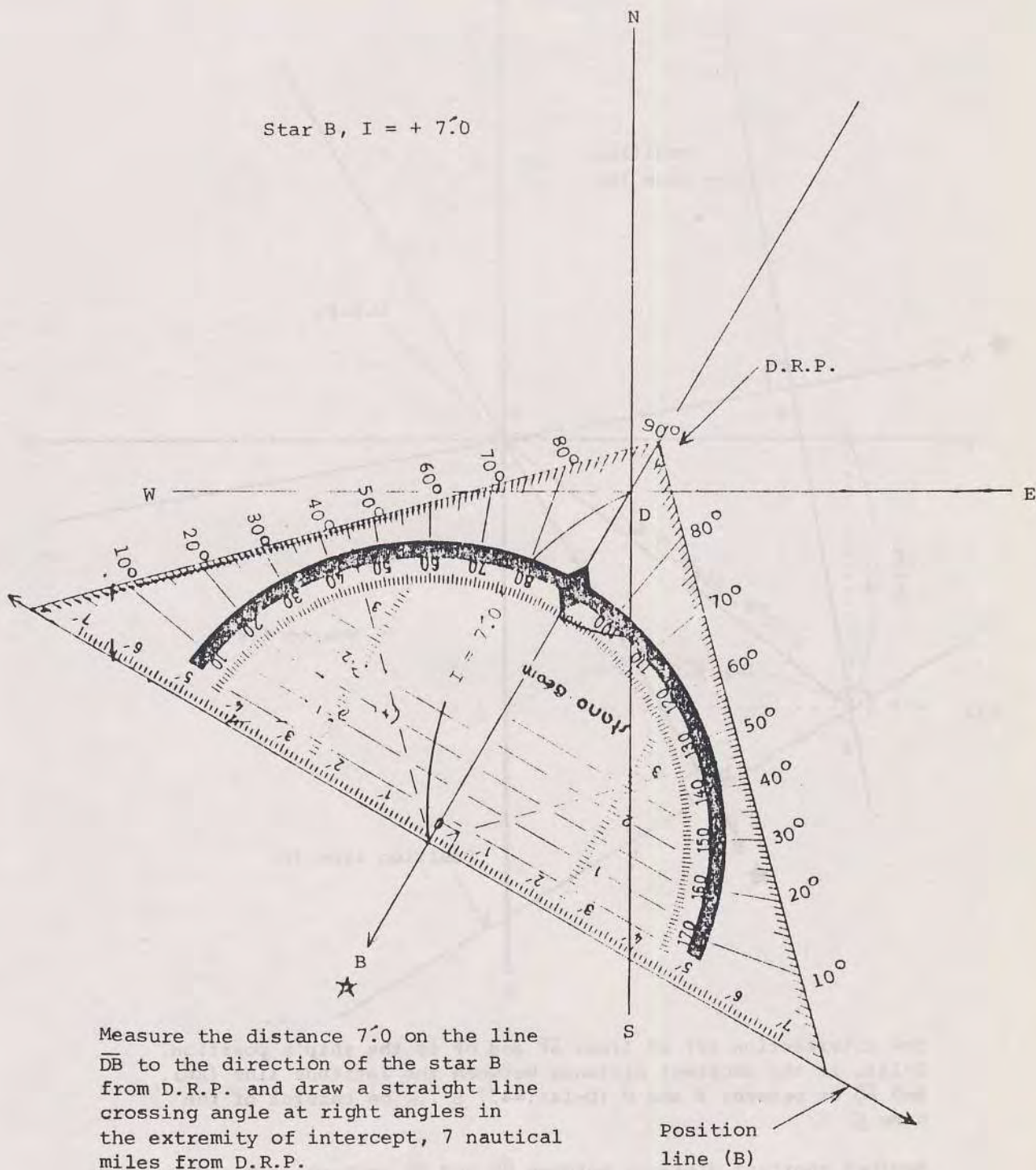
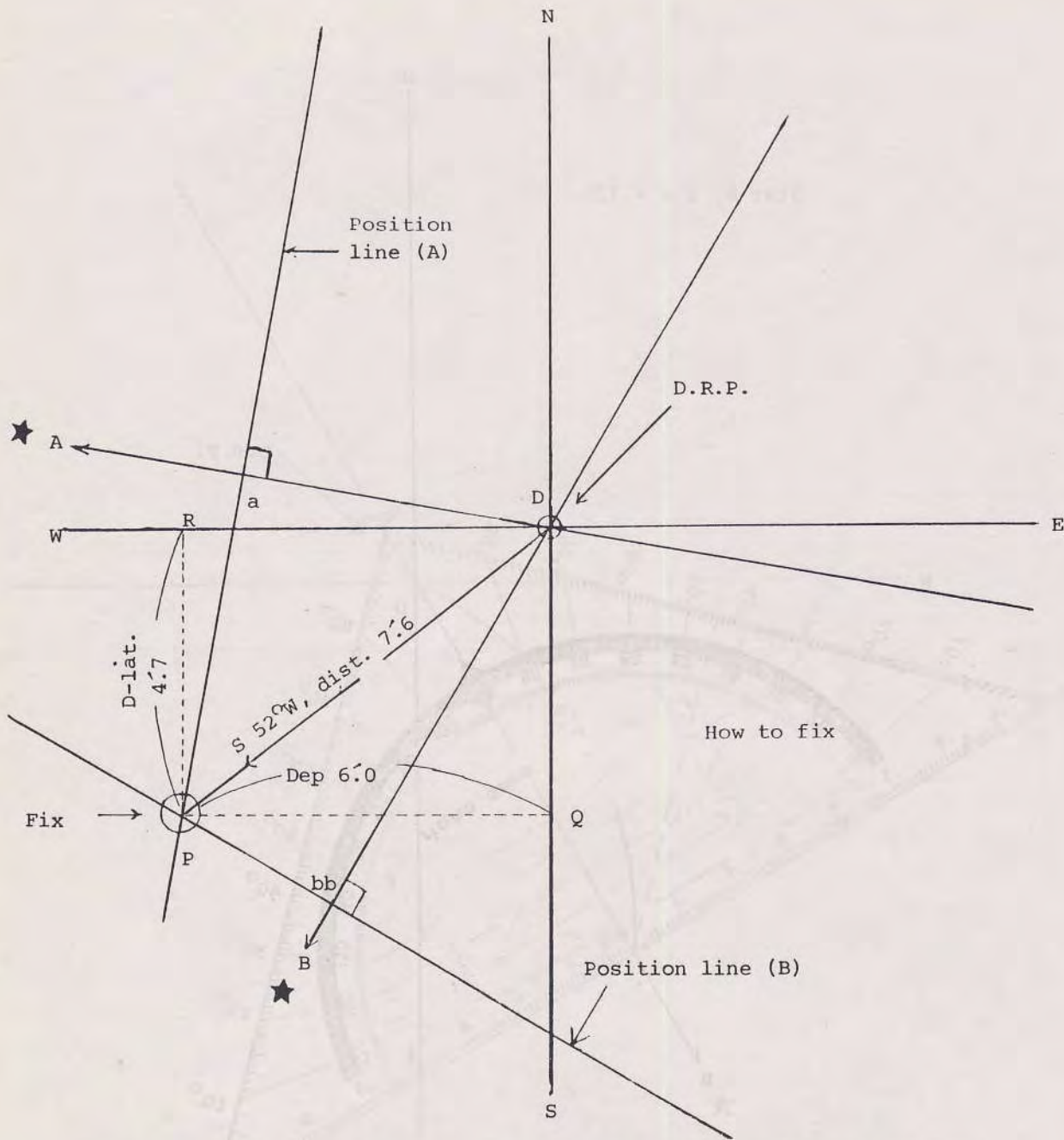


Fig. 95 How to draw line of position



The intersection (P) of lines \overline{aP} and \overline{bP} is the ship's position. D-lat. is the shortest distance between the latitude line (\overline{EW}) and \overline{PQ} or between R and P (D-lat.=4.7 S ... be careful of the name S)

Another shortest distance between \overline{NS} and \overline{RP} or between P and Q is Dep. (= 6.0 W ... be careful of the name W)

Fig. 96

- 4) Ship's position to be fixed (see Fig. 96)

The intersection (p) of line aP and bP is the ship's position.

- 5) Latitude and longitude (see Fig. 96)

To obtain both latitude and longitude of fix, it is necessary to measure D - Lat. It should be the shortest distance between the latitude line (\overline{EW}) and point P (or line \overline{PQ}). It is 4.7 nautical miles southerly (D - Lat. = 4.7 s = \overline{RP})

The value of departure (Dep.) should be the shortest distance between the longitude line (\overline{NS}) and point P (or line \overline{PR}). It is 6.0 nautical miles westerly (Dep. = 6.0 W = \overline{QP}).

By the mid-latitude sailing,

$$D - \text{long} = \frac{\text{Dep.}}{\cos \ell m} = \frac{6.0}{\cos 29^{\circ}57'65} = \frac{6.0}{0.866} = 6.9 \text{ W}$$

So, D.R.P. Lat. $30^{\circ}-00'0 \text{ N}$	D.R.P. long. $150^{\circ}-50'0 \text{ E}$
D - Lat. $\frac{4.7 \text{ S} \ominus}{29^{\circ}-55'3 \text{ N}}$	D - long. $\frac{6.9 \text{ W} \ominus}{150^{\circ}-43'1 \text{ E}}$

- 6) Current set and current drift (see Fig. 96)

Current set is \overline{DP} (= S 52°W, measured by a triangle ruler).

Current drift is the distance between point d and point P (= 7.6) measured by a triangle ruler).

- 7) Ans. Fixed position $29^{\circ}-55'3''$ N, $150^{\circ}-43'1''$ E
Current set S 52° W
Current drift $7'6''$ nautical miles

Note

It is convenient and advisable to use Solution B

Solution C ... by the position plotting sheet

Latitude scales are printed on this sheet (see Figs. 89 & 97), so you must mark longitudes depending on your D.R.P. (see Fig. 97).

1) Check your D.R.P. on the sheet and mark it with a small circle. next, draw azimuth line (\overrightarrow{OA}) of the star A through D.R.P. (point D) according to $Zc = N 80^{\circ}W$, then measure the distance 5.0 on this line to the direction of star A from D.R.P. according to $I = \oplus 5'0''$ and draw a line of position crossing angle at right angles on the extremity of intercept (point a) 5 nautical miles from D.R.P.

2) Draw the azimuth line (\overrightarrow{DB}) of the star B through D.R.P. (point D) according to $Zc = S 30^{\circ}W$, then measure the distance $7'0''$ on this line to the direction of the star B from D.R.P. according to $I = \oplus 5'0''$ and draw another line of position crossing angle at right angles on the extremity of intercept (point b), 7 nautical miles from D.R.P.

3) The intersection (point P) of both lines of position is the ship's fixed position. So the latitude and longitude of the fix can be directly obtained by divider measurement on the sheet.

4) Current set is the line \overrightarrow{DP} ($= S 52^{\circ}W$) and current drift is the distance between point D and P ($\hat{=} 7'6''$).

- 5) Ans. Fixed position $29^{\circ}-55'3''$ N, $150^{\circ}-43'1''$ E
Current set S 52° W
Current drift 7.6 nautical miles

Note This sheet is based on Mercator sailing

Solution D .. by plotting sheet for astronomical position

Longitude scales are printed on this sheet and latitude scales are also printed for every 10 nautical miles from latitude 0° to 60° (see Figs. 88, 98-100).

In this problem, the latitude is $30^{\circ} 00'$ north, so you must choose the scale of 30° latitude (see Figs. 98, 99 & 100), shown by a small circle as 30° , to measure distance and fixed latitude (or D - Lat.) on this sheet.

Scale of longitude is also shown on the sheet (see Figs. 98 & 101).

1) D.R.P. should be marked on the center of the sheet (see Fig. 101).

2) Draw the azimuth line \vec{DA} according to $Zc = N 80^{\circ}W$, and measure the distance 5.0 (see Figs. 99 & 101) on this line in the direction of the star A from D.R.P. according to $I = \oplus 5'0$, and draw a position line crossing angle at right angles on the extremity of intercept (point a), 5 nautical miles from D.R.P.

3) Draw the azimuth line \vec{DB} according to $Zc = S 30^{\circ}W$, and measure the distance 7.0 (see Figs. 100 & 101) on this line in the direction of the star B from D.R.P. according to $I = \oplus 7'0$ and draw another line of position crossing angle at right angles on the extremity of intercept (point b), 7 nautical miles from D.R.P.

4) The intersection (point P) of lines of position \vec{aP} and \vec{bP} , is the ship's position fixed.

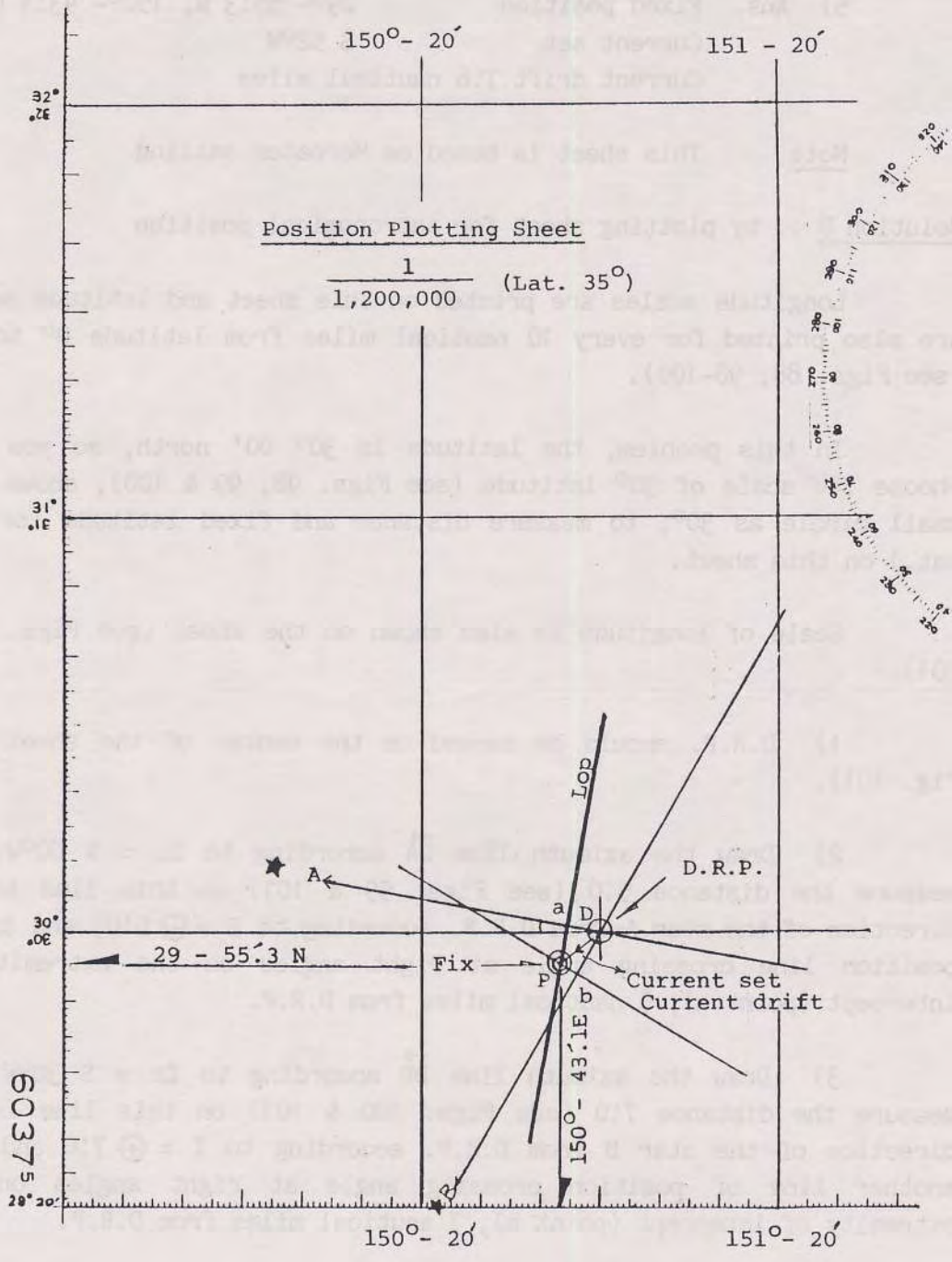


Fig. 97 How to fix

5) Latitude and longitude are obtained as follows;

1) To measure D - lat. on the sheet by dividers.

The shortest distance between latitude line ($\overline{EW} = 30^{\circ}-00'N$) and point P is D - Lat. (= 4!7 S ... Attention to the name S).

2) To measure D - Long. on the sheet by dividers.

The shortest distance between longitude line ($\overline{NS} = 150^{\circ}-50'E$) and point P is D - Long. (= 6!9 W ... Don't forget suffix W).

6) D.R.P. Lat. $30^{\circ}-00!0 N$	D.R.P. Long. $150^{\circ}-50!0 E$
D - Lat. $\frac{4!7 S \ominus}{29^{\circ}-55!3 N}$	D - Long. $\frac{6!9 W \ominus}{150^{\circ}-43!1 E}$

7) Current set is the line \overrightarrow{DP} (= S 52^oW) and current drift is the distance between D and P (= 7!6).

8) Ans. Fixed position $29^{\circ}-55!3 N$, $150^{\circ}-43!1 E$
Current set S 52^oW
Current drift 7!6 nautical miles

Note Plotting sheet for astronomical position is also based on Mercator sailing.



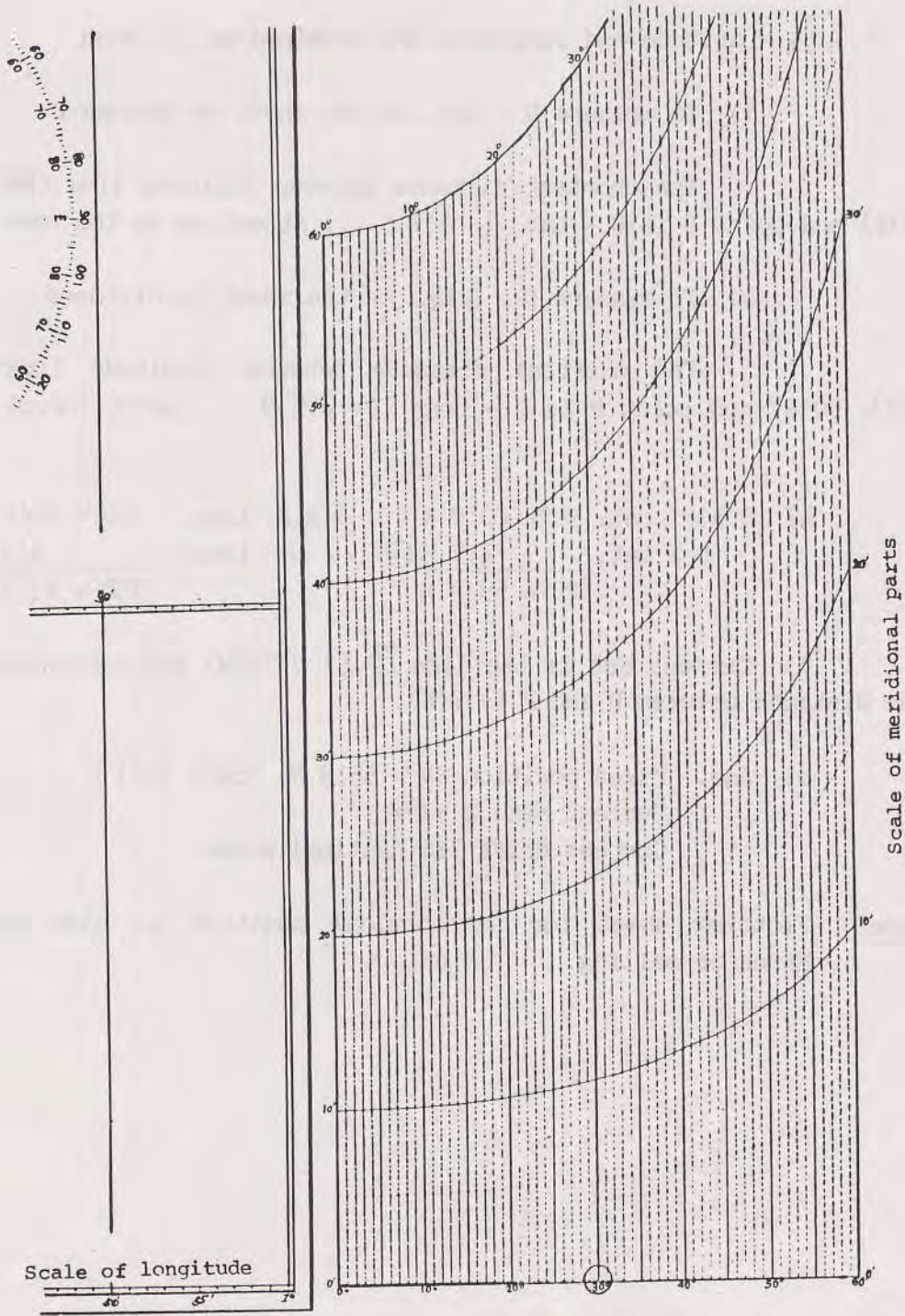


Fig. 98 Latitude

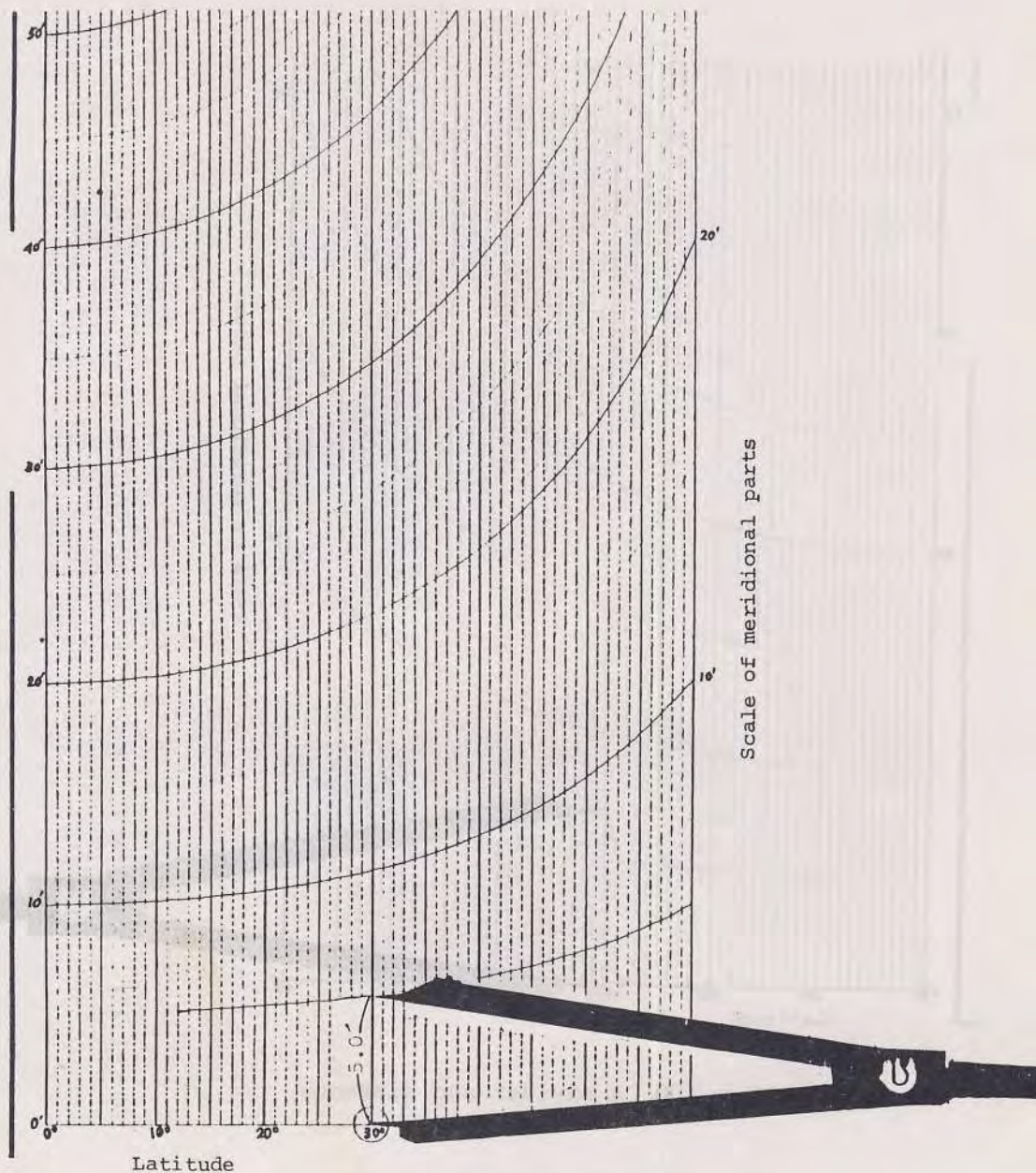


Fig. 99 A divider and distance

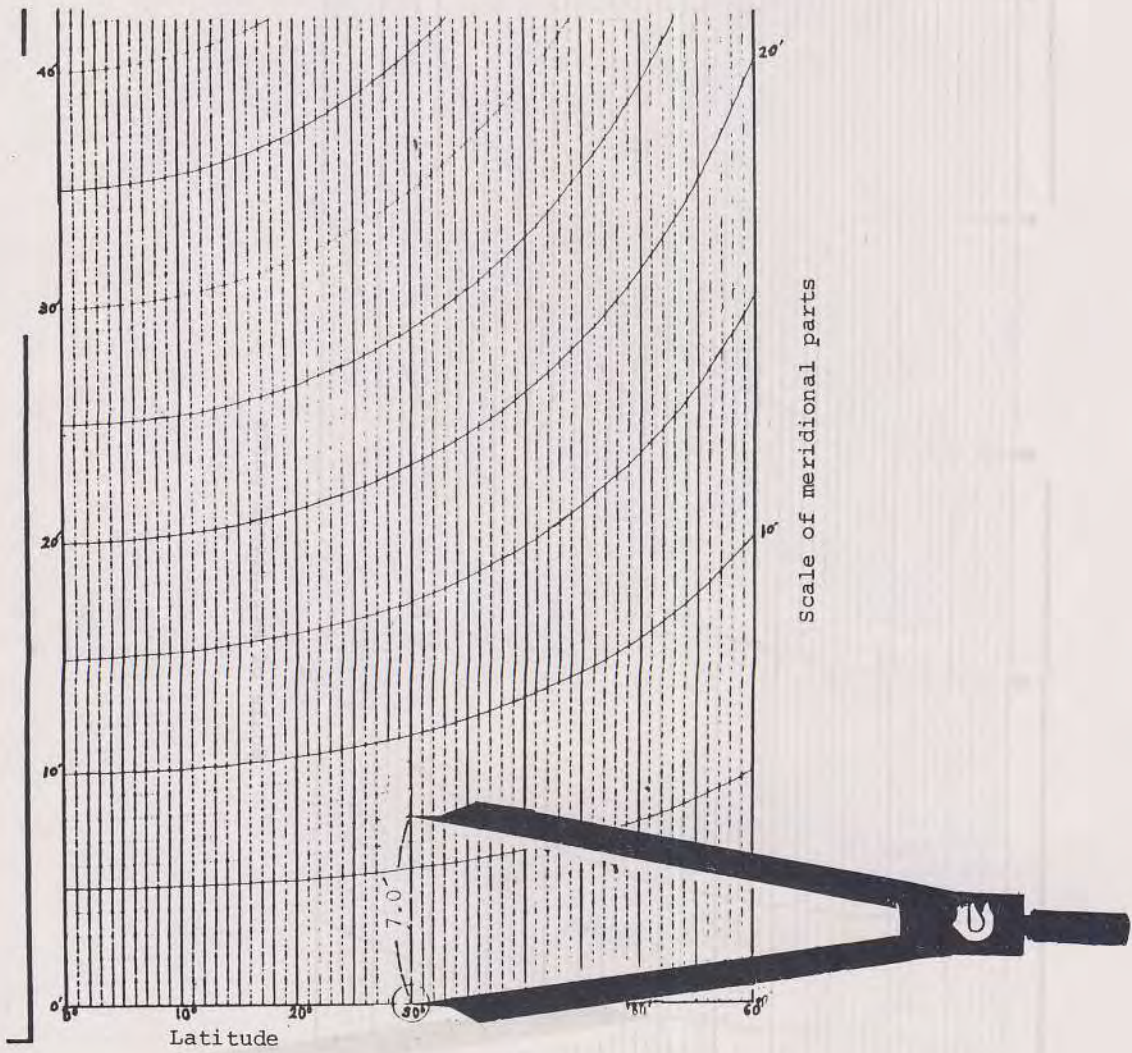


Fig. 100 A divider and distance

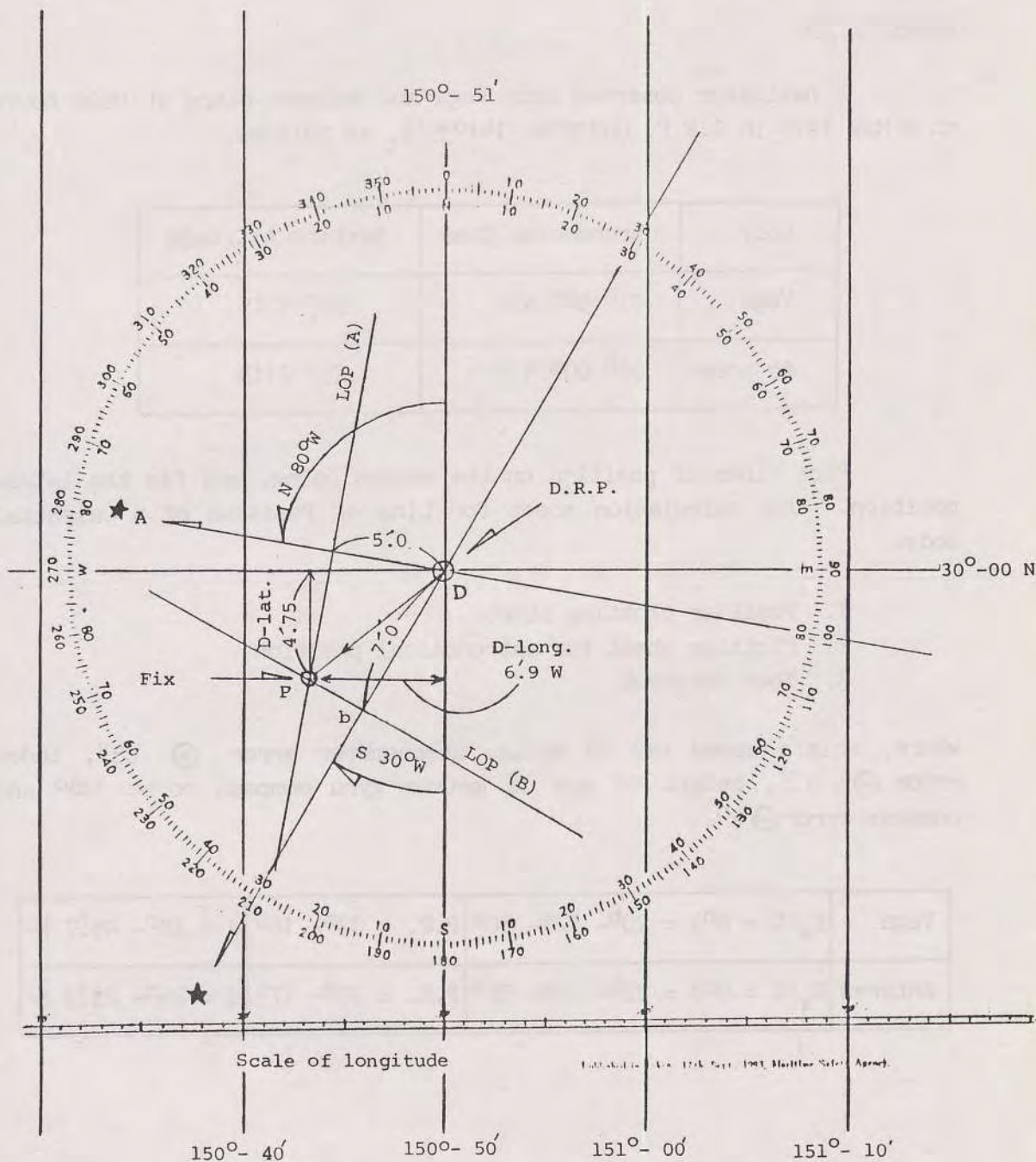


Fig. 101 How to fix

Example 15

A navigator observed both Vega and Antares stars at 0500 hours on 6 May 1979 in D.R.P. $06^{\circ}10'N$, $141^{\circ}35'E$, as follows,

Body	Chronometer Time	Sextant Altitude
Vega	07 ^h 54 ^m 57 ^s	50° 47'5
Antares	08 ^h 00 ^m 41 ^s	25° 21'3

Plot lines of position on the sheets below, and fix the latest position. Use calculation sheet for Line of Position of a Celestial Body.

1. Position plotting sheet
2. Plotting sheet for astronomical position
3. Your notebook

where, ship's speed was 20 knots, chronometer error $\oplus 05^s$, index error $\ominus 1'5$, height of eye 18 metres gyro compass course 128° and compass error $\oplus 2^{\circ}$.

Vega	$E_*(U = 0^h) = 20^h - 12^m - 50^s$	P.P. = 03 ^m 16 ^s	d = 38°- 45'7 N
Antares	$E_*(U = 0^h) = 22^h - 20^m - 56^s$	P.P. = 30 ^m 17 ^s	d = 26°- 23'1 S

Line of Position of a Celestial Body

Body's name		Date	Month	Year	Z. T.	\pm	h
						-	

D.R.P.	o /	N	o /	E	True Co.	o	sp'd	kt.
		S		W				

*1	Ship's Time	Date	Month	h	m	s	
	L. in T.						\pm
	Approx. U. (Date /)						
	Chro. T.			h	m	s	
	Chro. E.						\pm
	Corrected chro.T.						
	Morning or Afternoon (12)						+
	U. (Date /)						
	EOP (d = o / S)						
	P.P						+
				(24)			-
							⊙
	h_e in hours						
*2	h_e in degrees	$\oplus 360^\circ$					⊙
	Long.						\pm
		$\ominus 360^\circ$					⊙
	h						-

*3	h		→	A ₁		→	Z ₁	
	d	Z	→	A ₂		=	Z ₂	+
	l	Z	→	A ₃	+			
				A ₄				
				↓				
				A ₅				
	l ± d			A ₆	+			
				A ₇		→	Z ₃	-
				↓			Z ₄	
				ac	o /		↓	N o / E
						Z _c	S W	

Ref.

1. Approx. U = Ship's Time \pm L.in T. (E - long $\rightarrow \ominus$, W - long. $\rightarrow \oplus$)
2. $h = h_e \pm L$ (E - long $\rightarrow \oplus$, W - long $\rightarrow \ominus$)
3. When l and d same name $\rightarrow l-d$, contrary $\rightarrow l + d$
4. When $h > 180^\circ$ suffix of $Z_c \rightarrow E$, $h < 180^\circ$ suffix of $Z_c \rightarrow W$

Fig. 102 Calculation Sheet

Line of Position of a Celestial Body

Body's name	Vega.	Date	Month	Year	Z. T.	+	h
		6	May	1979	-	-	✓

D.R.P.	06° 10'	$\overset{N}{S}$	141° 35'	$\overset{E}{W}$	True Co.	130° sp'd	kt.
						20	

*1	Ship's Time	Date	Month	h	m	s		
		6	5	05	00	00		
	L. in T.				09	26	20	\oplus
	Approx. U. (Date 5/5)				19	33	40	
	Chro. T.				h	m	s	
					07	54	57	
	Chro. E.						05	\oplus
	Corrected chro.T.				07	55	02	
	Morning or Afternoon				(12)			\oplus
	U. (Date 5/5)				19	55	02	
	E \oplus *P (d = 38° 45.75')				20	12	50	
	P.P					03	16	+
					40	11	08	
				(24)			- \ominus	
h_g in hours				16	11	08		
h_g in degrees	$\oplus 360^\circ$			242°		47.0	\ominus	
Long.				141		35.0	\oplus	
	$\ominus 360^\circ$			384		22.0	\ominus	
							-	
h				24		22.0		

Sex. Alt.	50° 47'5"	
I.E.	01.5	\oplus
Obs. Alt	50 46.0	
Corr. 1	08.3	\oplus
	50 37.7	
Corr. 2	—	\pm
	—	
Corr. 3	—	\pm
	—	
at	50 37.7	
ac	50 39.7	-
I	02.0	\oplus

*2	h	24° 22'0"	\rightarrow	A ₁	135127		\rightarrow	Z ₁	38450	
	d	38 45.7	\rightarrow	A ₂	10804		=	Z ₂	10804	+
	l	06 10.0	\rightarrow	A ₃	252	+			49254	
				A ₄	146183					
				\downarrow						
				A ₅	3453					
				A ₆	7876	+				
*3	l±d			A ₇	11329		\rightarrow	Z ₃	19798	-
				\downarrow				Z ₄	29456	
				ac	50° 39'7"		\downarrow	Z _c	$\overset{N}{S}$ 30° 29'9" $\overset{E}{W}$	

Ref.

1. Approx. U = Ship's Time + L.in T. (E - long $\rightarrow \ominus$, W - long. $\rightarrow \oplus$)
2. h = h_g + L (E - long $\rightarrow \oplus$, W - long $\rightarrow \ominus$)
3. When l and d same name \rightarrow l-d, contrary \rightarrow l + d
4. When h > 180° suffix of Z_c \rightarrow E, h < 180° suffix of Z_c \rightarrow W

Fig. 103 Calculation Sheet

Line of Position of a Celestial Body

Body's name	Antares	Date	Month	Year	Z.T.	+	h
		6	May	1979	Z.T.	-	/

D.R.P.	06° 10' ^N _S	141° 35' ^E _W	True Co.	130°	sp'd	20	kt.
--------	-----------------------------------	------------------------------------	----------	------	------	----	-----

*1

Ship's Time	Date	Montl	h	m	s		Sex. Alt.	25° 21'3	
	6	5	05	00	00		I.E.	01.5	⊕
L. in T.			09	26	20	⊕	Obs. Alt	25 19.8	
Approx. U. (Date /)			19	33	40		Corr. 1	09.6	⊕
Chro. T.			h	m	s			25 10.2	
			08	00	41		Corr. 2	—	+
Chro. E.					05	⊕		—	+
Corrected chro.T.			08	00	46		Corr. 3	—	+
Morning or Afternoon			(12)			⊕		—	+
U. (Date 5/5)			20	00	46		at	25 10.2	
E ⊕ * P (d = 26° 23.1' ^N _S)			22	20	56		ac	25 14.6	-
P.P			03	17		+	I	04.4	⊕
			42	24	59				
			(24)			-			⊙
h _c in hours			18	24	59				
h _c in degrees	⊕360°		276°		14.8	⊙			
Long.			141		35.0	⊕			
	⊖360°		417		49.8	⊙			
h			57		49.8				

*2

h	57° 49'8	→	A ₁	63119		→	Z ₁	7239	
d	26 23.1	⊖	A ₂	4778		=	Z ₂	4778	+
l	06 10.0	⊖	A ₃	252	+			12017	
			A ₄	68149					
			↓						
			A ₅	20822					
l ± d			A ₆	7855	+				
			A ₇	28677		→	Z ₃		-
			↓				Z ₄		
			ac	25° 14'6		↓	Z _c	^N _S 56° 57'9 ^E _W	*4

Ref.

1. Approx. U = Ship's Time + L.in T. (E - long + ⊖, W - long. + ⊕)
2. h = h_c + L (E - long + ⊕, W - long + ⊖)
3. When l and d same name + l~d, contrary + l + d
4. When h > 180° suffix of Z_c + E, h < 180° suffix of Z_c + W

Fig. 104 Calculation Sheet

2) Running fix calculation

o Gyro Compass Course 128°
 Compass error $2^\circ +$
 True Course 130°

o Time lag between first and second observation
 First observation chro. T. = $07^h - 54^m - 57^s$
 Second observation chro. T. = $08 - 00 - 41 -$
 $05 - 44 = 5^m.7$

o Distance run = $\frac{20^m \times 5.7}{60^m} = 1.9$

20 miles \rightarrow 60 minutes
 1.9 miles \leftarrow 5.7 minutes

Date	Time	Lat	Long	Course	Distance
07	07:54:57	35	10	130	20
08	08:00:41	35	10	130	1.9

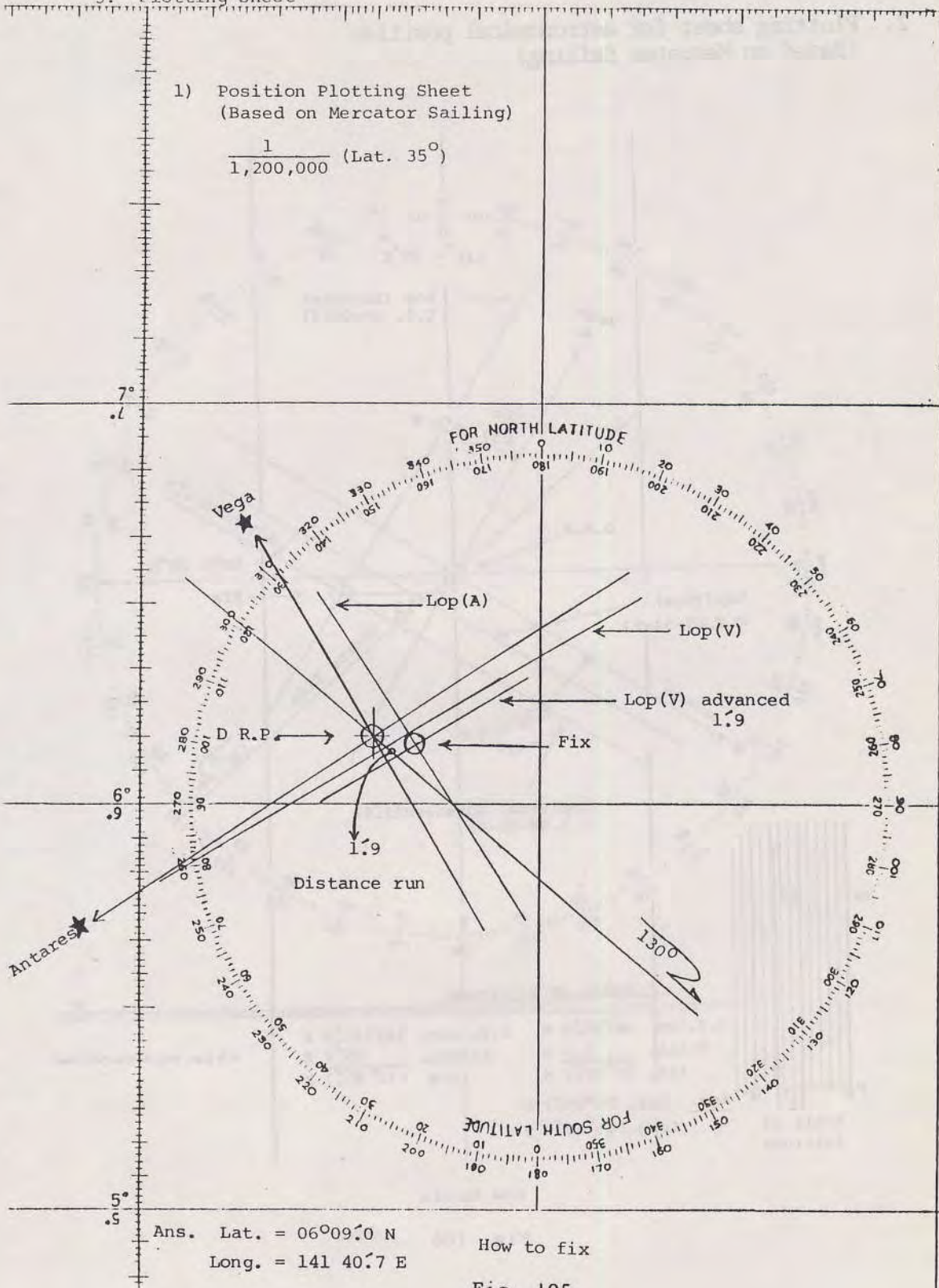
Lat	Long
35	10
35	10

Lat	Long
35	10
35	10

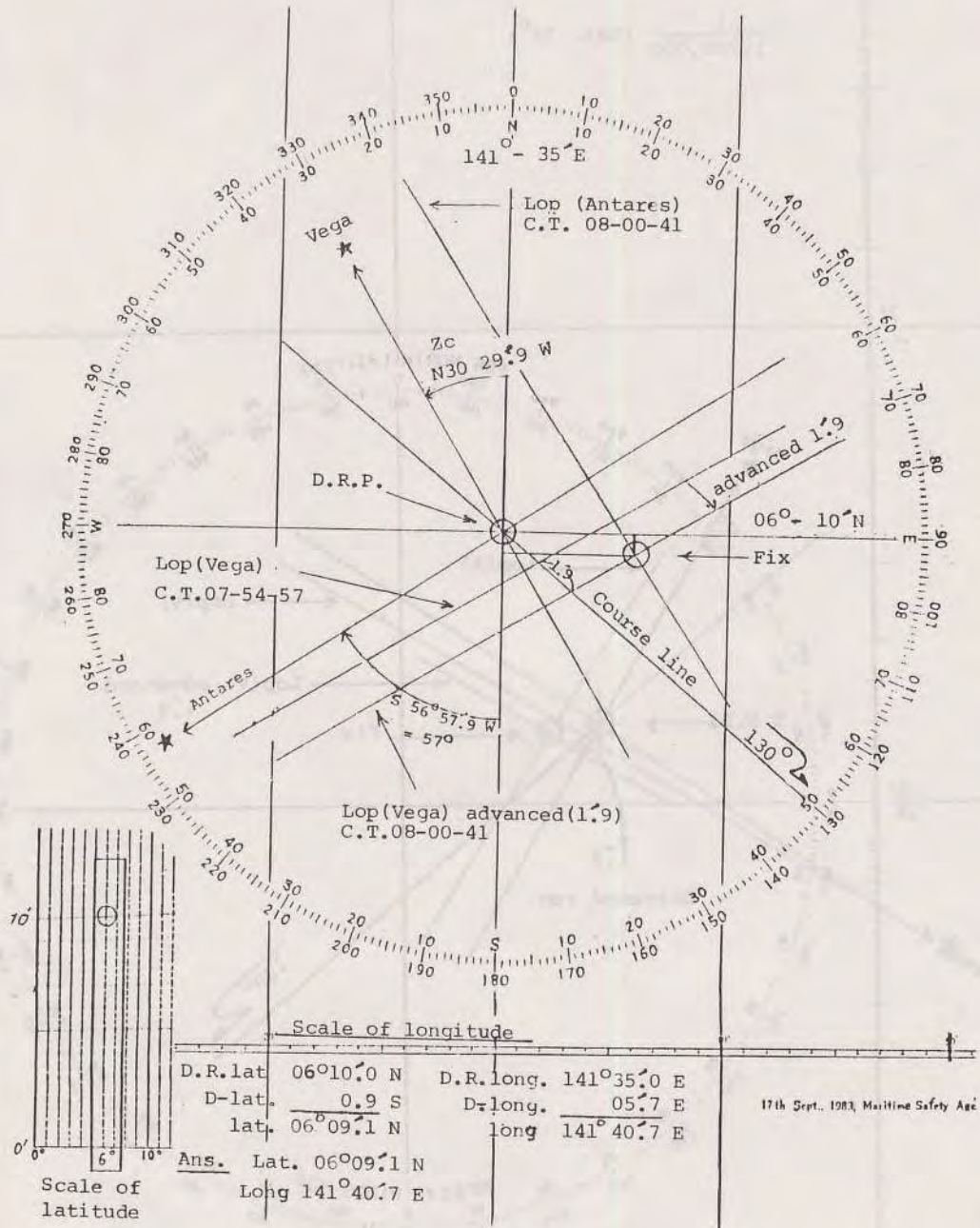
3. Plotting sheet

1) Position Plotting Sheet
(Based on Mercator Sailing)

$$\frac{1}{1,200,000} \text{ (Lat. } 35^\circ\text{)}$$



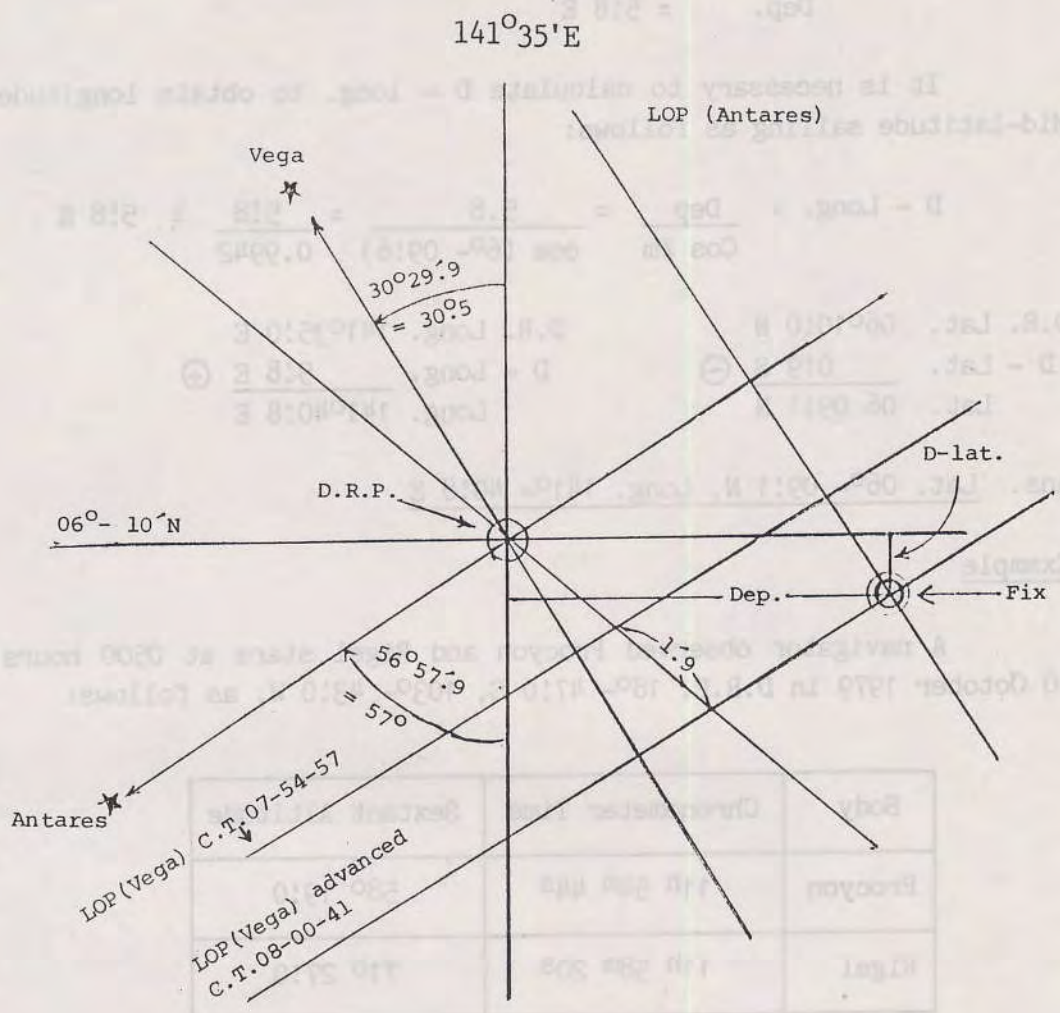
2. Plotting sheet for astronomical position
(Based on Mercator Sailing)



How to fix

Fig. 106

3. On note book (Based on Mid-latitude sailing)



By triangle ruler (This sheet is not based on Mercator Sailing)

$$\rightarrow D\text{-long.} = \frac{\text{Dep.}}{\text{Cos. } \lambda_m}$$

How to fix

Fig. 107

1	2	3	4
5	6	7	8

$$\begin{aligned} D - \text{Lat.} &= 0:9 \text{ S} \\ \text{Dep.} &= 5:8 \text{ E} \end{aligned}$$

It is necessary to calculate D - long. to obtain longitude by Mid-latitude sailing as follows:

$$D - \text{Long.} = \frac{\text{Dep}}{\cos \ell m} = \frac{5.8}{\cos (6^{\circ} - 09:6)} = \frac{5:8}{0.9942} \approx 5:8 \text{ E}$$

$$\begin{array}{ll} \text{D.R. Lat. } 06^{\circ}10:0 \text{ N} & \text{D.R. Long. } 141^{\circ}35:0 \text{ E} \\ D - \text{Lat. } \underline{0:9 \text{ S}} \ominus & D - \text{Long. } \underline{5:8 \text{ E}} \oplus \\ \text{Lat. } 06^{\circ}09:1 \text{ N} & \text{Long. } 141^{\circ}40:8 \text{ E} \end{array}$$

Ans. Lat. $06^{\circ} - 09:1 \text{ N}$, Long. $141^{\circ} - 40:8 \text{ E}$

Example

A navigator observed Procyon and Rigel stars at 0500 hours on 10 October 1979 in D.R.P. $18^{\circ} - 47:0 \text{ S}$, $103^{\circ} - 43:0 \text{ W}$, as follows:

Body	Chronometer Time	Sextant Altitude
Procyon	11 ^h 54 ^m 44 ^s	58° 19:0
Rigel	11 ^h 58 ^m 20 ^s	71° 27:0

Plot lines of position, fix the latest position in your note book and show the current set and current drift.

where; Ship's speed was 22 knots, true course 297° , chronometer error $\oplus 4^{\text{s}}$, index error $\ominus 1.5$, height of eye 21 metres.

Procyon	$E_*(U = 0^{\text{h}}) = 17^{\text{h}} 33^{\text{m}} 47^{\text{s}}$	P.P. = 1 ^m 57 ^s .5	d = $5^{\circ}16:6 \text{ N}$
Rigel	$E_*(U = 0^{\text{h}}) = 19^{\text{h}} 58^{\text{m}} 27^{\text{s}}$	P.P. = 1 ^m 58 ^s	d = $8^{\circ}13:4 \text{ S}$

Solution 1) Calculation for lines of position

Line of Position of a Celestial Body

Body's name	Procyon	Date	Month	Year	Z.T.	+	h
		10	Oct.	1979	-	-	✓

D.R.P.	18° 47' $\text{\textcircled{S}}$	130° 43' $\text{\textcircled{W}}$	True Co.	297°	sp'd	kt.
						22

*1

Ship's Time	Date	Month	h	m	s	
	10	10	05	00	00	
L. in T.			06	54	52	$\text{\textcircled{+}}$
Approx. U. (Date 10/10)			11	54	52	
Chro. T.			h	m	s	
			11	54	44	
Chro. E.					4	$\text{\textcircled{-}}$
Corrected chro. T.			11	54	48	
Morning or Afternoon			(12)			+
U. (Date 10/10)			11	54	48	
$E \text{\textcircled{+}} * (P (d = 5^{\circ} 16' 6''))$			17	33	47	
P.P				1	57.5	+
				29	30	32.5
			(24)			- $\text{\textcircled{O}}$
h_a in hours			05	30	32.5	
h_a in degrees	$\text{\textcircled{+}}360^{\circ}$		82°		38.1	$\text{\textcircled{O}}$
Long.			103		43.0	$\text{\textcircled{O}}$
	$\text{\textcircled{-}}360^{\circ}$					$\text{\textcircled{O}}$
						-
h			338		55.1	

*2

h	338° 55.1	→	A_1	147540	→	Z_1	44406	
d	5 16.6 $\text{\textcircled{S}}$	→	A_2	185	=	Z_2	185	+
ℓ	18 47.0 $\text{\textcircled{S}}$	→	A_3	2377	+		44591	
			A_4	150102				
			↓					
			A_5	3155				
ℓ & d	24° 03' 6"		A_6	4344	+			
			A_7	7499		→	Z_3	27841
			↓				Z_4	16750
			a_c	58° 12' 9"		↓	Z_c	S 42° 50' 6" W $\text{\textcircled{N}} \text{\textcircled{E}}$

*3

*4

Ref.

1. Approx. U = Ship's Time + L.in T. (E - long $\text{\textcircled{-}}$, W - long. $\text{\textcircled{+}}$)
2. $h = h_c + L$ (E - long $\text{\textcircled{+}}$, W - long $\text{\textcircled{-}}$)
3. When ℓ and d same name $\rightarrow \ell - d$, contrary $\rightarrow \ell + d$
4. When $h > 180^{\circ}$ suffix of $Z_c \rightarrow E$, $h < 180^{\circ}$ suffix of $Z_c \rightarrow W$

Fig. 108 Calculation Sheet

Line of Position of a Celestial Body

Body's name	Rigel	Day	Month	Year	% T.	l	h
		10	Oct.	1979		-	/

D.R.P.	18° 47'	N	130° 43'	E	True Co.	297°	sp'd	kt.
		(S)		(W)				22.0

* 1	Ship's Time	Date	Month	h	m	s	
		10	10				
	L. in T.						+
	Approx. U. (Date 10/10)						
	Chro. T.			h	m	s	
				11	58	20	
	Chro. E.					4	(+)
	Corrected chro. T.			11	58	24	
	Morning or Afternoon			(12)			+
	U. (Date 10/10)			11	58	24	
E(+) * P (d = 8° 13.4' N)			19	58	27		
P.P				1	58	+	
			31	58	49		
			(24)			-	
h _a in hours			07	58	49		
h _a in degrees	(+)	360°	119°	42.3		(+)	
Long.			103	43.0		(+)	
	(-)	360°	15	59.3		(+)	
h			15	59.3			

Sex. Alt.	71	27.0	
I.E.		1.5	(+)
Obs. Alt	71	25.5	
Corr. 1		8.5	(+)
	71	17.0	
Corr. 2		/	(+)
		/	(+)
Corr. 3		/	(+)
a _t	71	17.0	
a _c	71	13.6	-
I		3.4	(+)

* 3	h	15° 59.3	→	A ₁	171352		→	Z ₁	55997		
	d	8 13.4	(N)	→	A ₂	449		=	Z ₂	449	+
	l	18 47.0	(S)	→	A ₃	2377	+			56446	
					A ₄	174178					
					↓						
					A ₅	1813					
	l ± d				A ₆	846.8	+				
					A ₇	2659.8		→	Z ₃	49238	-
					↓				Z ₄	7208	
					a _c	71° 13.6			l	(N)	
								Z _c	S 57° 53.6	(E) (W)	

Ref.

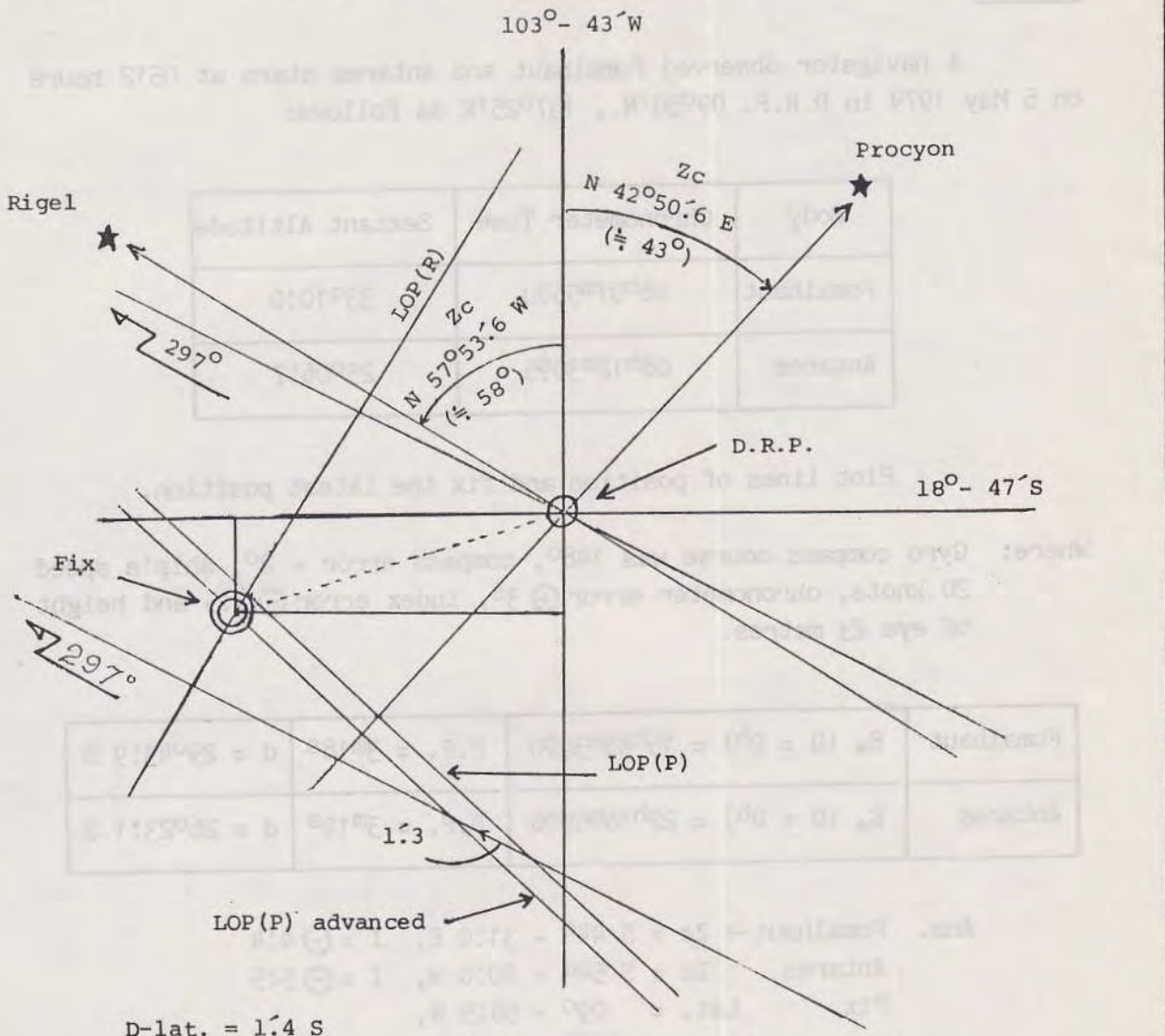
1. Approx. U = Ship's Time + L.in T. (E - long + (-), W - long. + (+))
2. h = h_G + L (E - long + (+), W - long + (-))
3. When l and d same name → l-d, contrary → l + d
4. When h > 180° suffix of Z_c → E, h < 180° suffix of Z_c → W

Fig. 109 Calculation Sheet

2) Running fix calculation

$$\text{Distance run} = \frac{22' \times 3^m.6}{60^m} = 1.32$$

3) Plotting sheet (note book)



D-lat. = 1.4 S

Dep. = 4.9 W → D-long. = $\frac{\text{Dep}}{\cos l} = \frac{4.9}{\cos(18^\circ 47')} = \frac{4.9}{0.94674} = 5.2 \text{ W}$

D.R. lat. 18°-47.0 S D.R. long. 103°-43.0 W

D-lat. 1.4 S + D-long. 5.2 W +

Lat. 18° 48.4 S Long. 103° 48.2 W

Ans. Lat 18°-48.4 S, Long. 103°-48.2 W

Current set = S 73°5 W, Current drift = 5.1

How to fix

Fig. 110

Problem

A navigator observed Fomalhaut and Antares stars at 0512 hours on 5 May 1979 in D.R.P. $09^{\circ}50'N.$, $137^{\circ}25'E$ as follows:

Body	Chronometer Time	Sextant Altitude
Fomalhaut	08 ^h 07 ^m 56 ^s .0	33°10!0
Antares	08 ^h 12 ^m 30 ^s .5	25°06!7

Plot lines of position and fix the latest position,

Where: Gyro compass course was 148° , compass error $+ 2^{\circ}$, ship's speed 20 knots, chronometer error $\oplus 3^s$, index error $\ominus 2!5$ and height of eye 23 metres.

Fomalhaut	$E_{*} (U = 0^h) = 15^h48^m39^s.0$	P.P. = 3 ^m 18 ^s	d = 29°43!9 S
Antares	$E_{*} (U = 0^h) = 22^h16^m59^s.0$	P.P. = 3 ^m 19 ^s	d = 26°23!1 S

Ans. Fomalhaut $\rightarrow Zc = S 44^{\circ} - 31!0 E$, $I = \ominus 4!4$

Antares $Zc = S 54^{\circ} - 40!0 W$, $I = \ominus 5!5$

Fix Lat. = $09^{\circ} - 56!5 N$,

Long. = $137^{\circ} - 27!2 E$

A navigator observed Rigel and Aldebaran stars at 0530 hours on 14 July 1979 in D.R.P. $12^{\circ} - 25!0 S.$, $163^{\circ} - 09!0 E$ as follows:

Body	Chronometer Time	Sextant Altitude
Rigel	6 ^h 54 ^m 51 ^s .0	30°44!8
Aldebaran	6 ^h 59 ^m 25 ^s .5	33°19!8

Plot lines of position and fix the latest position.

Where; Gyro compass course was 345° , compass error nil, ship's speed 18 knots, chronometer error $\oplus 3^s$, index error $\oplus 1'0$ and height of eye 20 metres.

Rigel	$E_* (U = 0^h) = 14^h07^m36^s0$	P.P. = 3^m06^s5	$d = 8^{\circ}13'5'' S$
Aldebaran	$E_* (U = 0^h) = 14^h46^m24^s0$	P.P. = 3^m07^s5	$d = 16^{\circ}28'0'' N$

Ans. Rigel $\rightarrow Zc = S 87^{\circ}42' E, I = + 6'4$
 Aldebaran $\rightarrow Zc = N 60^{\circ}40' E, I = + 5'7$
 Fix Lat. = $12^{\circ}24'0'' S$
 Long. = $163^{\circ}15'2'' E$

A navigator observed Procyon and Aldebaran stars at 1935 hours on 25 February 1979 in D.R.P. $39^{\circ}54'0'' S., 79^{\circ}55'0'' E$ as follows;

Body	Chronometer Time	Sextant Altitude
Procyon	$02^h21^m45^s$	$39^{\circ}34'0''$
Aldebaran	$02^h25^m15^s$	$29^{\circ}55'0''$

Plot lines of position and fix the latest position

Where; Gyro compass course was 159° , compass error nil, ship's speed 21 knots, chronometer error $\ominus 2^s0$, index error $\oplus 2'0$ and height of eye 20 metres.

Procyon	$E_* (U = 0^h) = 02^h38^m49^s$	P.P. = 2^m21^s0	$d = 5^{\circ}16'5'' N$
Aldebaran	$E_* (U = 0^h) = 05^h42^m20^s$	P.P. = 2^m22^s0	$d = 16^{\circ}27'9'' N$

Ans. Procyon → Zc = N 32°12'0 E, I = ⊖ 6'8
 Aldebaran → Zc = N 24°56'0 W, I = ⊖ 6'4
 Fix Lat. = 39°46'1 N,
 Long. = 79°52'8 E,

A navigator observed Bega and Antares stars at 18.50 hours on 10 August in E.R.R. 05°04'0 N., 75°13'0 E as follows:

Body	Chronometer Time	Sextant Altitude
Vega	01h46m59s	41°44'0
Antares	01h50m11s	58°08'0

Plot lines of position and fix the latest position.

Where: True course was 230°, ship's speed 18 knots, chronometer error ⊕ 3s, index error ⊖ 1.5 and height of eye 18 metres.

Vega	E* (U = 0h) = 02h-35m-15s	P.P. = 2m-15s	d = 38°-46'2 N
Antares	E* (U = 0h) = 04 -43- 21	P.P. = 2 - 16	d = 26°-23'2 S

Ans. Vega → Zc = N 40°-31'0 E, I = ⊕ 7'3
 Antares → Zc = S 09°-53'0 E, I = ⊖ 4'2
 Fix Lat. = 05°-09'0 N,
 Long. = 75°-17'0 E

A navigator observed Denebola and Procyon at 19.20 hours on 24 April 1979 in D.R.P. $34^{\circ}42'0''$ N., $134^{\circ}27'0''$ W as follows:

Body	Chronometer Time	Sextant Altitude
Denebola	$04^{\text{h}}20^{\text{m}}07^{\text{s}}$	$53^{\circ}38'0''$
Procyon	$04^{\text{h}}23^{\text{m}}39^{\text{s}}$	$50^{\circ}04'5''$

Plot lines of position and fix the latest position

Where; True course was 305° , ship's speed 20 knots, chronometer error $\ominus 3^{\text{s}}$, index error $\oplus 1.5$ and height of eye 20 metres.

Denebola	$E_{*} (U = 0^{\text{h}}) = 02^{\text{h}}21^{\text{m}}39^{\text{s}}$	P.P. = $0^{\text{m}}43^{\text{s}}$	d = $14^{\circ}41'2''$ N
Procyon	$E_{*} (U = 0^{\text{h}}) = 06^{\text{h}}31^{\text{m}}27^{\text{s}}$	P.P. = $0^{\text{m}}43^{\text{s}}$	d = $05^{\circ}16'5''$ N

Ans. Denebola $Z_c = S 65^{\circ}2' E, I = \ominus 5'2''$

Procyon $Z_c = S 49^{\circ}6' W, I = \oplus 3'2''$

Fix Lat. = $34^{\circ} - 43'9''$ N

Long. = $134^{\circ} - 34'1''$ E

Example 17

On 10 September 1953, a navigator observed the altitude of the sun's lower limb at 2300Z at ship's time 0730 hours. Chronometer time 195300.0, D.R.P. $15^{\circ}24'8''$ N and he noted 30 nautical miles to 180W from this D.R.P., and observed the altitude of the sun's lower limb again at 0758 at ship's time 1100, chronometer time 020000.0.

A navigation observed Procyon and Rigel stars of 0530 hours on 10 October 1979 in D.R.P. $18^{\circ}47'0''$ S, $103^{\circ}43'0''$ W as follows:

Body	Chronometer Time	Sextant Altitude
Procyon	11h54m14s	$58^{\circ}19'0''$
Rigel	11h58m20s	$71^{\circ}27'0''$

Plot lines of position and fix the latest position

Where: True course was 297° , ship's speed 22 knots, Chronometer error $\oplus 4^{\circ}0'$, index error $\ominus 1'5''$ and height of eye 21 metres.

Procyon	$E_* (U = 0h) = 17^{\text{h}}33^{\text{m}}47^{\text{s}}$	P.P. = $1^{\text{m}}57^{\text{s}}5$	d = $05^{\circ}16'6''$ N
Rigel	$E_* (U = 0h) = 19^{\text{h}}58^{\text{m}}27^{\text{s}}$	P.P. = $1^{\text{m}}58^{\text{s}}$	d = $08^{\circ}13'4''$ S

Ans. Procyon \rightarrow Zc = N $42^{\circ}50'5''$ E, I = $\ominus 4'0''$
 Rigel \rightarrow Zc = N $57^{\circ}54'6''$ W, I = $\oplus 3'1''$
 Lat. = $18^{\circ}48'5''$ S
 Long. = $103^{\circ}48'0''$ W

Example 17

On 10 September 1963, a navigator observed the altitude of the sun's lower limb as $23^{\circ}02'0''$ at ship's time 0730 hours, chronometer time $10^{\text{h}}31^{\text{m}}24^{\text{s}}$ in D.R.P. $19^{\circ}56'N$, $128^{\circ}24'E$ and he sailed 30 nautical miles to S $18^{\circ}W$ from this D.R.P., and observed the altitude of the sun's lower limb again as $69^{\circ}58'$ at ship's time 1100, chronometer time $02^{\text{h}}04^{\text{m}}02^{\text{s}}$.

Line of Position of a Celestial Body

Plot the position at ship's time 1100 on the PLOTTING SHEET for ASTRONOMICAL POSITION.

Where: Chronometer error was + 23^m10^s, local variation 4^oW, deviation 4^oW, index error + 1.0, height of eye 16 metres.

1) $E \odot = 12^h 02^m 39^s$ (at $U = 22^h 54^m 34^s$, Sept. 9th)
 d for $U = 22^h = 05^{\circ} 20' 0''$ N
 P.P. of d for $54^m 34^s = 0.9 \ominus$

2) $E \odot = 12^h 02^m 41^s$ (at $U = 02^h 27^m 12^s$, Sept, 10th)
 d for $U = 02^h = 05^{\circ} 16' 2''$ N
 P.P. of d for $27^m 12^s = 0.4 \ominus$

Solution

- To obtain true course
 Comp. Co. S 180^oW
 Deviation 4^oW \ominus
 Mag. Co S 14^oW
 Variation 4^oW \ominus
 True Co. S 10^oW

- To calculate at, ac and Zc of 1st observation (see Fig. 111)

Body	Time	Observed Altitude	Corrected Altitude	Distance	Local Hour Angle	Local Sidereal Time	Right Ascension	Declination	Greenwich Hour Angle	Greenwich Sidereal Time
\odot	1100	30.0	30.9	10.0	100.0	100.0	100.0	10.0	100.0	100.0
\odot	1100	30.0	30.9	10.0	100.0	100.0	100.0	10.0	100.0	100.0

1. Approx. $U = \text{Ship's Time} + L \text{ in T. } (E - \text{long} + \ominus, W - \text{long} + \oplus)$
 2. $h = h_0 + L \text{ in } - \text{long} + \oplus, W - \text{long} + \ominus$
 3. When L and S same name + $L - D$, contrary - $L + D$
 4. When $h > 180^{\circ}$ either of $S + E, h < 180^{\circ}$ either of $S - W$

Line of Position of a Celestial Body

Body's name	Sun	\odot	Day	Month	Year	Z. T.	+	h
			10	Sept.	1963		-	/

1st. D.R.P.	$19^{\circ} 56'$	N S	$128^{\circ} 24'$	E W	True Co. Comp.	S 18 W	sp'd	$30/3.5$ kt.
-------------	------------------	-----------------	-------------------	-----------------	-------------------	--------	------	--------------

* 1	Ship's Time	Date	Month	h	m	s	
		10	9	07	30	00	
	L. in T.			08	33	36	\oplus
	Approx. U. (Date 9/9)			22	56	24	
	Chro. T.			h	m	s	
				10	31	24	
	Chro. E.			23	10		\oplus
	Corrected chro. T.			10	54	34	
	Morning or Afternoon			(12)			\oplus
	U. (Date 9/9)			22	54	34	
	E \odot *P (d = $^{\circ}$ N S)			12	02	39	
	P.P						+
			34	57	13		
			(24)			\ominus \odot	
h_G in hours			10	57	13		
h_G in degrees	$\oplus 360^{\circ}$		164°		18.3	\odot	
Long.			128		24.0	\oplus	
	$\ominus 360^{\circ}$		—		—	\odot	
			—		—	-	
h			292		42.3		

Sex. Alt.	$23^{\circ} 02.0$	
I.E.	01.0	\oplus
Obs. Alt	$23^{\circ} 03.0$	
Corr. 1	6.5	\oplus
	$23^{\circ} 09.5$	
Corr. 2	0.2	\oplus
	$23^{\circ} 09.7$	
Corr. 3	—	\oplus
a _t	$23^{\circ} 09.7$	
a _c	$23^{\circ} 08.2$	-
I	01.5	\oplus

* 2	h	$292^{\circ} 42.3$	\rightarrow	A ₁	51286		\rightarrow	Z ₁	3504		
	d	$05^{\circ} 19.1$	\rightarrow	A ₂	187		=	Z ₂	187	\oplus	
	l	$19^{\circ} 56.0$	\rightarrow	A ₃	2683	+			3691		
				A ₄	54156						
				A ₅	28736						
	* 3	l+d	$14^{\circ} 36.9$		A ₆	1618	+		Z ₃	3641	-
					A ₇	30354		\rightarrow	Z ₄	50	
				a _c	$23^{\circ} 08.2$			Z _c	$\text{N } 87^{\circ} 15' \text{ W}$	\oplus	

Ref.

1. Approx. U = Ship's Time + L.in T. (E - long + \ominus , W - long. + \oplus)
2. h = h_G + L (E - long + \oplus , W - long + \ominus)
3. When l and d same name \rightarrow l-d, contrary \rightarrow l + d
4. When h > 180° suffix of Z_c + E, h < 180° suffix of Z_c + W

Fig. 111

- 3 To obtain 2nd D.R.P. for second observation

2nd D.R.P. is the point which is 30 nautical miles away and direction is S 10°W from the extremity of intercept of the first observation (see Fig. 112).

By plotting course line S 10°W and distance 30 nautical miles from the extremity of intercept of the first observation, 2nd D.R.P. is 19°26'.4 N, 128°20'.1 E on the plotting sheet (see Fig. 112).

- 4 To calculate at ac and Zc of 2nd observation (see Fig. 114).

- 5 Plotting LOP and fix (see Fig. 112).



Fig. 112 How to fix

Plotting Sheet for Astronomical Position

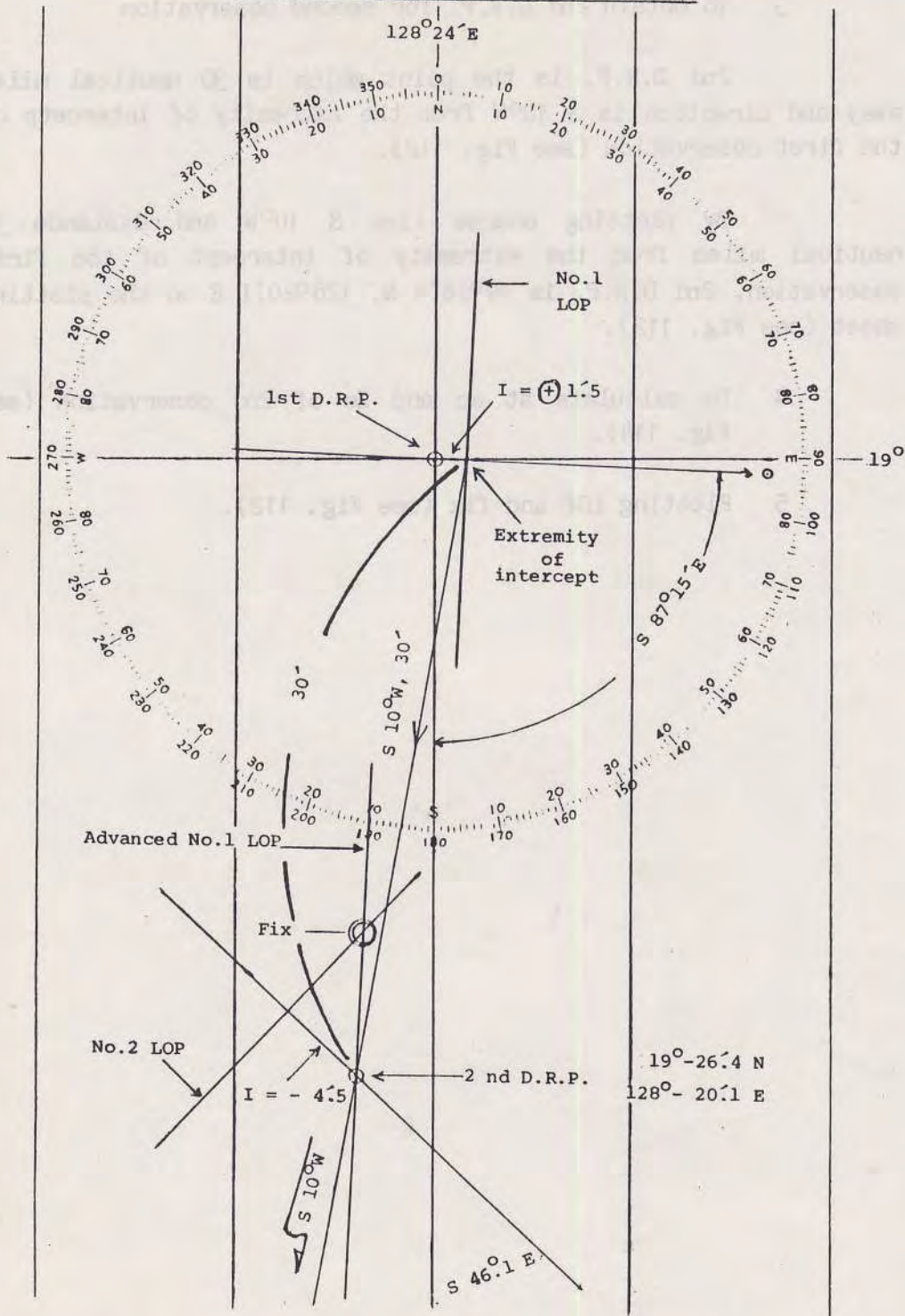
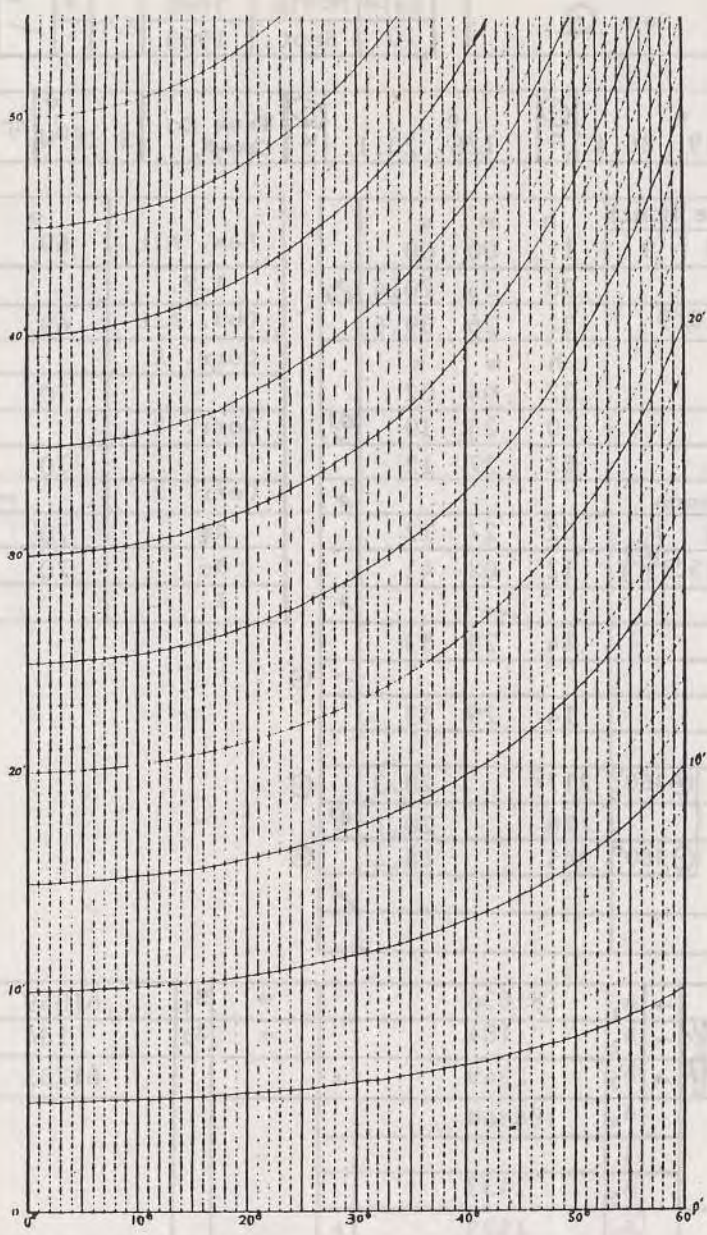



Fig. 112 How to fix









Latitude & Distance Scale






Fig. 113






Line of Position of a Celestial Body





Body's name	Sun 	Date	Month	Year	Z.T.	+	h
		10	Sept.	1963	-	-	-

D.R.P.	19° 26.4' 	128° 20.1' 	True Co. 	S 18° W	sp'd	3 1/2 kt.
--------	---	--	--	---------	------	-----------

*1	Ship's Time	Date	Month	h	m	s	
		10	9	11	00	00	
	L. in T.			08	33	20.4	
	Approx. U. (Date 10/9)			02	26	39.6	
	Chro. T.			h	m	s	
				02	04	02	
	Chro. E.			0	23	10	
	Corrected chro. T.			02	27	12	
	Morning or Afternoon						
	U. (Date 10/9)			02	27	12	

Sex. Alt.	69° 58.0'	
I.E.	1.0'	
Obs. Alt	69 59.0	
Corr. 1	8.3	
	70 07.3	
Corr. 2	0.2	
	70 07.5	
Corr. 3		
at	70 07.5	
ac	70 12.0	-
I	04.5	

*2	h _c in hours		14	29	53	
	h _c in degrees		360°	217°	28.3	
	Long.			128	20.1	
			360°	345	48.4	
	h					

*3	h	345° 48.4	→	A ₁	181636		→	Z ₁	61049	
	d	05 15.8		A ₂	184		=	Z ₂	184	
	l	19 26.4		A ₃	2549	+			61233	
				A ₄	184369					
				↓						
				A ₅	1433					
	l±d			A ₆	1523	+				
				A ₇	2956		→	Z ₃	47014	-
				↓				Z ₄	14219	
				a _c	70 12.0			↓	N 46 07.2 	

*4

Ref.





1. Approx. U = Ship's Time + L.in T. (E - long → , W - long. → )
2. h = h_c + L (E - long → , W - long → )
3. When l and d same name → l~d, contrary → l + d
4. When h > 180° suffix of Z_c → E, h < 180° suffix of Z_c → W

Fig. 114 Calculation Sheet

6 According to plotting sheet,

$$\begin{array}{rcl} \text{D - Lat.} & = & 22'8 \text{ S} \\ \text{Lat.} & & 19^{\circ}56'0 \text{ N} \\ \text{D - Lat.} & \frac{22'8 \text{ S}}{19^{\circ}33'2 \text{ N}} & \\ \text{D - Long.} & = & 3'5 \text{ W} \\ \text{Long.} & & 128^{\circ}24'0 \text{ E} \\ \text{D - Long.} & \frac{03'5 \text{ W} \ominus}{128^{\circ}20'5 \text{ E}} & \end{array}$$

Ans. $19^{\circ}33'2 \text{ N}$, $128^{\circ}20'5 \text{ E}$

- REVIEW -

Amplitude

Example :

On 5 August 1956, a navigator observed the sun's bearing by amplitude with magnetic compass in D.R.P. $32^{\circ}20' \text{ N}$, $129^{\circ}48' \text{ E}$.

What was the deviation of this compass? (Variation was $5^{\circ}2 \text{ W}$ here)

Solution 1

1 To obtain h



$$d (5/81956) U = 0^{\text{h}}$$

$$d = 17^{\circ}02'8 \text{ N (by nautical almanac (5/8))} \rightarrow h = 06^{\text{h}}45^{\text{m}}$$

$$l = 32^{\circ}20'0 \text{ N}$$

by the table of "Rising and setting Hour angle" (true Alt. = 0°)

2 To obtain G.A.T.

	12 ^h 00 ^m 00 ^s	
h	06 45 00	⊖
L.A.T.	5 15 00	
L. in T.	08 39 12	⊖
G.A.T. (4/8)	20 ^h 35 ^m 48 ^s	

↓

d = 17°05'1 N (by nautical almanac 4/8 → azimuth
 (true Lat.
 = 0°
 = E 20°3 N

l = 32°20'0 N

True amplitude = E 20°3 N
 = N 69°7 E → (90°-20°3
 = 69°7)

Compass bearing = N 88°5 E ⊖

by the table of "Rising and Setting Azimuth" (true Alt. = 0°

Compass error = 18°8 W
 Variation = 5.2 W -
 Deviation = 13°6 W

Ans. Deviation was 13°6 W

and setting for angle (true Alt. = 0°)

5 August 1956
Nautical Almanac

Moon d
Age 27.8

☉ Sun				Planet				P.P.				☾ Moon Tr.				P.P.			
U	E ₀	d	P.P. of d	U	E ₀	d	E _p d	U	E ₀	d	E _p d	U	E ₀	d	E _p d	U	E ₀	d	E _p d
h m s	° ' "	° ' "	h m s	h m s	° ' "	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s	h m s
0 11 54	N 17 2.8	0 0 0.0	0 0 0.0	♁ Venus				Tr.	h m s	h m s	h m s	0 13 23	33	N 18 9.3	1 2 0.1	0 13 23	33	N 18 9.3	1 2 0.1
2	1.5	10	1	♂ Mars				Tr.	h m s	h m s	h m s	1	21 8	18 1.1	3 7 4	1	21 8	18 1.1	3 7 4
4	17 0.1	20	2	h m s	° ' "	h m s	h m s	h m s	h m s	h m s	h m s	2	18 55	17 57.0	4 10 6	2	18 55	17 57.0	4 10 6
6	16 58.8	30	4	0 14 52	30	N 18 32.3	0 0 0.0	0 0 0.0	0 0 0.0	0 0 0.0	0 0 0.0	3	17 29	48.6	6 14 0.9	3	17 29	48.6	6 14 0.9
8	57.4	40	5	2	37	32.6	10 1 0	10 1 0	10 1 0	10 1 0	10 1 0	4	16 17	44.4	7 17 1.0	4	16 17	44.4	7 17 1.0
10	56.1	50	6	4	43	32.9	20 1 1	20 1 1	20 1 1	20 1 1	20 1 1	5	15 4	40.1	8 19 2	5	15 4	40.1	8 19 2
12 11 54	N 16 54.7	1 0 0.7	1 0 0.7	6	49	33.2	30 2 1	30 2 1	30 2 1	30 2 1	30 2 1	6	13 52	35.8	9 22 3	6	13 52	35.8	9 22 3
14	53.8	10	8	8	52 55	33.5	40 2 1	40 2 1	40 2 1	40 2 1	40 2 1	7	12 39	31.5	10 24 5	7	12 39	31.5	10 24 5
16	52.0	20	0.9	10	53 2	33.7	0 50 3	0 50 3	0 50 3	0 50 3	0 50 3	8	11 27	27.1	11 26 6	8	11 27	27.1	11 26 6
18	50.6	30	1.1	12 14 53	8	N 18 84.0	1 0 3 0.2	1 0 3 0.2	1 0 3 0.2	1 0 3 0.2	1 0 3 0.2	9	10 14	22.7	12 29 8	9	10 14	22.7	12 29 8
20	40.2	40	2	14	14	84.3	10 4 2	10 4 2	10 4 2	10 4 2	10 4 2	10			13 31 1.9	10			13 31 1.9
22	47.9	50	3	16	20	84.6	20 4 2	20 4 2	20 4 2	20 4 2	20 4 2	11			14 34 2.1	11			14 34 2.1
24 11 54	N 16 46.5	2 0 1.4	2 0 1.4	18	26	84.8	30 5 2	30 5 2	30 5 2	30 5 2	30 5 2	12			15 36 2	12			15 36 2
S.D. 15 49				20	32	85.1	40 5 3	40 5 3	40 5 3	40 5 3	40 5 3	13			16 38 3	13			16 38 3
S.D. 15 49				22	38	85.4	1 50 6	1 50 6	1 50 6	1 50 6	1 50 6	14			17 41 5	14			17 41 5
S.D. 15 49				24 14 53	44	N 18 35.7	2 0 6 0.3	2 0 6 0.3	2 0 6 0.3	2 0 6 0.3	2 0 6 0.3	15			18 43 6	15			18 43 6
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	16			19 46 8	16			19 46 8
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	17			20 48 2.9	17			20 48 2.9
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	18			21 50 3.1	18			21 50 3.1
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	19			22 53 2	19			22 53 2
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	20			23 55 4	20			23 55 4
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	21			24 58 7	21			24 58 7
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	22			26 02 3.8	22			26 02 3.8
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	23			27 05 1.0	23			27 05 1.0
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	24			28 07 1	24			28 07 1
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	25			29 09 3	25			29 09 3
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	26			30 11 5.1	26			30 11 5.1
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	27				27			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	28				28			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	29				29			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	30				30			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	31				31			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	32				32			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	33				33			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	34				34			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	35				35			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	36				36			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	37				37			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	38				38			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	39				39			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	40				40			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	41				41			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	42				42			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	43				43			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	44				44			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	45				45			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	46				46			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	47				47			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	48				48			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	49				49			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	50				50			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	51				51			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	52				52			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	53				53			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	54				54			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	55				55			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	56				56			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	57				57			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	58				58			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	59				59			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	60				60			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	61				61			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	62				62			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	63				63			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	64				64			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	65				65			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	66				66			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	67				67			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	68				68			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	69				69			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	70				70			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	71				71			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	72				72			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	73				73			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	74				74			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	75				75			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	76				76			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	77				77			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	78				78			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	79				79			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	80				80			
S.D. 15 49				♂ Mars				Tr.	h m s	h m s	h m s	81				81			
S.D. 15 49				♃ Jupiter				Tr.	h m s	h m s	h m s	82				82			
S.D. 15 49				♄ Saturn				Tr.	h m s	h m s	h m s	83				83			
S.D. 15 49				♅ Uranus				Tr.	h m s	h m s	h m s	84				84			
S.D. 15 49				♆ Neptune				Tr.	h m s	h m s	h m s	85				85			
S.D. 15 49				♁ Venus				Tr.	h m s	h m s	h m s	86				86			
S.D. 15 49																			

4 August 1956
Nautical Almanac

Moon Age 26.8

☉ Sun				Planet				P.P.				☾ Moon Tr. ^{h m} / _{10 2}				P.P.						
U	E _s	d	P.P. of d	U	E _p	d	P.P. of d	U	E _p	d	P.P. of d	U	E _t	d	P.P. of d	U	E _t	d	P.P. of d			
h h m s	° ' "		h m s	h h m s	° ' "		h m s	h h m s	° ' "		h m s	h h m s	° ' "		h m s	h h m s	° ' "		h m s			
0 11 53 59	N17 18.9		0 0 0.0	♀ Venus				Tr. ^{h m} / _{9 8}	0 14 22 31	N20 42.9		0 14 22 31	N20 42.9		0 14 22 31	N20 42.9		0 14 22 31	N20 42.9			
2 53 59	17.5		10 1	h h m s	° ' "		h m s	1 21 17	40.6		1 21 17	40.6		1 21 17	40.6		1 21 17	40.6		1 21 17	40.6	
4 54 0	16.2		20 2	0 14 51 12	N18 29.0		0 0 0.0	2 18 49	35.8		2 18 49	35.8		2 18 49	35.8		2 18 49	35.8		2 18 49	35.8	
6 0 0	14.9		30 3	2 19 19	29.2		10 1 0	4 17 35	33.4		4 17 35	33.4		4 17 35	33.4		4 17 35	33.4		4 17 35	33.4	
8 0 0	13.5		40 4	4 25 40	29.5		20 1 1	6 16 20	30.9		6 16 20	30.9		6 16 20	30.9		6 16 20	30.9		6 16 20	30.9	
10 1 1	12.2		50 5	6 32 29.8	30 2 1			8 15 6	28.4		8 15 6	28.4		8 15 6	28.4		8 15 6	28.4		8 15 6	28.4	
12 11 54 1	N17 10.9		1 0 0.7	8 39 30.1	40 2 1			10 13 52	25.8		10 13 52	25.8		10 13 52	25.8		10 13 52	25.8		10 13 52	25.8	
14 2 2	9.5		10 8	10 45 30.4	0 50 3 1			12 12 38	23.2		12 12 38	23.2		12 12 38	23.2		12 12 38	23.2		12 12 38	23.2	
16 2 2	8.2		20 0.9	12 14 51 52	N18 30.7		1 0 4 0.2	14 11 24	20.6		14 11 24	20.6		14 11 24	20.6		14 11 24	20.6		14 11 24	20.6	
18 3 3	6.9		30 1.0	14 51 58	30.9		10 4 2	16 10 10	17.9		16 10 10	17.9		16 10 10	17.9		16 10 10	17.9		16 10 10	17.9	
20 3 3	5.5		40 1	16 52 5	31.2		20 5 2	18 8 56	15.2		18 8 56	15.2		18 8 56	15.2		18 8 56	15.2		18 8 56	15.2	
22 4 4	4.2		1 50 2	18 11 31.5	30 5 2			(H.P.60.8, S.D.16 34)				14 35 3		14 35 3		14 35 3		14 35 3				
24 11 54 4	N17 2.8		2 0 1.3	20 18 31.8	40 6 3			6 14 7 42	N20 12.5		6 14 7 42	N20 12.5		6 14 7 42	N20 12.5		6 14 7 42	N20 12.5		6 14 7 42	N20 12.5	
S.D. 15 48				22 24 32.1	1 50 6 3			7 5 14	6.9		7 5 14	6.9		7 5 14	6.9		7 5 14	6.9		7 5 14	6.9	
U=0h				24 14 52 30	N18 32.3		2 0 7 0.3	8 4 0	4.0		8 4 0	4.0		8 4 0	4.0		8 4 0	4.0		8 4 0	4.0	
No. *	Star	E _s	d	♂ Mars				Tr. ^{h m} / _{2 54}	(H.P.60.9, S.D.16 36)				(H.P.61.0, S.D.16 39)									
1	Polaris	18 56 9	N89 3.4	h h m s	° ' "		h m s	12 21 7 18	S 7 49.7		1 0 9 0.0	12 13 57 55	N19 36.8		12 13 57 55	N19 36.8		12 13 57 55	N19 36.8		12 13 57 55	N19 36.8
2	Kochab	5 59 20	74 20.3	0 21 5 32	S 7 49.6		0 0 0 0.0	14 36	49.8		10 11 0	13 50 27	30.1		13 50 27	30.1		13 50 27	30.1		13 50 27	30.1
3	Dubhe	9 49 6	61 59.2	2 5 50	49.6		10 2 0	16 7 54	49.8		20 12 0	15 57 50	49.1		15 57 50	49.1		15 57 50	49.1		15 57 50	49.1
4	β Cassiop.	20 43 14	58 54.6	4 6 7	49.7		20 3 0	18 8 12	49.8		30 14 0	14 48 0	23.5		14 48 0	23.5		14 48 0	23.5		14 48 0	23.5
5	Menak	9 50 55	56 37.0	6 25	49.7		30 5 0	20 30	49.9		40 15 0	15 46 46	20.1		15 46 46	20.1		15 46 46	20.1		15 46 46	20.1
6	Alioth	7 58 1	N56 11.9	8 6 43	49.7		40 6 0	22 8 48	49.9		1 50 17 0	15 45 32	16.7		15 45 32	16.7		15 45 32	16.7		15 45 32	16.7
7	Schedir	20 12 4	56 17.9	10 7 1	49.7		0 50 8 0	24 21 9 6	S 7 49.3		2 0 18 0.0	16 44 19	13.2		16 44 19	13.2		16 44 19	13.2		16 44 19	13.2
8	Mizar	7 27 57	55 9.3	12 21 7 18	S 7 49.7		1 0 9 0.0	14 36	49.8		10 11 0	17 41 52	6.2		17 41 52	6.2		17 41 52	6.2		17 41 52	6.2
9	α Persei	17 28 54	49 42.3	14 36	49.8		10 11 0	16 7 54	49.8		20 12 0	17 40 38	19 2.7		17 40 38	19 2.7		17 40 38	19 2.7		17 40 38	19 2.7
10	Benetnasch	7 4 18	49 32.0	16 7 54	49.8		20 12 0	18 8 12	49.8		30 14 0	18 35 25	18 59.1		18 35 25	18 59.1		18 35 25	18 59.1		18 35 25	18 59.1
11	Capella	15 36 39	N45 57.2	20 30	49.9		40 15 0	20 30	49.9		40 15 0	14 48 0	23.5		14 48 0	23.5		14 48 0	23.5		14 48 0	23.5
12	Deneb	0 10 8	45 7.6	22 8 48	49.9		1 50 17 0	22 21 9 6	S 7 49.3		2 0 18 0.0	15 46 46	20.1		15 46 46	20.1		15 46 46	20.1		15 46 46	20.1
13	Vega	2 14 38	38 44.8	24 21 9 6	S 7 49.3		2 0 18 0.0	♃ Jupiter				Tr. ^{h m} / _{13 38}	(H.P.61.0, S.D.16 39)									
14	Castor	19 18 18	31 59.1	♃ Jupiter				Tr. ^{h m} / _{13 38}	(H.P.61.0, S.D.16 39)				(H.P.61.0, S.D.16 39)									
15	Alpheratz	20 43 58	28 51.1	h h m s	° ' "		h m s	12 10 21 42	N10 25.2		1 0 8 0.2	18 13 38 11	N18 55.5		18 13 38 11	N18 55.5		18 13 38 11	N18 55.5		18 13 38 11	N18 55.5
16	Pollux	13 7 29	N28 7.9	0 10 20 7	N10 27.5		0 0 0 0.0	14 21 57	24.8		10 9 2	19 35 45	48.1		19 35 45	48.1		19 35 45	48.1		19 35 45	48.1
17	α Cor. Bar.	5 17 16	26 51.8	2 23	27.1		10 1 0	16 22 13	24.4		20 11 3	20 33 18	44.4		20 33 18	44.4		20 33 18	44.4		20 33 18	44.4
18	Arcturus	6 36 26	19 24.6	4 38	26.7		20 3 1	18 29	24.0		30 12 3	21 32 5	36.8		21 32 5	36.8		21 32 5	36.8		21 32 5	36.8
19	Aldebaran	16 16 42	16 25.4	6 20 54	26.3		30 4 1	20 22 45	23.7		40 13 3	21 30 52	33.0		21 30 52	33.0		21 30 52	33.0		21 30 52	33.0
20	Markeb	21 47 30	14 58.4	8 21 10	26.0		40 5 1	22 23 1	23.3		1 50 15 4	22 28 25	25.2		22 28 25	25.2		22 28 25	25.2		22 28 25	25.2
21	Denebola	9 3 17	N14 48.9	10 26	25.6		0 50 7 2	24 10 23 16	N10 22.9		2 0 16 0.4	23 27 12	21.3		23 27 12	21.3		23 27 12	21.3		23 27 12	21.3
22	α Ophiuchi	3 17 11	12 35.6	♄ Saturn				Tr. ^{h m} / _{18 44}	(H.P.61.0, S.D.16 39)				(H.P.61.0, S.D.16 39)									
23	Regulus	10 44 4	12 10.8	h h m s	° ' "		h m s	12 5 14 40	S17 21.1		1 0 10 0.0	24 13 23 33	N18 9.3		24 13 23 33	N18 9.3		24 13 23 33	N18 9.3		24 13 23 33	N18 9.3
24	Altair	1 1 26	8 45.4	0 5 12 42	S17 20.9		0 0 0 0.0	14 15 0	21.1		10 12 0	Planet										
25	Betelgeuse	14 57 19	7 24.0	2 13 2	21.0		10 2 0	16 19	21.2		20 13 0	R.A.	d	Mag.	H.P.	S.D.						
26	Bellatrix	15 27 20	N 6 18.7	4 22	21.0		20 3 0	18 39	21.2		30 15 0	♀ 5 59	N18 29	-4.2	0.3	17						
27	Procyon	13 13 6	N 5 20.2	6 13 41	21.0		30 5 0	20 15 58	21.2		40 17 0	♂ 23 45	S 7 50	-1.9	0.3	10						
28	Rigel	15 37 41	S 8 14.9	8 14 1	21.0		40 7 0	22 16 18	21.3		1 50 18 0	♃ 10 30	N10 27	-1.3	0.0	15						
29	α Hydrae	11 24 41	8 28.2	10 20	21.1		0 50 8 0	24 16 37	S17 21.3		2 0 20 0.0	♄ 15 37	S17 21	+0.7	0.0	8						
30	Spica	7 27 13	10 56.2	12 5 14 40	S17 21.1		1 0 10 0.0	Planet				♅ 9 58	N13 52	-0.5	0.1	3						
31	Sirius	14 6 54	S16 39.3	14 15 0	21.1		10 12 0	Planet				Planet										
32	β Ceti	20 8 42	18 13.2	16 19	21.2		20 13 0	Planet				Planet										
33	Antares	4 23 22	26 20.3	18 39	21.2		30 15 0	Planet				Planet										
34	α Sgittarii	1 57 31	26 21.0	20 15 58	21.2		40 17 0	Planet				Planet										
35	Fomalhaut	21 54 50	29 50.9	22 16 18	21.3		1 50 18 0	Planet				Planet										
36	λ Scorpii	3 19 26	S37 4.5	24 16 37	S17 21.3		2 0 20 0.0	Planet				Planet										
37	Canopus	14 27 10	52 40.2	Planet				Planet				Planet										
38	α Pavonis	0 27 51	86 52.4	Planet				Planet				Planet										
39	Achernar	19 14 1	57 27.0	Planet				Planet				Planet										
40	β Crucis	8 4 57	59 27.4	Planet				Planet				Planet										
41	β Centauri	6 49 22	S60 10.2	Planet				Planet				Planet										
42	α Centauri	6 13 28	60 39.8	Planet				Planet				Planet										
43	α Crucis	3 25 57	62 51.8	Planet				Planet				Planet										
44	α Tri. Aust.	4 8 1	68 57.3	Planet				Planet				Planet										
45	β Carinae	11 37 27	S69 32.4	Planet				Planet				Planet										
R ₀ ^{h m s} / _{20 50 8}				Planet				Planet				Planet										

Fig. 116

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN

RISING AND SETTING AZIMUTH (True Alt.=0°)

lat. l	Declination						d								
	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°
0	16.0	17.0	18.0	19.0	20.0	21.0	22.0	23.0	24.0	25.0	26.0	27.0	28.0	29.0	30.0
2	16.0	17.0	18.0	19.0	20.0	21.0	22.0	23.0	24.0	25.0	26.0	27.0	28.0	29.0	30.0
4	16.0	17.1	18.1	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	29.1	30.1
6	16.1	17.1	18.1	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.2	27.2	28.2	29.2	30.2
8	16.2	17.2	18.2	19.2	20.2	21.2	22.2	23.2	24.3	25.3	26.3	27.3	28.3	29.3	30.3
10	16.3	17.3	18.3	19.3	20.3	21.4	22.4	23.4	24.4	25.4	26.4	27.5	28.5	29.5	30.5
12	16.4	17.4	18.4	19.4	20.5	21.5	22.5	23.6	24.6	25.6	26.6	27.7	28.7	29.7	30.7
14	16.5	17.5	18.6	19.6	20.6	21.7	22.7	23.8	24.8	25.8	26.9	27.9	28.9	30.0	31.0
16	16.7	17.7	18.8	19.8	20.9	21.9	22.9	24.0	25.0	26.1	27.1	28.2	29.2	30.3	31.4
18	16.9	17.9	19.0	20.0	21.1	22.1	23.2	24.3	25.3	26.4	27.5	28.5	29.6	30.7	31.7
20	17.1	18.1	19.2	20.3	21.4	22.4	23.5	24.6	25.6	26.7	27.8	28.9	30.0	31.1	32.2
21	17.2	18.3	19.3	20.4	21.5	22.6	23.7	24.8	25.8	26.9	28.0	29.1	30.2	31.3	32.4
22	17.3	18.4	19.5	20.6	21.7	22.7	23.8	24.9	26.0	27.1	28.2	29.3	30.4	31.5	32.6
23	17.4	18.5	19.6	20.7	21.8	22.9	24.0	25.1	26.2	27.3	28.4	29.6	30.7	31.8	32.9
24	17.6	18.7	19.8	20.9	22.0	23.1	24.2	25.3	26.4	27.6	28.7	29.8	30.9	32.1	33.2
25	17.7	18.8	19.9	21.1	22.2	23.3	24.4	25.5	26.7	27.8	28.9	30.1	31.2	32.3	33.5
26	17.9	19.0	20.1	21.2	22.4	23.5	24.6	25.8	26.9	28.0	29.2	30.3	31.5	32.6	33.8
27	18.0	19.2	20.3	21.4	22.6	23.7	24.9	26.0	27.2	28.3	29.5	30.6	31.8	33.0	34.1
28	18.2	19.3	20.5	21.6	22.8	24.0	25.1	26.3	27.4	28.6	29.8	30.9	32.1	33.3	34.5
29	18.4	19.5	20.7	21.9	23.0	24.2	25.4	26.5	27.7	28.9	30.1	31.3	32.5	33.7	34.9
30	18.6	19.7	20.9	22.1	23.3	24.5	25.6	26.8	28.0	29.2	30.4	31.6	32.8	34.1	35.3
31	18.8	19.9	21.1	22.3	23.5	24.7	25.9	27.1	28.3	29.5	30.8	32.0	33.2	34.5	35.7
32	19.0	20.2	21.4	22.6	23.8	25.0	26.2	27.4	28.7	29.9	31.1	32.4	33.6	34.9	36.1
33	19.2	20.4	21.6	22.9	24.1	25.3	26.5	27.8	29.0	30.3	31.5	32.8	34.0	35.3	36.6
34	19.4	20.5	21.9	23.1	24.4	25.6	26.9	28.1	29.4	30.7	31.9	33.2	34.5	35.8	37.1
35	19.7	20.9	22.2	23.4	24.7	26.0	27.2	28.5	29.8	31.1	32.4	33.7	35.0	36.3	37.6
36	19.9	21.2	22.5	23.7	25.0	26.3	27.6	28.9	30.2	31.5	32.8	34.1	35.5	36.8	38.2
37	20.2	21.5	22.8	24.1	25.4	26.7	28.0	29.3	30.6	31.9	33.3	34.6	36.0	37.4	38.8
38	20.5	21.8	23.1	24.4	25.7	27.1	28.4	29.7	31.1	32.4	33.8	35.2	36.6	38.0	39.4
39	20.8	22.1	23.4	24.8	26.1	27.5	28.8	30.2	31.6	32.9	34.3	35.8	37.2	38.6	40.1
40	21.1	22.4	23.8	25.2	26.5	27.9	29.3	30.7	32.1	33.5	34.9	36.4	37.8	39.3	40.8
41	21.4	22.8	24.2	25.6	27.0	28.4	29.8	31.2	32.6	34.1	35.5	37.0	38.5	40.0	41.5
42	21.8	23.2	24.6	26.0	27.4	28.8	30.3	31.7	33.2	34.7	36.2	37.7	39.2	40.7	42.3
43	22.1	23.5	25.0	26.4	27.9	29.3	30.8	32.3	33.8	35.3	36.8	38.4	39.9	41.5	43.1
44	22.5	24.0	25.4	26.9	28.4	29.9	31.4	32.9	34.4	36.0	37.5	39.2	40.7	42.4	44.0
45	23.0	24.4	25.9	27.4	28.9	30.5	32.0	33.6	35.1	36.7	38.3	39.9	41.6	43.3	45.0
46	23.4	24.9	26.4	28.0	29.5	31.1	32.6	34.2	35.8	37.5	39.1	40.8	42.5	44.3	46.0
47	23.8	25.4	27.0	28.5	30.1	31.7	33.3	35.0	36.6	38.3	40.0	41.7	43.5	45.3	47.2
48	24.3	25.9	27.5	29.1	30.7	32.4	34.1	35.7	37.4	39.2	40.9	42.7	44.5	46.4	48.4
49	24.9	26.5	28.1	29.8	31.4	33.1	34.8	36.6	38.3	40.1	41.9	43.8	45.7	47.7	49.7
50	25.4	27.1	28.7	30.4	32.2	33.9	35.6	37.4	39.3	41.1	43.0	44.9	46.9	49.0	51.1
51	26.0	27.7	29.4	31.2	32.9	34.7	36.5	38.4	40.3	42.2	44.2	46.2	48.2	50.4	52.6
52	26.6	28.4	30.1	31.9	33.8	35.6	37.5	39.4	41.4	43.4	45.4	47.5	49.7	52.0	54.3
53	27.3	29.1	30.9	32.8	34.6	36.6	38.5	40.5	42.5	44.6	46.7	49.0	51.3	53.7	56.2
54	28.0	29.8	31.7	33.6	35.6	37.6	39.6	41.7	43.8	46.0	48.2	50.6	53.0	55.6	58.3
55	28.7	30.7	32.6	34.6	36.7	38.7	40.8	42.9	45.2	47.5	49.8	52.3	54.9	57.7	60.7
56	29.5	31.5	33.6	35.6	37.7	39.9	42.1	44.3	46.7	49.1	51.6	54.3	57.1	60.1	63.4
57	30.4	32.5	34.6	36.7	38.9	41.2	43.5	45.9	48.3	50.9	53.6	56.5	59.6	62.9	66.7
58	31.3	33.5	35.7	37.9	40.2	42.6	45.0	47.5	50.1	52.9	55.8	58.9	62.4	66.2	70.7
59	32.4	34.6	36.9	39.2	41.6	44.1	46.7	49.4	52.2	55.1	58.3	61.8	65.7	70.3	76.2
60	33.5	35.8	38.2	40.6	43.3	45.8	48.5	51.4	54.4	57.7	61.2	65.2	69.9	75.8	90.0
61	34.7	37.1	39.6	42.2	44.9	47.7	50.6	53.7	57.0	60.6	64.7	69.4	75.5	90.0	
62	36.0	38.5	41.2	43.9	46.3	49.8	52.9	56.3	60.0	64.2	69.0	75.2	90.0		
63	37.4	40.1	42.9	45.8	48.9	52.1	55.6	59.4	63.6	68.6	74.9	90.0			
64	39.0	41.8	44.8	48.0	51.3	54.8	58.7	63.0	68.1	74.6	90.0				
65	40.7	43.8	47.0	50.4	54.0	58.0	62.4	67.6	74.2	90.0					

Prefix of Azimuth should be measured from East or west.
 Suffix of Azimuth is the same as the name of declination.

Fig. 117

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

RISING AND SETTING HOUR ANGLE (True Alt.=0°)

lat. l	Declination												d					
	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°			
0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0	6 0			
2	2	2	3	3	3	3	3	3	4	4	4	4	4	4	5			
4	5	5	5	6	6	6	6	7	7	7	8	8	9	9	9			
6	7	7	8	8	9	9	10	10	11	11	12	12	13	13	14			
8	9	10	10	11	12	12	13	14	14	15	16	16	17	18	19			
10	6 12	6 12	6 13	6 14	6 15	6 16	6 16	6 17	6 18	6 19	6 20	6 21	6 22	6 22	6 23			
12	14	15	16	17	18	19	20	21	22	23	24	25	25	27	28			
14	16	17	19	20	21	22	23	24	25	27	28	29	30	32	33			
16	19	20	21	23	24	25	27	28	29	31	32	34	35	37	38			
18	21	23	24	26	27	29	30	32	33	35	36	38	40	42	43			
20	6 24	6 26	6 27	6 29	6 30	6 32	6 34	6 36	6 37	6 39	6 41	6 43	6 45	6 47	6 49			
21	25	27	29	30	32	34	35	38	39	41	43	45	47	49	51			
22	27	28	30	32	34	36	38	40	41	43	45	48	50	52	54			
23	28	30	32	34	36	38	40	42	44	46	48	50	52	54	57			
24	29	31	33	35	37	39	41	44	46	48	50	52	55	6 57	7 0			
25	6 31	6 33	6 35	6 37	6 39	6 41	6 43	6 46	6 48	6 50	6 53	6 55	6 57	7 0	7 2			
26	32	34	36	39	41	43	45	48	50	53	55	6 58	7 0	3	5			
27	34	36	38	40	43	45	48	50	52	55	6 58	7 0	3	6	8			
28	35	37	40	42	45	47	50	52	55	6 57	7 0	3	6	9	12			
29	37	39	42	44	47	49	52	54	6 57	7 0	3	6	9	12	15			
30	6 38	6 41	6 43	6 46	6 49	6 51	6 54	6 57	7 0	7 2	7 5	7 8	7 12	7 15	7 18			
31	40	42	45	48	51	53	56	6 59	2	5	8	11	15	18	21			
32	41	44	47	50	53	56	6 58	7 2	5	8	11	14	18	21	25			
33	43	46	49	52	55	6 58	7 1	4	7	11	14	17	21	24	28			
34	45	48	51	54	57	7 0	3	7	10	13	17	20	24	28	32			
35	6 46	6 49	6 53	6 56	6 59	7 2	7 6	7 9	7 13	7 16	7 20	7 24	7 27	7 31	7 35			
36	48	51	55	6 58	7 1	5	8	12	15	19	23	27	31	35	39			
37	50	53	57	7 0	4	7	11	15	18	22	26	30	34	39	43			
38	52	55	6 59	7 2	6	10	14	17	21	25	30	34	38	43	47			
39	54	57	7 1	5	9	12	16	20	25	29	33	37	42	47	51			
40	6 55	6 59	7 3	7 7	7 11	7 15	7 19	7 23	7 24	7 32	7 37	7 41	7 45	7 51	7 56			
41	6 58	7 2	6	10	14	18	22	27	31	36	40	45	50	7 55	8 0			
42	7 0	4	8	12	17	21	25	30	35	39	44	49	54	8 0	5			
43	2	6	11	15	19	24	29	33	38	43	48	53	7 59	4	10			
44	4	9	13	18	22	27	32	37	42	47	52	7 58	8 4	9	16			
45	7 7	7 11	7 16	7 21	7 25	7 30	7 35	7 40	7 46	7 51	7 57	8 3	8 8	8 15	8 21			
46	9	14	19	24	29	34	39	44	50	7 55	8 1	7	14	20	27			
47	12	17	22	27	32	37	43	48	54	8 0	6	12	19	26	33			
48	14	19	25	30	35	41	47	53	7 59	5	11	18	25	32	40			
49	17	22	28	33	39	45	51	7 57	8 3	10	17	24	31	38	46			
50	7 20	7 25	7 31	7 37	7 43	7 49	7 55	8 2	8 8	8 15	8 22	8 30	8 37	8 45	8 54			
51	23	29	35	41	47	53	8 0	6	13	21	28	36	44	8 53	9 2			
52	26	32	38	45	51	7 58	5	12	19	27	35	43	8 52	9 1	11			
53	29	36	42	49	7 56	8 2	10	17	25	33	41	50	9 0	9	20			
54	33	40	46	53	8 0	8	15	23	31	40	49	8 53	8	19	30			
55	7 37	7 44	7 51	7 58	8 5	8 13	8 21	8 29	8 38	8 47	8 57	9 7	9 13	9 20	9 42			
56	41	48	7 55	8 3	11	19	27	36	45	8 55	9 5	15	23	41	9 55			
57	45	52	8 0	8	16	25	34	43	8 53	9 4	15	27	40	9 54	10 11			
58	49	7 57	5	14	22	32	41	8 51	9 2	13	25	38	9 53	10 10	30			
59	54	8 2	11	20	29	39	49	9 0	11	24	37	9 52	10 9	29	10 56			
60	7 59	8 8	8 17	8 26	8 36	8 47	8 58	9 9	9 22	9 35	9 51	10 8	10 29	10 55	12 0			
61	8 5	14	24	34	44	8 55	9 7	20	34	9 49	10 7	27	10 54	12 0				
62	11	20	31	41	8 53	9 5	18	32	9 47	10 5	26	10 54	12 0					
63	17	27	38	8 50	9 2	16	30	9 46	10 4	25	10 53	12 0						
64	24	35	47	9 0	13	28	9 44	10 2	24	10 52	12 0							
65	8 32	8 44	8 57	9 10	9 25	9 42	10 0	10 22	10 51	12 0								

when name of declination is the same as that of latitude, use the tabulated value. If contrary, use the value (12h- tabulated value)

Fig. 118

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Solution 2

1 To obtain h
d (5/8/1956) U = 0h

↓
d = 17°-20.8 N (by nautical almanac 5/8) → h = 06h45m
l = 32°-20.0 N

by the table of
"Rising and Setting
Hour Angle (true
Alt. = 0°

2 To obtain G.A.T. to seek correct d.

h	12 ^h 00 ^m 00 ^s	
L.A.T. (5/8)	06 45 00	⊖
L. in T.	05 15 00	
G.A.T. (4/8)	08 39 12	⊖
	20 35 48	
	↓	
d =	17°05.1 N	}
l =	32°20.0 N	

By formula $\sin \text{Amplitude} = \frac{\sin d}{\cos l}$

$\frac{\sin (17^{\circ}05')}{\cos (32^{\circ}20')} = \frac{0.29376}{0.84495} = 0.3474$

Amplitude = E 20°20' N (By natural trigonometric functions table)

Because of rising sun The same name as declination (d)

Ref.

Solution by electronic calculator CASIO fx-950 or fx-180P

$$\sin \text{Amplitude} = \frac{\sin (17^{\circ}05')}{\cos (32^{\circ}20')}$$

Example 18

On 14 February 1956, a navigator observed the sun's bearing by amplitude with magnetic compass when the sun was setting in D.R.P. $22^{\circ}06' N$, $109^{\circ}17' W$. The magnetic compass bearing of the sun was $N 87^{\circ}5' W$, and local variation was $11^{\circ} E$.

What was the deviation of this compass?

Solution

1 To obtain h

14/2/56 $U = 0^h \rightarrow d = 13^{\circ}26'.0 S$ (By nautical almanac 14/2/1956 Fig. 119)

$d = 13^{\circ}26'.0 S$ $h = (12^h - 6^h22^m) = 5^h38^m$

$l = 22^{\circ}06'.0 N$

↑
Be careful!

By the table of "Rising and Setting Hour Angle true Alt. = 0°

2 To obtain G.A.T. to seek correct d

	$12^h00^m00^s$	
h	<u>05 38 00</u> ⊕	
L.A.T. (14/2)	17 38 00	
L in T	<u>07 17 08</u> ⊕	
	24 55 08	

	<u>24</u> ⊖	
G.A.T. (15/2)	00 55 08	

$d = (U = 0^h)$	$13^{\circ}05.7 S$	
P.P. (55^m08^s)	<u>0.8</u> ⊖	
$d = (U = 00^h55^m08^s)$	$13^{\circ}04.9 S$	

→ By nautical almanac 15/2/1956 (Fig. 120)

d = 13°04'9 S

l = 22°06'0 N

sin amplitude = $\frac{\sin d}{\cos l}$

= $\frac{\sin (13^{\circ}04'9)}{\cos (22^{\circ}06'0)}$

By electronic calculator CASIO fx-950 or fx-180P

1 3 0 0 4 . 9 0 → 13 . 0 8 1 6 6 6 6 7

INV 0 → 13° 4' 54"

Sin → 0 . 2 2 6 3 3 9 6 4 5

+ 2 2 0 6 0 → 22 . 1

INV 0 → 22° 6' 0"

cos → 0 . 9 2 6 5 2 8 6 3

= → 0 . 2 4 4 2 8 7 8 0 5

INV Sin → 14 . 1 3 9 7 4 9 1 6

Ans. 14°1

INV 0 → 14° 8' 23"1

Amplitude = W 14°1 S
 ↓
 Amplitude = S 75°9 W (= 90°-14°1) Be careful!
 Compass bearing = N 87°5 W ⊖
 Compass error = 16°6 W
 Variation = 11°0 E ⊕
 Deviation = 27°6 W

Ans. Deviation was 27°6 W



15 February 1956

Moon ^d
Age 3.1

Nautical Almanac

☉ Sun				Planet				☾ Moon				
U	E _s	d	P.P.	U	E _p	d	P.P.	U	E _t	d	P.P.	
h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	
0 11 45.43	S 13 5.7	0 0	0.0	♀ Venus				Tr. 14.41	h m s	° ' "	h m s	° ' "
2 47	4.0	10	1						0 9 39 18	N 4 53.4	1 2 0.2	
4 41	2.3	20	3						39 24	4 59.4	2 4 4	
6 43	13 0.6	30	4						37 29	5 5.5	3 5 6	
8 44	12 58.9	40	6						36 31	11.5	4 7 0.0	
10 44	57.2	50	7						35 33	17.5	5 9 1.0	
12 11 45 44	S 12 55.5	1 0	0.9						34 44	23.5	6 11 2	
14 44	53.8	10	1.0						33 49	29.5	7 13 4	
16 44	52.1	20	1						32 54	35.5	8 15 6	
18 45	50.4	30	3						31 59	41.5	9 16 1.8	
20 45	48.7	40	4						30 9	47.5	10 18 7.0	
22 45	47.0	50	6						29 13	53.5	11 20 2	
24 11 45 45	S 12 45.3	2 0	1.7							59.5	12 22 4	
S.D. 16 14.1									(H.P.56.4, S.D.15 21)			
U=Ob				♂ Maxs				Tr. 7.44				
No.	Star	E _t	d	h m s	° ' "	h m s	° ' "	h m s	° ' "	h m s	° ' "	
1	Polaris	7 43 10	N 89 3.9	0 16 15 26	S 23 2.5	0 0 0 0.0		6 9 29 18	N 6 5.5	16 29 2		
2	Kochab	18 45 8	71 10.7	2 32	2.7	10 1 0		27 23	11.5	17 31 4		
3	Dubhe	22 34 51	61 59.0	4 37	3.0	20 1 1		26 27	17.4	18 33 6		
4	α Cassiop.	9 29 8	58 54.7	6 43	3.3	30 2 1		25 32	23.4	19 35 3.8		
5	Merak	22 36 41	55 36.8	8 48	3.6	40 2 1		24 37	29.4	20 37 4.0		
6	Alioth	20 43 49	N 56 11.5	10 54	3.9	0 50 3 1		23 41	35.3	21 39 2		
7	Schedir	8 57 57	56 18.1	12 16 15 59	S 23 4.2	1 0 3 0.2		22 46	41.3	22 40 4		
8	Mizar	20 13 45	55 8.9	14 16 5	4.5	10 4 2		21 50	47.2	23 42 6		
9	α Persei	6 14 45	49 42.6	16 10	4.8	20 4 2		20 54	53.2	24 44 4.8		
10	Benetnasch	19 50 7	49 31.5	18 16	5.1	30 5 2		19 59	6 59.1	25 46 5.0		
11	Capella	4 22 28	N 45 57.5	20 21	5.3	40 5 3		19 3	7 5.0	26 48 2		
12	Dench	12 56 2	45 7.3	22 27	5.6	1 50 6 3		18 7	10.9	27 49 4		
13	Vega	15 0 30	38 44.3	24 16 16 32	S 23 5.9	2 0 6 0.3				28 51 6		
14	Castor	2 4 6	31 59.1					(H.P.56.5, S.D.15 23)				
15	Alphertaz	9 29 50	29 51.0									
16	Pollux	1 53 17	N 29 7.9									
17	α Cor. Ber.	18 3 7	26 51.4									
18	Arcturus	19 22 16	19 24.3									
19	Aldebaran	5 2 31	16 25.3									
20	Markab	10 33 23	14 58.2									
21	Deerhola	21 49 6	N 14 48.8									
22	α Ophiuchi	16 3 3	12 35.3									
23	Regulus	23 29 52	12 10.7									
24	Alhaz	13 47 19	8 45.0									
25	Betelgeuse	3 43 7	7 23.9									
26	Bellatrix	4 13 9	N 6 18.6									
27	Procyon	1 59 55	N 5 20.1									
28	Rigel	4 23 30	S 8 15.2									
29	α Hydrae	0 10 29	8 28.3									
30	Spica	20 13 3	10 56.1									
31	Sirius	2 52 42	S 16 39.5									
32	β Ceti	8 54 34	18 13.7									
33	Antares	17 9 13	26 20.7									
34	α Sagittarii	14 43 24	26 21.1									
35	Fomalhaut	10 40 44	29 51.3									
36	λ Scorpii	16 5 19	S 37 4.3									
37	Canopus	3 12 57	52 40.6									
38	α Pavonis	13 13 47	56 52.5									
39	Achernar	7 59 53	57 27.8									
40	β Crucis	20 50 45	59 26.9									
41	β Centauri	19 35 12	S 60 9.6									
42	α Centauri	18 59 19	60 33.2									
43	α Crucis	21 11 45	62 51.3									
44	α Tri. Austral.	16 51 56	68 56.8									
45	β Carinae	0 23 9	S 69 32.3									
R _o 9 35 57												
				♂ Saturn				Tr. 6.25				
				h m s	° ' "	h m s	° ' "					
				0 17 33 37	S 18 35.3	0 0 0 0.0						
				2 33 55	35.4	10 2 0						
				4 34 14	35.4	20 3 0						
				6 33	35.4	30 5 0						
				8 54 52	35.5	40 6 0						
				10 35 11	35.5	0 50 8 0						
				12 17 35 29	S 18 35.5	1 0 10 0.0						
				14 35 48	35.5	10 11 0						
				16 36 7	35.6	20 13 0						
				18 26	35.6	30 14 0						
				20 36 45	35.6	40 16 0						
				22 37 4	35.6	1 50 17 0						
				24 17 37 22	S 18 35.7	2 0 19 0.0						
								Planet				
								R.A.	d	Mag	H.P. S.D.	
								♀	0 17 N 1 20	-3.6	0.1 7	
								♂	17 21 S 23 2	+1.3	0.1 3	
								♂	9 57 N 13 43	-2.1	0.0 21	
								♂	16 2 S 18 35	+0.7	0.0 7	
								♂	20 7 S 18 56	+0.4	0.2 4	

Fig. 120

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

Example

On 28 December 1973, a navigator observed the bearing of the sun by amplitude as S 56°15'E with magnetic compass when the sun was rising in D.R.P. 42°56'N, 140°12'E and local variation was 4°20'W.

What was the deviation?

Note In this case ship's time was not given. So you must calculate Local Mean Time of Sunrise first by the table attached in the nautical almanac.

Solution

1 To obtain L.M.T. of Sunrise

By the table L.M.T. of Sunrise, Sunset and Duration of Twilight for Northern Latitudes,

L.M.T. Sunrise 28/12	07 ^h 30 ^m 00 ^s
L. in T.	09 20 48 ⊖
G.M.T. 27/12	22 09 12

↓

d for 22	23°18'3 S
P.P. for 09 ^m 12 ^s	0.0
d for 22 ^h 09 ^m 12 ^s	23°18'3 S

d = 23°18'3 S

{ $\ell = 42^{\circ}56'.0$ N (By D.R.P.)

$$\sin \text{Amplitude} = \frac{\sin d}{\cos \ell} = \frac{\sin (23^{\circ}18'.3)}{\cos (42^{\circ}56'.0)}$$

2. Calculation by electronic calculator CASIO fx-950 or fx-180P

23 000 18 000 . 3 000 INV 000 → 23° 18' 18"

sin → 0 . 3 9 5 6 2 5 6 5

÷ 42 000 56 000 INV 000 → 42° 56' 0"

cos → 0 . 7 3 2 1 4 6 7 4 7

= → 0 . 5 4 0 3 6 3 8 7 1

INV Sin → 32 . 7 0 8 4 1 2 5 5

INV 000 → 32° 42' 30" 29

= E 32°43' S

True b'g Amp.	=	E 32°43' S
		<u>90°</u> ⊖
True b'g by Amp.		S 57°17' E
Comp. b'g		S 56°15' E ⊖
Comp. error		1°02' W
Variation		<u>4°20' W</u> ⊖
Deviation		3°18' E

Ans. Deviation = 3°18' E

SUNRISE SUNSET AND DURATION OF TWILIGHT FOR NORTHERN LATITUDES L.M.T.

Date	Sunrise												
	42°N	44°N	46°N	48°N	50°N	52°N	54°N	56°N	58°N	60°N	62°N	65°N	70°N
1 1	7 28	7 34	7 42	7 49	7 58	8 08	8 18	8 31	8 45	9 02	9 22	10 05	...
1 11	7 27	7 33	7 40	7 47	7 55	8 01	8 14	8 25	8 38	8 53	9 11	9 47	...
1 21	7 22	7 28	7 34	7 40	7 47	7 55	8 03	8 13	8 24	8 37	8 52	9 21	10 55
1 31	7 14	7 18	7 23	7 29	7 36	7 41	7 49	7 57	8 06	8 16	8 28	8 50	9 50
2 10	7 02	7 06	7 10	7 15	7 19	7 24	7 30	7 36	7 43	7 51	8 00	8 17	8 58
2 20	6 49	6 52	6 55	6 58	7 01	7 05	7 09	7 14	7 19	7 24	7 31	7 42	8 09
3 2	6 31	6 35	6 37	6 39	6 41	6 41	6 46	6 49	6 52	6 56	7 00	7 06	7 22
3 12	6 17	6 18	6 19	6 19	6 19	6 20	6 21	6 22	6 23	6 25	6 26	6 27	6 36
3 22	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00
4 1	5 43	5 42	5 40	5 39	5 39	5 39	5 35	5 33	5 31	5 28	5 25	5 22	5 03
4 11	5 26	5 24	5 21	5 18	5 16	5 12	5 09	5 05	5 00	4 55	4 50	4 39	4 15
4 21	5 10	5 07	5 03	4 59	4 55	4 50	4 45	4 40	4 33	4 26	4 18	4 02	3 25
5 1	4 56	4 52	4 47	4 42	4 36	4 30	4 21	4 16	4 08	3 58	3 47	3 26	2 31
5 11	4 41	4 36	4 33	4 26	4 20	4 12	4 04	3 55	3 41	3 32	3 17	2 49	1 22
5 21	4 34	4 28	4 21	4 14	4 06	3 57	3 48	3 36	3 24	3 09	2 50	2 14	...
5 31	4 27	4 20	4 13	4 05	3 56	3 46	3 35	3 23	3 08	2 50	2 28	1 40	...
6 10	4 21	4 10	4 00	4 00	3 51	3 40	3 28	3 14	2 58	2 38	2 13	1 12	...
6 20	4 24	4 16	4 08	3 59	3 50	3 39	3 26	3 12	2 55	2 34	2 08	0 57	...
6 30	4 27	4 20	4 12	4 03	3 51	3 41	3 31	3 17	3 00	2 40	2 14	1 09	...
7 10	4 31	4 26	4 19	4 10	4 01	3 51	3 40	3 27	3 12	2 53	2 30	1 38	...
7 20	4 11	4 05	4 00	4 00	4 00	4 00	4 00	4 00	4 00	4 00	4 00	4 00	4 00
7 30	4 51	4 45	4 39	4 33	4 26	4 18	4 09	3 59	3 48	3 35	3 19	2 49	1 00
8 9	5 01	4 56	4 51	4 46	4 40	4 33	4 26	4 18	4 09	3 58	3 46	3 23	2 20
8 19	5 11	5 08	5 04	4 59	4 55	4 50	4 44	4 38	4 31	4 23	4 13	3 56	3 14
8 29	5 22	5 19	5 16	5 13	5 10	5 06	5 02	4 57	4 52	4 47	4 40	4 28	4 00
9 8	5 32	5 30	5 29	5 27	5 25	5 22	5 20	5 17	5 14	5 10	5 06	4 59	4 42
9 18	5 42	5 42	5 41	5 40	5 39	5 38	5 37	5 36	5 35	5 34	5 32	5 29	5 22
9 28	5 53	5 53	5 54	5 54	5 55	5 55	5 55	5 56	5 57	5 57	5 58	5 59	6 02
10 8	6 04	6 05	6 07	6 08	6 10	6 12	6 14	6 16	6 18	6 21	6 24	6 30	6 42
10 18	6 15	6 18	6 20	6 23	6 26	6 29	6 33	6 36	6 41	6 46	6 51	7 01	7 24
10 28	6 27	6 30	6 34	6 38	6 42	6 47	6 52	6 58	7 04	7 11	7 19	7 34	8 09
11 7	6 39	6 44	6 48	6 53	6 59	7 05	7 11	7 19	7 27	7 36	7 47	8 08	9 00
11 17	6 52	6 57	7 02	7 09	7 15	7 22	7 31	7 40	7 50	8 02	8 16	8 42	10 00
11 27	7 03	7 09	7 16	7 23	7 30	7 39	7 48	7 59	8 11	8 25	8 42	9 16	...
12 7	7 14	7 20	7 27	7 35	7 43	7 53	8 03	8 15	8 29	8 45	9 05	9 46	...
12 17	7 22	7 29	7 36	7 44	7 53	8 03	8 14	8 26	8 41	8 58	9 20	10 05	...
12 27	7 27	7 33	7 41	7 49	7 58	8 07	8 18	8 31	8 46	9 03	9 24	10 10	...
12 37	7 28	7 34	7 41	7 49	7 57	8 07	8 17	8 29	8 42	8 58	9 18	9 58	...
Date	Duration of Twilight												
	42°N	44°N	46°N	48°N	50°N	52°N	54°N	56°N	58°N	60°N	62°N	65°N	70°N
1 1	1 40	1 44	1 48	1 53	1 58	2 05	2 12	2 20	2 31	2 43	2 59	3 35	...
1 11	1 39	1 43	1 47	1 51	1 56	2 02	2 09	2 17	2 27	2 39	2 53	3 23	...
1 21	1 37	1 41	1 45	1 49	1 51	2 00	2 06	2 13	2 22	2 32	2 45	3 10	4 36
1 31	1 35	1 39	1 43	1 47	1 51	1 57	2 03	2 09	2 17	2 27	2 38	2 58	3 57
2 10	1 34	1 37	1 41	1 45	1 49	1 54	2 00	2 06	2 13	2 22	2 32	2 50	3 37
2 20	1 33	1 36	1 39	1 43	1 47	1 52	1 58	2 04	2 11	2 19	2 28	2 46	3 27
3 2	1 32	1 35	1 39	1 43	1 47	1 52	1 57	2 03	2 10	2 18	2 28	2 45	3 27
3 12	1 33	1 36	1 39	1 43	1 48	1 54	1 58	2 05	2 12	2 21	2 31	2 50	3 39
3 22	1 34	1 37	1 41	1 45	1 50	1 55	2 01	2 09	2 17	2 27	2 39	3 02	4 20
4 1	1 36	1 39	1 44	1 48	1 54	2 00	2 07	2 15	2 26	2 38	2 54	3 31	...
4 11	1 39	1 43	1 48	1 53	1 59	2 07	2 16	2 27	2 41	3 00	3 29
4 21	1 43	1 48	1 53	2 00	2 08	2 17	2 29	2 45	3 10	4 08
5 1	1 48	1 54	2 00	2 09	2 19	2 32	2 51	3 25
5 11	1 54	2 01	2 09	2 20	2 35	2 57	3 51
5 21	2 00	2 09	2 20	2 34
5 31	2 06	2 16	2 30	2 51	3 45
6 10	2 11	2 22	2 39	3 08
6 20	2 12	2 25	2 43	3 18
6 30	2 11	2 23	2 40	3 11
7 10	2 07	2 18	2 32	2 55

Fig. 122

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

27 December 1973
Nautical Almanac

Moon ^d₄
Age 2.4

☉ Sun				Planet				P. P.		☾ Moon Tr. ^{h m} _{14 13}				P. P.											
U	E _☉	d	d. P. P.	U	E _P	d	E _P d	U	E _☾	d	E _☾ d	U	E _☾	d	E _☾ d										
0 11 59 10 223 20.7 0 00 0.0 1 11 59 07 223 20.5 10 0.0 2 11 59 05 223 20.3 20 0.0 3 11 59 02 223 20.1 30 0.1 4 11 59 00 223 19.9 40 0.1 10 11 58 57 223 19.7 0 50 0.1 12 11 58 55 223 19.4 1 00 0.1 14 11 58 53 223 19.2 10 0.1 16 11 58 50 223 19.0 20 0.1 18 11 58 48 223 18.8 30 0.2 20 11 58 45 223 18.6 40 0.2 22 11 58 43 223 18.3 1 50 0.2 24 11 58 40 223 18.1 2 00 0.2				♀ Venus Tr. ^{h m} _{14 28} 0 9 30 27 517 26.1 0 00 0.0 2 9 30 42 517 24.8 10 1 0.1 4 9 30 57 517 23.5 20 3 0.2 6 9 31 13 517 22.1 30 4 0.3 8 9 31 28 517 20.8 40 5 0.4 10 9 31 44 517 19.5 0 50 7 0.5 12 9 31 59 517 18.2 1 00 8 0.7 14 9 32 15 517 16.9 10 9 0.8 16 9 32 31 517 15.6 20 10 0.9 18 9 32 47 517 14.3 30 12 1.0 20 9 33 02 517 13.0 40 13 1.1 22 9 33 18 517 11.7 1 50 14 1.2 24 9 33 34 517 10.4 2 00 16 1.3				♂ Mars Tr. ^{h m} _{19 30} 0 4 28 00 112 44.5 0 00 0.0 2 4 28 14 112 45.2 10 1 0.1 4 4 28 27 112 45.9 20 2 0.1 6 4 28 41 112 46.5 30 3 0.2 8 4 28 55 112 47.2 40 5 0.2 10 4 29 08 112 47.9 0 50 6 0.3 12 4 29 22 112 48.5 1 00 7 0.3 14 4 29 35 112 49.2 10 8 0.4 16 4 29 49 112 49.9 20 9 0.4 18 4 30 02 112 50.5 30 10 0.5 20 4 30 16 112 51.2 40 11 0.6 22 4 30 29 112 51.9 1 50 12 0.6 24 4 30 43 112 52.5 2 00 14 0.7		♃ Jupiter Tr. ^{h m} _{14 41} 0 9 17 16 517 31.4 0 00 0.0 2 9 17 31 517 31.1 10 1 0.0 4 9 17 46 517 30.8 20 3 0.1 6 9 18 02 517 30.5 30 4 0.1 8 9 18 17 517 30.2 40 5 0.1 10 9 18 33 517 29.9 0 50 6 0.1 12 9 18 48 517 29.6 1 00 6 0.2 14 9 19 04 517 29.2 10 9 0.2 16 9 19 19 517 28.9 20 10 0.2 18 9 19 35 517 28.6 30 12 0.2 20 9 19 50 517 28.3 40 13 0.3 22 9 20 05 517 28.0 1 50 14 0.3 24 9 20 21 517 27.7 2 00 15 0.3				♄ Saturn Tr. ^{h m} _{23 39} 0 0 17 14 222 23.4 0 00 0.0 2 0 17 36 222 23.4 10 2 0.0 4 0 17 57 222 23.4 20 4 0.0 6 0 18 19 222 23.4 30 5 0.0 8 0 18 40 222 23.4 40 7 0.0 10 0 19 02 222 23.4 0 50 9 0.0 12 0 19 23 222 23.4 1 00 11 0.0 14 0 19 44 222 23.5 10 13 0.0 16 0 20 06 222 23.5 20 14 0.0 18 0 20 27 222 23.5 30 16 0.0 20 0 20 49 222 23.5 40 18 0.0 22 0 21 10 222 23.5 1 50 20 0.0 24 0 21 32 222 23.5 2 00 21 0.0				☾ Moon Tr. ^{h m} _{14 13} 0 10 12 31 517 16.1 1 2 0.1 1 10 11 37 517 11.9 2 4 0.3 2 10 10 43 517 07.6 3 5 0.4 3 10 09 48 517 03.3 4 7 0.6 4 10 08 54 516 58.9 5 9 0.7 5 10 08 00 516 54.6 6 11 0.9 6 10 07 06 516 50.2 7 13 1.0 7 10 06 12 516 45.9 8 14 1.2 8 10 05 17 516 41.5 9 16 1.3 9 10 04 23 516 37.0 10 18 1.5 10 10 03 29 516 32.6 11 20 1.6 11 10 02 35 516 28.2 12 22 1.8 12 10 01 41 516 23.7 13 23 1.9 13 10 00 48 516 19.2 14 25 2.1 14 9 59 54 516 14.7 15 27 2.2 15 9 59 00 516 10.2 16 29 2.4 16 9 58 06 516 05.7 17 31 2.5 17 9 57 12 516 01.1 18 32 2.7 18 9 56 19 515 56.5 19 34 2.8 19 9 55 25 515 52.0 20 36 3.0 20 9 54 32 515 47.4 21 38 3.1 21 9 53 38 515 42.7 22 40 3.1 22 9 52 45 515 38.1 23 43 3.1 23 9 51 51 515 33.4 24 45 3.2 24 9 50 58 515 28.8 25 47 3.3 25 9 50 04 515 24.1 26 49 3.4 26 9 49 11 515 19.4 27 50 4.2 27 9 48 18 515 14.7 28 52 4.3 28 9 47 24 515 09.9 29 54 4.5 29 9 46 31 515 05.2 30 54 4.5 30 9 45 38 515 00.4 1 2 0.2 31 9 44 45 514 55.7 1 2 0.2 32 9 43 52 514 50.9 2 4 0.3 33 9 42 58 514 46.0 3 5 0.5 34 9 42 05 514 41.2 4 7 0.6 35 9 41 12 514 36.4 5 9 0.8 36 9 40 19 514 31.5 6 11 1.0 37 9 39 26 514 26.8 7 12 1.1 38 9 38 34 514 21.8 8 14 1.3 39 9 37 41 514 16.9 9 16 1.5 40 9 36 48 514 11.9 10 18 1.6 41 9 35 55 514 07.0 11 19 1.8 42 9 35 02 514 02.1 12 21 1.9 43 9 34 10 513 57.1 13 23 2.1 44 9 33 17 513 52.1 14 25 2.3 45 9 32 24 513 47.1 15 27 2.4 46 9 31 32 513 42.1 16 29 2.4 47 9 30 39 513 37.1 17 31 2.5 48 9 29 46 513 32.1 18 33 2.6 49 9 28 54 513 27.1 19 35 2.7 50 9 28 01 513 22.1 20 37 2.8 51 9 27 09 513 17.1 21 39 2.9 52 9 26 16 513 12.1 22 41 3.0 53 9 25 24 513 07.1 23 43 3.1 54 9 24 32 513 02.1 24 45 3.2 55 9 23 40 512 57.1 25 47 3.3 56 9 22 48 512 52.1 26 49 3.4 57 9 21 56 512 47.1 27 51 3.5 58 9 21 04 512 42.1 28 53 3.6 59 9 20 12 512 37.1 29 55 3.7 60 9 19 20 512 32.1 30 57 3.8				Planet RA. d Mag. H.P.S.D. ♃ 20 51 517 26 -4.4 0.4 23 ♄ 1 53 112 45 -0.4 0.3 8 ♀ 21 04 517 31 -1.6 0.0 16 ♁ 6 04 222 23 -0.3 0.0 9 ♀ 17 49 524 19 -0.6 0.1 2			

Fig. 123

Extracted from the NAUTICAL ALMANAC, MARITIME SAFETY AGENCY, JAPAN.

When we are observing compass bearing of the sun's amplitude at sea, we have to check the time simultaneously. By this checked time, we can calculate the declination (d) of the sun at universal time came using the local time.

Latitude (ℓ) is given by our D.R.P. after obtaining the value of ℓ and d, we can calculate the rising or setting azimuth by the formula:

$$\sin \text{amplitude} = \frac{\sin d}{\cos \ell}$$

to check our compass error

Solution of problem on page

Ship's Time 6/7/56	06h50m00s	
L. in T.	<u>09 00 00</u>	⊖
U. 5/7/56	21 50 00	
Chro. time	10h21m50s	
Chro. E	<u>29 00</u>	⊖
Corrected chro. time	09 52 50	
	<u>12</u>	⊕
U. 5/7/56	21 52 50	
R.	18 51 51	(By nautical almanac 5/7/56)
P.P. (E*)	<u>3 36</u>	⊕ (see page p.p. for E*)
G.sin. T.	40 48 17	
	<u>24</u>	⊖
G.sin. T.	16 48 17	
L. in T.	<u>9 00 00</u>	⊕
L. sin T.	25 48 17	
	<u>24</u>	⊖
L. sin T.	01 48 17	

		K	D	H	
Z	57°E	264		3187	
a	50°	3076 +	2884		
ℓ	+ 34°N	3340			
K	+ 25		43	2626	
ℓ+K	+ 59		2933 +	288 ⊕	
			5860	6101 →	h_E 3 ^h 28 ^m
			↓		L. sin T. 1 49 ⊕
			<u>d = 46°N</u>		R.A. <u>5^h17^m</u>

$d = 46^\circ\text{N}, \text{R.A.} = 5^{\text{h}}17^{\text{m}},$

By the table "Position of navigation stars" on page , this star's proper name must be Capella.

Ans. Capella

Solution of problem on page

L.A.T. (4/8)	12 ^h 00 ^m 00 ^s
L. in T.	<u>00 29 00</u> ⊕
G.A.T. (4/8)	12 29 00
E.T.	⊖ 00 05 59 ⊖ (Note, E.T. = E - 12 ^h)
U. (4/8)	12 34 59 → d = 17°10'6" N
	↓
	12 ^h d = 17°10.9' N
P.P. of d (34 ^m 59 ^s)	= <u>0.3</u> ⊖
d for 12 ^h 34 ^m 59 ^s	= 17°10'6" N

Sex Alt.	66°05'5			
I.E.	02'4	⊕		
Obs. Alt.	66°07'9			
Corr. 1	9'2	⊕		
	66°17'1			
Corr. 2	0'1	⊕		
	66°17'2			
Corr. 3	0'2	⊕		
True Alt.	66°17'4			
	90°00'0			
Zu	23°42'6 S			
d	17°10'6 N	⊖		
λ	6°32'0 S			
Ans. <u>Latitude 6°32'0 S</u>				

Solution of problem on page
 Ans. Capelin
 By the table "Position of navigation stars" on page
 this star, a proper name must be labelled.
 d = 15° 00' N, R.A. = 217° 15' W
 L.A.T. (W/B) 15 00
 L. in T. 00 29 00 ⊕
 O.A.T. (W/B) 15 29 00
 S.T. 00 02 29 ⊖ (Note, E.T. = E - 15p)
 H. (W/B) 15 34 29 - d = 17° 10'6 N
 15p d = 17° 10'6 N
 P.P. of d (3mags) = 0.3 ⊖
 d for 15mags = 17° 10'6 N

3. Time

THE CONCEPT OF TIME

Time is the most important factor in navigation. Any navigation such as celestial, coastal, radio or by dead reckoning is based on the measurement and use of time.

For time measurement, the diurnal motion of celestial bodies such as the sun, the moon, the stars and the celestial point of reference should be observed. There are three major time measurements.

They are:

1. Solar time
2. Sidereal time
3. Lunar time

The units of time are: year, month, week, day, hour, minute and second.

(1) Solar time

1) Apparent Solar Time (Apparent Time, A.T.)

The time when the sun transits the lower branch of a certain location is called apparent Midnight, and when it transits the upper branch it is called Apparent Noon (A.N.).

The sun as mentioned above is the actual sun and is called Apparent Sun (A.S.). The interval from one Apparent Midnight to the next Apparent Midnight is called Apparent Solar Day.

$$A.T. = 12h + h - (24)$$

Apparent Time at Greenwich is called Greenwich Apparent Time (G.A.T.) and Apparent Time at a given location is called Local Apparent Time (L.A.T.).

In terms of navigation, Local Apparent Time is sometimes called Ship's Apparent Time (S.A.T.).

2) Mean Solar Time or Mean Time (M.T.)

Apparent Solar Time (Apparent Time, or A.T.) is not regular because the apparent rotation of the sun around the earth is not at a constant velocity since the apparent path of the sun is along the ecliptic. The included angle between the plane of the celestial equator and the ecliptic is about $23^{\circ}27'$.

To solve this irregularity and other difficulties, Mean Solar Time is based on an imaginary sun that has an hour circle moving along the celestial equator at a constant rate. Mean Solar Time is nearly equal to the average Apparent Solar Time.

Chronometers on board a ship indicate Mean Solar Time and are used for the coordinates of celestial bodies in nautical almanacs.

The time when Mean Sun transits the lower branch of the meridian at a certain location is called Mean Midnight, and the time when Mean Sun transits the upper branch of the meridian at a certain location is called Mean Noon. The interval or length of time from the Mean Midnight to the next Mean Midnight is called Mean Solar Day and,

$$\begin{aligned} \text{M.T.} &= 12\text{h} + \text{H.A.M.S.} - (24\text{h}) \\ (\text{H.A.M.S.} &= \text{Hour Angle of Mean Sun}) \end{aligned}$$

Mean Time (M.T.) is also sometimes called Civil Time and the day introduced by Mean Time is called Civil Day. Greenwich Mean Time (G.M.T.) or Universal Time (U.T.) is Mean Time at Greenwich in the United Kingdom. Local Mean Time (L.M.T.) is Mean Time at a given location and is sometimes called ship's Mean Time (S.M.T.).

3) Equation of Time (E.T.)

The difference between Apparent Time and Mean Time is called equation of Time, as follows:

$$E.T. = A.T. - M.T.$$

This has the same value as the difference between the Right Ascension of Mean Sun (R.A.M.S.) and the Right Ascension of Apparent Sun (R.A.A.S.);

(2) Sidereal Time (Sid. T.)

The hour angle of the Vernal Equinox is called Sidereal Time. When the Vernal Equinox transits the upper branch of an observer's meridian it is zero hour of Sidereal Time at the observer's location, and the time when the Vernal Equinox's hour angle is one hour it is called one hour of Sidereal Time. Sidereal Time shows the position of the stars and their daily movement westward, which is almost one degree every night.

Sidereal time is not exactly constant in rate because of the earth's rotation. Time based on the average rate is called Mean Sidereal Time. Greenwich Sidereal Time (G.S.T.) uses the meridian of Greenwich as its terrestrial reference and Local Sidereal Time (L.S.T.) or Ship's Sidereal Time uses the observer's meridian as its reference. Some timepieces are adjusted to keep Sidereal Time. If they are set to G.S.T., they permit the navigator to read the G.H.A., which is G.S.T. expressed in units of arc, directly from the timepiece at the instant of making a star observation, obviating from the almanac.

Sidereal Time = Hour angle of Vernal Equinox = Right Ascension of meridian

$$\text{Sid. T.} = h = \text{R.A. meri}$$

(3) Lunar Time

1) The hour angle of the moon is called Lunar Time. When the moon transits the upper branch of the meridian of a place (hour angle - zero), Lunar Time is zero. When the hour angle of the moon becomes one hour, Lunar Time is one hour. The interval between the moon's transit of the upper branch of the meridian and the next transit of the upper branch is called Lunar Day. The average value of a Lunar Day is approximately 24 hours 50 minutes and 28 seconds because the moon's diurnal motion is irregular.

2) Age of the moon

The moon's age is calculated on the basis of the mean solar day starting from the new moon (zero day to 29th day of the age). The new moon rises and sets with the sun and the full moon rises at almost the same time as the sun sets, and it sets when the sun rises. The phases of the moon are expressed as follows:

1. New moon → 2. Crescent → 3. First quarter → 4. Gibbous
 5. Full moon → 6. Gibbous → 7. Last quarter → 8. Crescent (new moon).
- So if the age of the moon is given, it is possible to imagine its phase, but its 15th age does not always indicate a full moon. (see Fig. 124 & 125).

Ref. Lunar Time and phase are very important in regard to tide and fisheries.

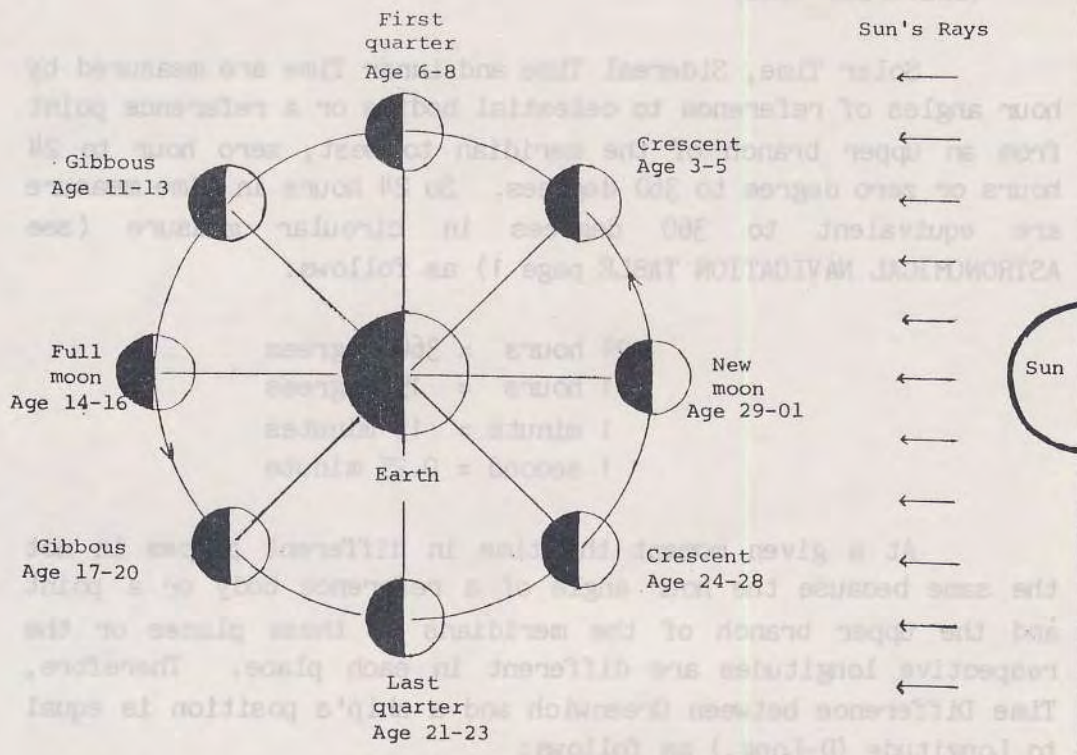


Fig. 124

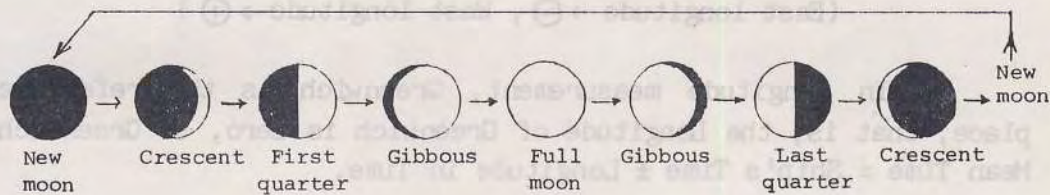


Fig. 125 The eight phases of the moon

(4) Conversion of Local Mean Time to Greenwich Mean Time
(Universal Time)

Solar Time, Sidereal Time and Lunar Time are measured by hour angles of reference to celestial bodies or a reference point from an upper branch of the meridian to west, zero hour to 24 hours or zero degree to 360 degrees. So 24 hours in time measure are equivalent to 360 degrees in circular measure (see ASTRONOMICAL NAVIGATION TABLE page 1) as follows:

24 hours . = 360 degrees
1 hours = 15 degrees
1 minute = 15 minutes
1 second = 0.25 minute

At a given moment the time in different places is not the same because the hour angle of a reference body or a point and the upper branch of the meridians at these places or the respective longitudes are different in each place. Therefore, Time Difference between Greenwich and a ship's position is equal to Longitude (D-Long.) as follows:

Greenwich Meantime = Ship's Time \pm D-Long. in Time
(East longitude \rightarrow \ominus , West longitude \rightarrow \oplus)

In longitude measurement, Greenwich is the reference place, that is, the Longitude of Greenwich is zero, so Greenwich Mean Time = Ship's Time \pm Longitude in Time.

G.M.T. = Ship's Time \pm L. in Time
(East longitude \rightarrow \ominus , West longitude \rightarrow \oplus)

For conversion of Ship's Apparent Time (S.A.T.) to Greenwich Apparent Time (G.A.T.), the same formula can be applied as follows:

$$\text{G.A.T.} = \text{S.A.T.} \pm \text{L. in Time}$$

(5) Time Zone

At sea, central longitudes are selected for ship's time. These longitudes are exactly multiplied by 15 degrees each, then there are 24 standard longitudes, each of one hour and the boundaries of longitude of each zone are 7 and 1/2 degrees on each side as shown in Figure 126. When a ship is in a Time Zone, it is convenient and recommendable to use the time in that zone on board. But in case of contact or communication among ships, it is advisable to use Greenwich Mean Time as a common time and, in the case of communication with offices of ship owners or agencies, the standard time of the place where they are located is generally used.

Questions

What zone time should be kept on ship in the following longitudes:

- 1) 55 degrees west?
- 2) 90 degrees east?
- 3) 120 degrees east?
- 4) 175 degrees west?
- 5) 173 degrees east?
- 6) 170 degrees west?

Answers

- 1) +3,
- 2) -6,
- 3) -8,
- 4) +12,
- 5) -12,
- 6) +11 (see Fig. 126)

The positive sign + or negative sign - of Zone means that Ship's Mean Time plus or minus Zone equals Greenwich Mean Time.

Questions

What zone time should be kept on ship in the following

longitudes:

- 1) 55 degrees west?
- 2) 90 degrees east?
- 3) 150 degrees east?
- 4) 175 degrees west?
- 5) 175 degrees east?
- 6) 170 degrees west?

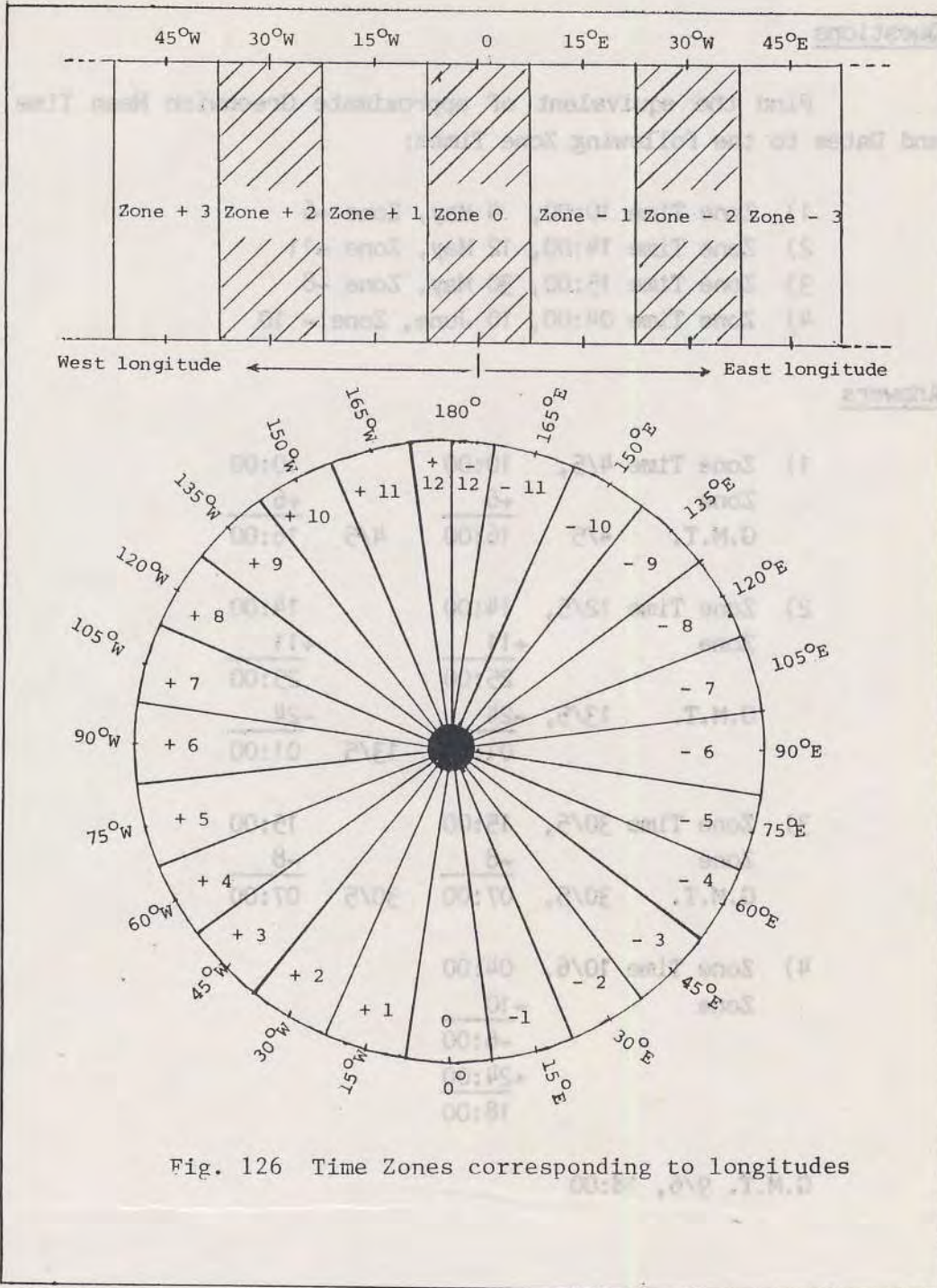


Fig. 126 Time Zones corresponding to longitudes

Questions

Find the equivalent of approximate Greenwich Mean Time and Dates to the following Zone Times:

- 1) Zone Time 10:00, 4 May, Zone +6
- 2) Zone Time 14:00, 12 May, Zone +11
- 3) Zone Time 15:00, 30 May, Zone -8
- 4) Zone Time 04:00, 10 June, Zone - 10

Answers

1) Zone Time	4/5,	10:00		10:00
Zone		<u>+6</u>		<u>+6</u>
G.M.T.	4/5	16:00	4/5	16:00

2) Zone Time	12/5,	14:00		14:00
Zone		<u>+11</u>		<u>+11</u>
		25:00		25:00
G.M.T.	13/5,	<u>-24</u>		<u>-24</u>
		01:00	13/5	01:00

3) Zone Time	30/5,	15:00		15:00
Zone		<u>-8</u>		<u>-8</u>
G.M.T.	30/5,	07:00	30/5	07:00

4) Zone Time	10/6,	04:00		
Zone		<u>-10</u>		
		-6:00		
		<u>+24:00</u>		
		18:00		

G.M.T. 9/6, 18:00

6) Chronometer Time and chronometer error

For calculations in celestial navigation, it is essential to know the correct Greenwich Mean Time because in the nautical almanac, the elementary position of celestial bodies are described by G.M.T. A ship's chronometer must therefore be set by G.M.T. chronometer error is the difference between the ship's chronometer time and G.M.T. as shown below

$$\text{G.M.T.} - \text{Chronometer Time} = \text{Chronometer error}$$

Question

Ship's Time 6/8/85,	18h 20m 00s
Long. in Time (E-, W+)	<u>3 37 44 +</u>
Approx. G.M.T.	21 57 44
Chronometer Time	09h 54m 18s
Chronometer error	<u>02 14</u>

	12+
G.M.T. 6/8/85	21 56 32
6/8/85	21h 56m 32s

Answer

Chronometer error is measured by means of the radio time signal. It should be recorded as F₁ - (fast) or S₁ + (slow) accordingly. Navigation should check the chronometer error everyday and record the daily rate in the Chronometer Error and Rate Book. Sample entries in such a book are shown in Fig. 127.

Date				Error Relative to Radio Signal				
	Ship's Time	Chro. Time	Radio Signal Time	+ -	Minutes	Seconds	+ -	Successive Daily Rate
1985 August								
1	12-00-00	09-00-03.0	09-00-00	-	0	3.0	+	
2	12-00-00	09-00-04.5	09-00-00	-	0	4.5	+	1.5 ^s
3	12-00-00	09-00-06.0	09-00-00	-	0	6.0	+	1.5
4	12-00-00	08-00-07.5	08-00-00	-	0	7.5	+	1.5
5	12-00-00	08-00-09.0	08-00-00	-	0	9.0	+	1.5
6	12-00-00	08-00-10.5	08-00-00	-	0	10.5	+	1.5
7	12-00-00	07-00-12.5	07-00-00	-	0	12.5	+	2.0
8	12-00-00	07-00-14.5	07-00-00	-	0	14.5	+	2.0
9	12-00-00	07-00-16.5	07-00-00	-	0	16.5	+	2.0

(Fig. 127)

Exercise

Fix by stars, Altair and Vega.

1. British method (Sight Reduction Table)
2. Japanese method (Astronomical Navigation Table)
3. By formulae

A navigator observed the altitude of stars, Altair and Vega, when ship's time was 05h 17m, 13 June 1985, in D.R.P. 17-11.3 N, 118-23.4 E, on the way to Japan from Bangkok:

Altair: Sex. Alt. 51° - 17.5, Chronometer time
09h 08m 00s.

Vega : Sex. Alt. 35° - 30.6 Chronometer time
09h 10m 30s.

Ref. Chronometer error and Index error were nil. Ship's speed was 10 knots. Set course was on 042° . Height of eye was 22 feet.

Question : Fix position by:

1. British method (Sight Reduction Table)
2. Japanese method (Astronomical Navigation Table)
3. By formulae.

Top of Star by Sight Reduction Table (Pub. No. 229) (U.K., U.S.A.)

Date	13/6/85	Z.T.	8 ^h	Ship's Time	05 ^h 17 ^m	G.E.	0 ^m 0 ^s
Co.	042°	Speed	10.0 Kt.	22	IE	0	

D.R.P.	17-11.3	(N) S
Assumed Latitude	17°	(N) S
Body	Altair	
Zone Time	13	h m s
Ship's Time	05-17-00	
Long. in time or Z.T.	07-53-34	(E) W (+)
Approx. U (GMT)	13/6	h m s
If required	24	
Approx. U (GMT)	13/6	h m s
Chronometer Time	09-08-00	h m s
Chronometer error	0	m s
Corrected Chro. Time	09-08-00	h m s
If approx. U (GMT) is in afternoon	12	
U (GMT)	12/Sun.	h m s
Almanac Table ARIES GHA (21)	216-07.5	P. 249
Incre.	08 ^m 00 ^s	P. 251
Star SIA	62-28.8	P. 249
GHA (h m s)	280 36.6	
Assumed Longitude	118-23.4	(E) W-
If required	360° (-)	
LHA	39	
Table LHA	39	
Dec.	8° 49.6	(N) S
Table Dec.	8°	(N) S
Dec. diff/Dec. incre	49.6	
Table alt.	50-57.3	P. 255
Int. Alt. diff.	14.2	(+) (-)
Corr. Table Alt. (Hc)	51-11.5	

Sex. Alt.	51-17.5	
I.E.	0.0	+ -
Obs. Alt.	51-17.5	
Dip (H.E.)	4.6	-
App. Alt.	51-12.9	
App. Alt. Corr.	0.8	-
True Alt. (Ht)	51-12.1	
Corr. Table Alt. (Hc)	51-11.5	-
Intercept	0.6	(+) (-) to any

Sight Reduction Table	
Table Z	98.4
diff. 1.2	= 97.2
Zn (Azimuth)	360° - Z = 262.8 (11A < 180°)
✓ In north latitude	

Table Dec	Table Z	
8°	98.4	P. 257
9°	96.7	
1.5	→ I.T. diff. 1.2	
Sight Reduction Table		
Table Z	diff.	=
Zn (Azimuth)	180° - Z =	11A > 180°
	180° + Z =	11A < 180°
In South latitude		

Table alt.	50-57.3	P. 255
Int. Alt. diff.	14.2	(+) (-)
Corr. Table Alt. (Hc)	51-11.5	

Sight Reduction Table	
Table alt.	50-57.3
Int. Alt. diff.	14.2
Corr. Table Alt. (Hc)	51-11.5

LoP of Star by Sight Reduction Table (Pub. No. 229) (U.K., U.S.A.)

Date	13/6/85	Z.T.	8 ^h +	Ship's Time	05 ^h 17 ^m	C.E.	0 ^m 0 ^s +
Co.	042°	Speed	10.0 Kt.	DR	22 M	IE	0' +

D.R.P.	17-11.3	(N) S
	118-23.4	(E) W
Assumed Latitude	17	(N) S
Body	Vega.	
Zone Time	13	
Ship's Time	05-17-00	
Long. in line or Z.T.	07-53-34	E(-) W(+)
Approx. U (GHT)	12/6	
Date	21-23-26	
If required	24	
Approx. U (GHT)	12/6	
Date	21-23-26	
Chronometer Time	09-10-30	
Chronometer error	0	
Corrected Chro. Time	09-10-30	
If approx. U (GHT) is in afternoon	12	
U (GHT)	12/Jun.	
Date	21-10-30	

Sex. Alt.	35-30.6	
I.E.	0.0	+ -
Obs. Alt.	35-30.6	
Dip (H.E.)	4.6	-
App. Alt.	35-26.0	
App. Alt. Corr.	1.4	-
True Alt. (Ht)	35-24.6	
Corr. Table Alt. (Ht)	35-19.3	-
Intercept	5.3(-)	to my

Sight Reduction Table

Table Z $\frac{0.9}{0.9} = 54.2$

Zn (Azimuth) $360-Z = 305.8$ $114 < 180$

In north latitude

Almanac Table ARIES (21 ^h)	216-07.5	
Incr. (10 ^m 30 ^s)	2-37.9	
Star SIA	80-53.1	+
GIA (21 ^h 10 ^m 30 ^s)	299 38.5	
Assumed Longitude	118 21.5	(E) W
	418 0.0	
If required	360° (-)	
LHA	58	

Dec	38-46.0	(N) S
Table Dec	38	
Table Z	53.1	
	53.9(-)	
	1.2	→ I.T. → diff

Sight Reduction Table

Table Z = $\frac{+}{-} \text{diff.} = 0$

Zn (Azimuth) $180-Z = 180$ $114 > 180$

$180+Z = 180$ $114 < 180$

In South latitude

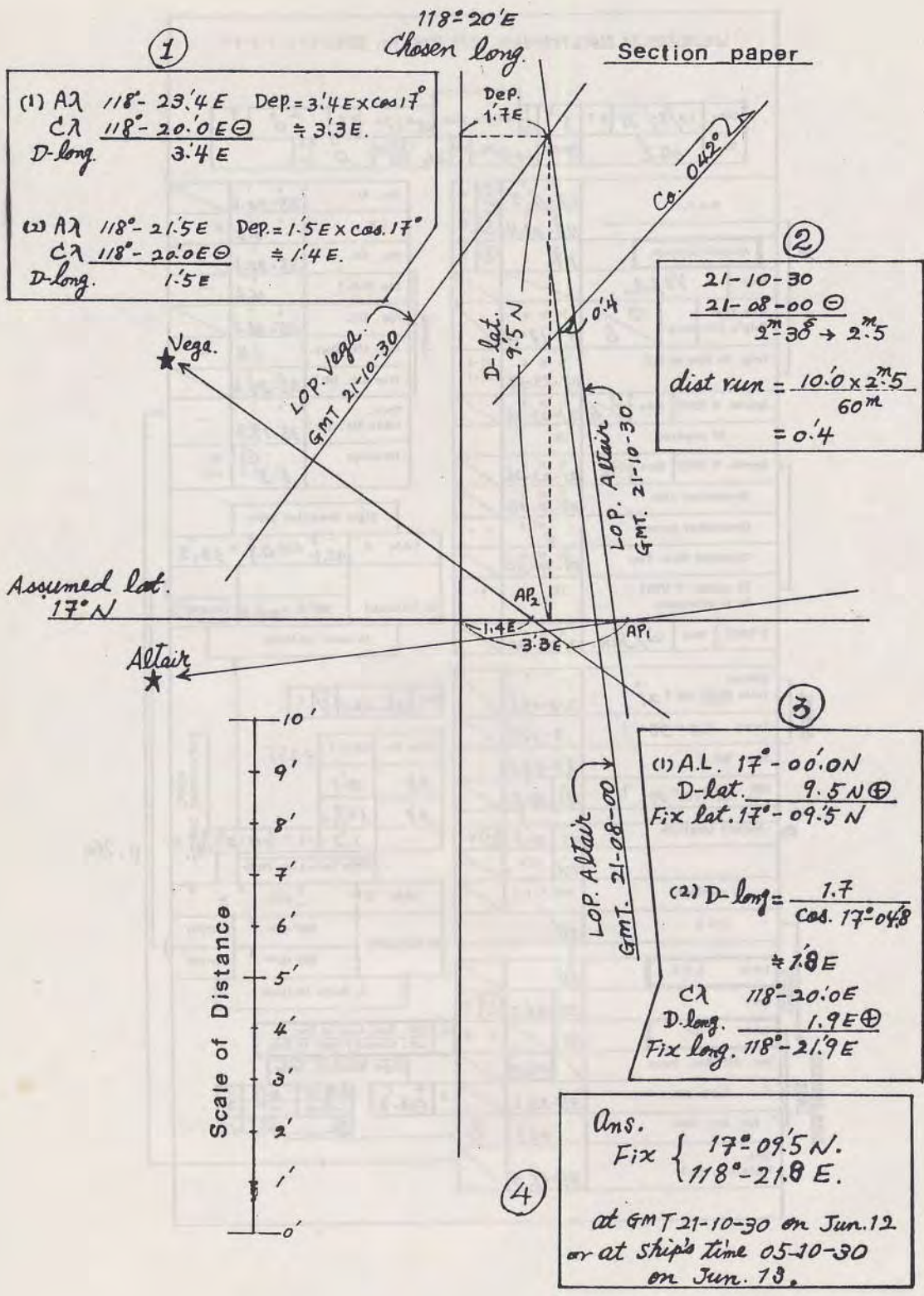
Table LHA	58	
Dec.	38 46.0	(N) S
Table Dec.	38	N S
Dec. diff/Dec. Incr	46.0	
Table alt.	35-24.2	
lst. Alt. diff.	04.9	+
Corr. Table Alt. (Ht)	35-19.3	

Lat. Same name as Dec.
Lat. Contrary name to Dec.

Sight Reduction Table

d	+	6.3	0.3 → 4.9
	+	6.3	→ 4.9

p. 264



①

(1) $A\lambda$ $118^\circ-23.4'E$ $Dep. = 3.4E \times \cos 17^\circ$
 $C\lambda$ $118^\circ-20.0'E \ominus \approx 3.3E$
 $D-long.$ $3.4E$

(2) $A\lambda$ $118^\circ-21.5'E$ $Dep. = 1.5E \times \cos 17^\circ$
 $C\lambda$ $118^\circ-20.0'E \ominus \approx 1.4E$
 $D-long.$ $1.5E$

②

$21-10-30$
 $21-08-00 \ominus$
 $\hline 2^m-30^s \rightarrow 2^m.5$

$dist\ run = \frac{10.0 \times 2^m.5}{60^m}$
 $= 0.4$

③

(1) $A.L.$ $17^\circ-00.0'N$
 $D-lat.$ $9.5'N \oplus$
 $Fix\ lat.$ $17^\circ-09.5'N$

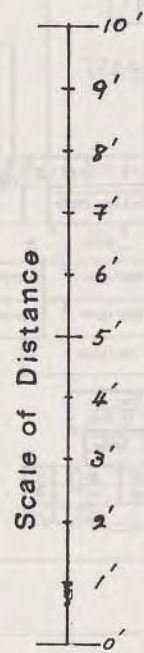
(2) $D-long = \frac{1.7}{\cos 17^\circ 04.8}$
 $\approx 1.8E$

$C\lambda$ $118^\circ-20.0'E$
 $D-long.$ $1.9E \oplus$
 $Fix\ long.$ $118^\circ-21.9'E$

④

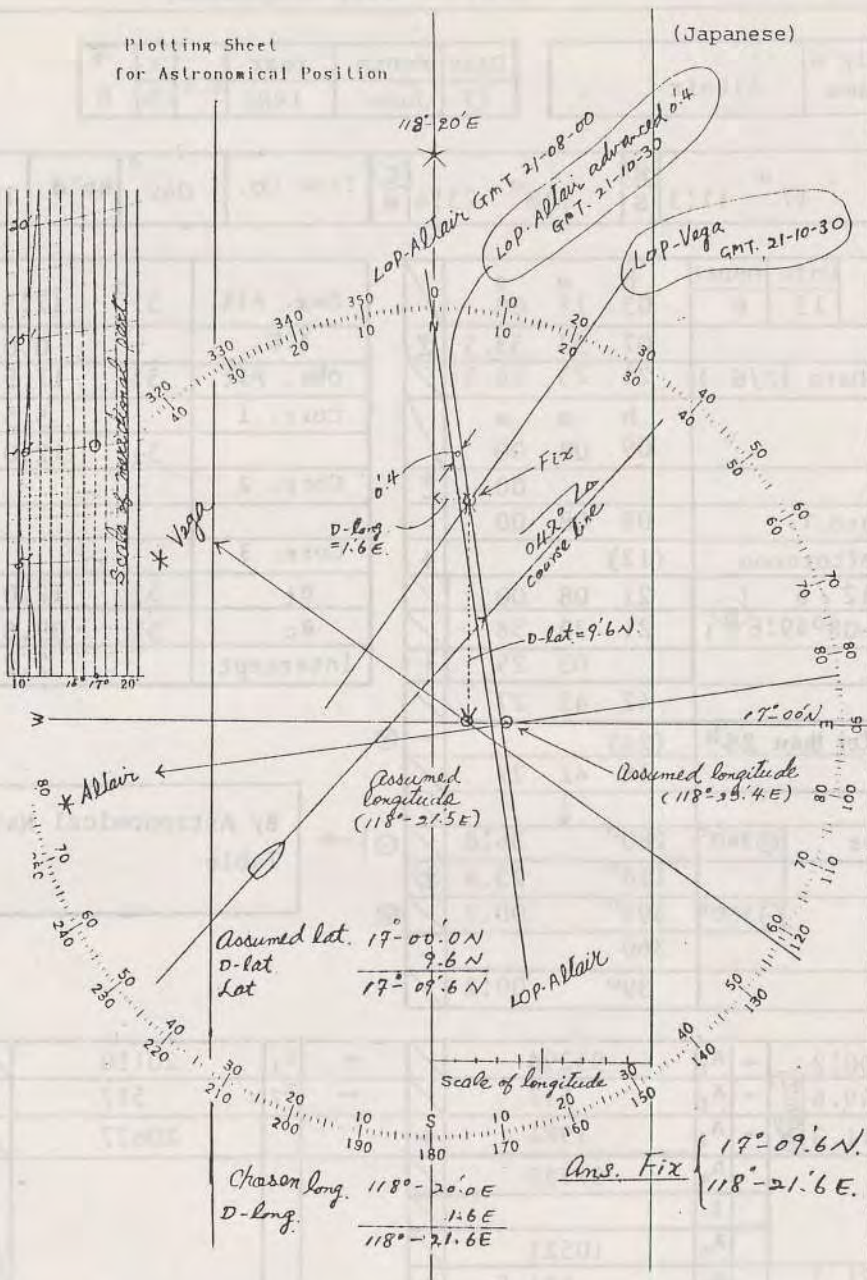
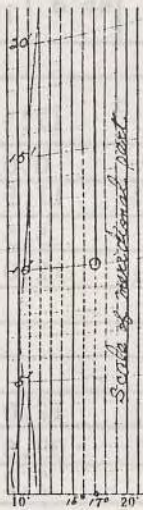
Ans.
 $Fix \left\{ \begin{array}{l} 17^\circ-09.5'N. \\ 118^\circ-21.8'E. \end{array} \right.$

at GMT 21-10-30 on Jun. 12
 or at Ship's time 05-10-30
 on Jun. 13.



Plotting Sheet
for Astronomical Position

(Japanese)



1. ...
2. ...
3. ...
4. ...

Line of Position of a Celestial Body (Japanese)

Body's name	Altair
-------------	--------

Date	Month	Year	Z.T.	+	h
13	June	1985	⊖		8

D.R.P.	17° 11'3"	^N / _S	118° 23'4"	^E / _W	True Co.	042°	sp'd	10.0	kt.
--------	-----------	-----------------------------	------------	-----------------------------	----------	------	------	------	-----

Ship's Time	Date	Month	h	m	s	
	13	6	05	17	00	
*1 → L. in T.			07	53	33.5	+
Approx. U. (Date 12/6)			21	23	26.5	⊖
Chro. T.			h	m	s	
			09	08	00	
Chro. E.					00	+
Corrected chro. T.			09	08	00	
Morning or Afternoon			(12)			+
U. (Date 12/6)			21	08	00	
E ⊙ * P (d = 08° 49' 6" S)			21	30	58	
P.P				03	29	+
h _g			42	42	27	
If h _g is greater than 24h			(24)			⊖
h _a in hours			18	42	27	
h _a in degrees	⊕360°		280°		36'8"	⊖
*2 → Long.			118°		23.4	⊕
	⊖360°		399°		00.2	⊖
			360			-
h			39°		00'2"	

Sex. Alt.	51°	17'5"	
I.E.		0.0	+
Obs. Alt	51	17.5	
Corr. 1		5.5	⊖
	51	12.0	
Corr. 2			+
Corr. 3			+
a _t	51	12.0	
a _c	51	09.8	-
Intercept		2.2	⊕

By Astronomical Navigation Table

h	39°	00'2"	→	A ₁	95294		→	Z ₁	20110	
d	08	49.6	→	A ₂	517		→	Z ₂	517	+
l	17	11.3	→	A ₃	1984	+			20627	
				A ₄	97795					
				A ₅	10521					
*3 → l ± d	08	21.7		A ₆	531.5	+				
				A ₇	11052.5		→	Z ₃	20266	-
				l				Z ₄	361	
				a _c	51°	09'8"		l	^N / _S	^E / _W
								Z _c	(S) 82° 37'5"	(W)

Ref.

1. Approx. U = Ship's Time ± L. in T. (E - long → ⊖, W - long. → ⊕)
2. h = h_a ± L (E - long → ⊕, W - long → ⊖)
3. When l and d same name → l - d, contrary → l + d.
4. When h > 180° suffix of Z_c → E, h < 180° suffix of Z_c → W.

Line of Position of a Celestial Body (Japanese)

Body's name	Vega.
-------------	-------

Date	Month	Year	Z.T.	+	h
13	Jun.	1985		⊖	8

D.R.P.	17° 11!3	^(N) S	118° 23!4	^(E) W	True Co.	042°	sp'd	kt.
								10.0

*1 →	Ship's Time	Date	Month	h	m	s	/	
		13	6	05	17	00		
	L. in T.							±
	Approx. U. (Date 12/6)							/
								/
	Chro. T.							/
	Chro. E.							+
	Corrected chro.T.							-
	Morning or Afternoon	(12)						+
	U. (Date /)							/
	E⊙*⊕P (d = 38°46!0 ^(N) S)							/
	P.P							+

Sex. Alt.	35° 30!6	/
I.E.	0.0	±
Obs. Alt	35 30.6	/
Corr. 1	6.0	⊕
	35 24.6	/
Corr. 2	-	+
Corr. 3	-	+
At	35 24.6	/
Ac	35 24.5	-
Intercept	0.1	⊕

Almanac	h _G	43 58 34			/
	If h _G is greater than 24h	(24)			- ⊕
	h _G in hours	19 58 34			/
	h _G in degrees	⊕360°	299°	38!5	⊕ } →
*2 → Long.		118	23.4	⊕	
	⊖360°	418	01.9	⊕	
		360		-	
	h	58°	01.9	/	

By Astronomical Navigation Table

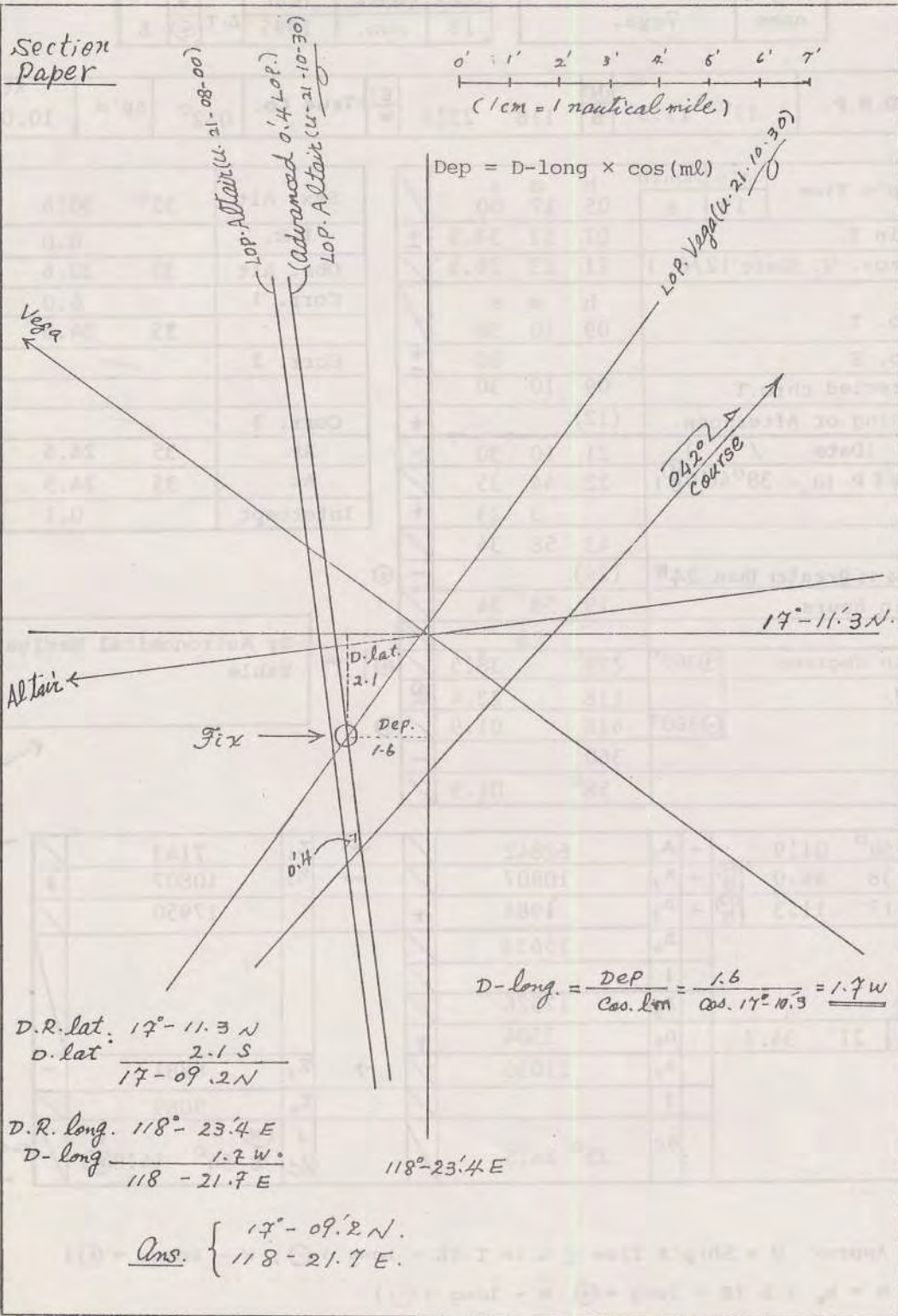
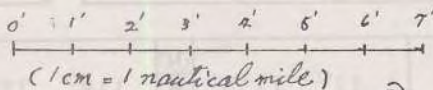
*3 →	h	58° 01!9	→ A ₁	62842	/	→ Z ₁	7143	/
	d	38 46.0	→ A ₂	10807	/	= Z ₂	10807	+
	l	17 11.3	→ A ₃	1984	+		17950	/
			A ₄	75633	/			/
			A ₅	17526	/			/
	l+d	21 34.7	A ₆	3504	+	→ Z ₃	8881	-
			A ₇	21030	/	→ Z ₄	9069	/
		d	35° 24!5	/	↓ Z _c	^(N) S 54° 14!8 ^(W)	← *4	

Ref.

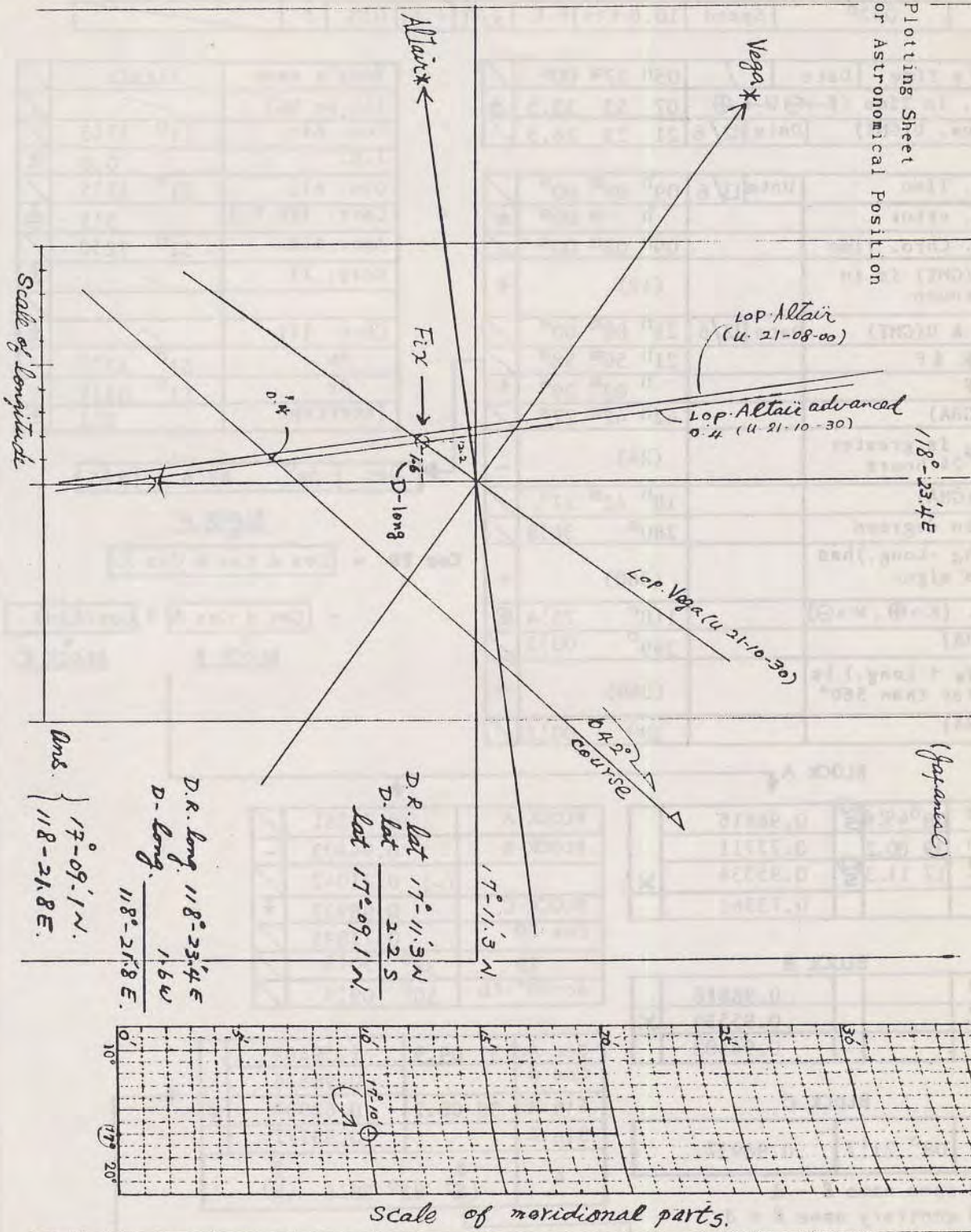
1. Approx. U = Ship's Time ± L. in T. (E - long → ⊖, W - long. → ⊕)
2. h = h_G ± L (E - long → ⊕, W - long → ⊖)
3. When l and d same name → l-d, contrary → l + d.
4. When h > 180° suffix of Z_c → E, h < 180° suffix of Z_c → W.

(Japanese)

Section Paper



Plotting Sheet
for Astronomical Position



LOP of Celestial Body → By formulae (C) (* P.)

	D.R.P.	17° 11'3"	(N)	S	118° 23'4"	(E)	W		
Date	13 Jun. '85	ZT	8 h 0	Ship's Time	05h 17m 00s	C.E	0m 0s	±	
Co.	042°	Speed	10.0 Kts	H.E	22 ft	I.E.	0!0	±	

Ship's Time	Date	/	05h 17m 00s	/
Long. in Time (E→⊖ W→⊕)			07 53 33.5	±
Approx. U(GMT)	Date	12/6	21 23 26.5	
Chro. Time	Date	13/6	09 ^h 08 ^m 00 ^s	/
Chro. error			h m 00 ^s	±
Corr. Chro. Time			09 ^h 08 ^m 00 ^s	/
If U(GMT) is in afternoon			(12)	+
Date & U(GMT)	Date	12/6	21 ^h 08 ^m 00 ^s	/
E O * P			21 ^h 50 ^m 58 ^s	/
P.P			h 03 ^m 29 ^s	+
h _G (GHA)			42 ^h 42 ^m 27 ^s	/
If h _G is greater than 24 hours			(24)	-
h _G (GHA)			18 ^h 42 ^m 27 ^s	/
h _G in degrees			280° 36!8	/
If (h _G - Long.) has "minus" sign.			(360)	+
Long. (E→⊕, W→⊖)			118° 25!4	⊕
h (LHA)			399° 00!2	/
If (h _G + Long.) is greater than 360°			(360)	-
h (LHA)			39° 00!2	/

Body's name	Altair	/
(LL or UL)		/
Sex. Alt.	51° 17!5	/
I.E.	0.0	±
Obs. Alt.	51° 17!5	/
Corr. I(H.E.)	5!5	⊕
App. Alt.	51° 12!0	/
Corr. II	-	±
Corr. III	-	±
At	51° 12!0	/
Ac	51° 09!9	-
Intercept	2!1	±

Dec. 08° 49!6 N S

BLOCK A

$$\text{Cos ZD} = \text{Cos } d \text{ Cos } h \text{ Cos } l$$

$$- \text{Cos } d \text{ Cos } l + \text{Cos}(l+d)$$

BLOCK B BLOCK C

BLOCK A

Cos d	08° 49!6 N S	0.98816	
Cos h	39 00.2	0.77711	
Cos l	17 11.3 N S	0.95534	X
		0.73361	

BLOCK A	0.73361	/
BLOCK B	0.94403	-
	(-) 0.21042	/
BLOCK C	0.98937	+
Cos ZD	0.77895	/
ZD	38° 50!1	/
Ac=90°-ZD	50° 09!9	/

BLOCK B

Cos d		0.98816	
Cos l		0.95534	X
		0.94403	

BLOCK C

Cos (l+d)	08° 21!7	0.98937	
-----------	----------	---------	--

Sec Ac	51 09.9	1.59469	
Cos d		0.98816	
Sin h	39 00.2	0.62937	X
Sin Z		0.99177	
Z	(S) 82° 38!6 (W)		

l & d same name l - d
 l & d contrary name l + d
 Prime Vertical
 $a = \sin^{-1} \left(\frac{\sin d}{\sin l} \right) = 31^{\circ} 16!9 < 51^{\circ} 09!9$
 Contrary name to latitude

h > 180° suffix E
 h < 180° suffix W
 $\text{Sin } Z = \sin^{-1} \left(\frac{\cos d \times \sin h}{\cos Ac} \right)$ or
 $\text{Sin } Z = \text{Sec } Ac \text{ Cos } d \text{ Sin } h$

LOP of Celestial Body → By formulae (⊙ ⊙ * P.)

	D.R.P.	17° 11.3' (N) S	118° 23.4' (E) W						
Date	13/Jun./'85	ZT	h ±	Ship's Time	05 ^h 17 ^m 00 ^s	C.E	m	s	±
Co.	042°	Speed	10.0 Kts	H.E	22 f.	I.E.	0!0	±	

Ship's Time	Date	13/6	05 ^h 17 ^m 00 ^s
Long. in Time (E→⊖ W→⊕)			07 53 33.5
Approx. U(GMT)	Date	12/6	21 23 26.5

Chro. Time	Date	13/6	09 ^h 10 ^m 30 ^s
Chro. error			h m s ±
Corr. Chro. Time			09 ^h 10 ^m 30 ^s
If U(GMT) is in afternoon		(12)	+
Date & U(GMT)	Date	12/6	21 ^h 10 ^m 30 ^s
E.O. * (P.)			22 ^h 44 ^m 35 ^s
P.P			h m s ±
h _G (GHA)			43 ^h 58 ^m 34 ^s
If h _G is greater than 24 hours		(24)	-
h _G (GHA)			19 ^h 58 ^m 34 ^s
h _G in degrees			299° 38!5
If (h _G - Long.) has "minus" sign		(360)	+
Long. (E→⊕, W→⊖)			118° 23!4
h (LHA)			418° 01!9
If (h _G + Long.) is greater than 360°		(360)	-
h (LHA)			58° 01!9

Body's name	Vega.
(LL or UL)	
Sex. Alt.	35° 30!6
I.E.	±
Obs. Alt.	35° 30!6
Corr. I(H.E.)	6.0
App. Alt.	35° 24.6
Corr. II	±
Corr. III	±
At	35° 24.6
Ac	35 24.6 -
Intercept	0.0 ±

Dec. 38° 46!0 (N) S

BLOCK A

$\cos ZD = \cos d \cos h \cos l$

$- \cos d \cos l + \cos(l \pm d)$

BLOCK B

BLOCK C

BLOCK A

Cos d	38° 46!0 (N) S	0.77970
Cos h	58 01.9	0.52945
Cos l	17 11.3 (S)	0.95534
		0.39438

BLOCK B

Cos d		0.77970
Cos l		0.95534
		0.74488

BLOCK C

Cos (l±d)	21° 34!7	0.92992
-----------	----------	---------

BLOCK A	0.39438
BLOCK B	0.74488 -
(-)	0.35050
BLOCK C	0.92992 +
Cos ZD	0.57942
ZD	54° 35!4
Ac=90°-ZD	35° 24!6

Sec Ac	35° 24!6	1.22695
Cos d		0.77970
Sin h	58° 01!9	0.84834
Sin Z		0.81157
Z	(N) S 54° 14!9 (W)	

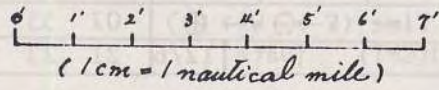
h > 180° suffix E
h < 180° suffix W

$\sin Z = \sec Ac \cos d \sin h$

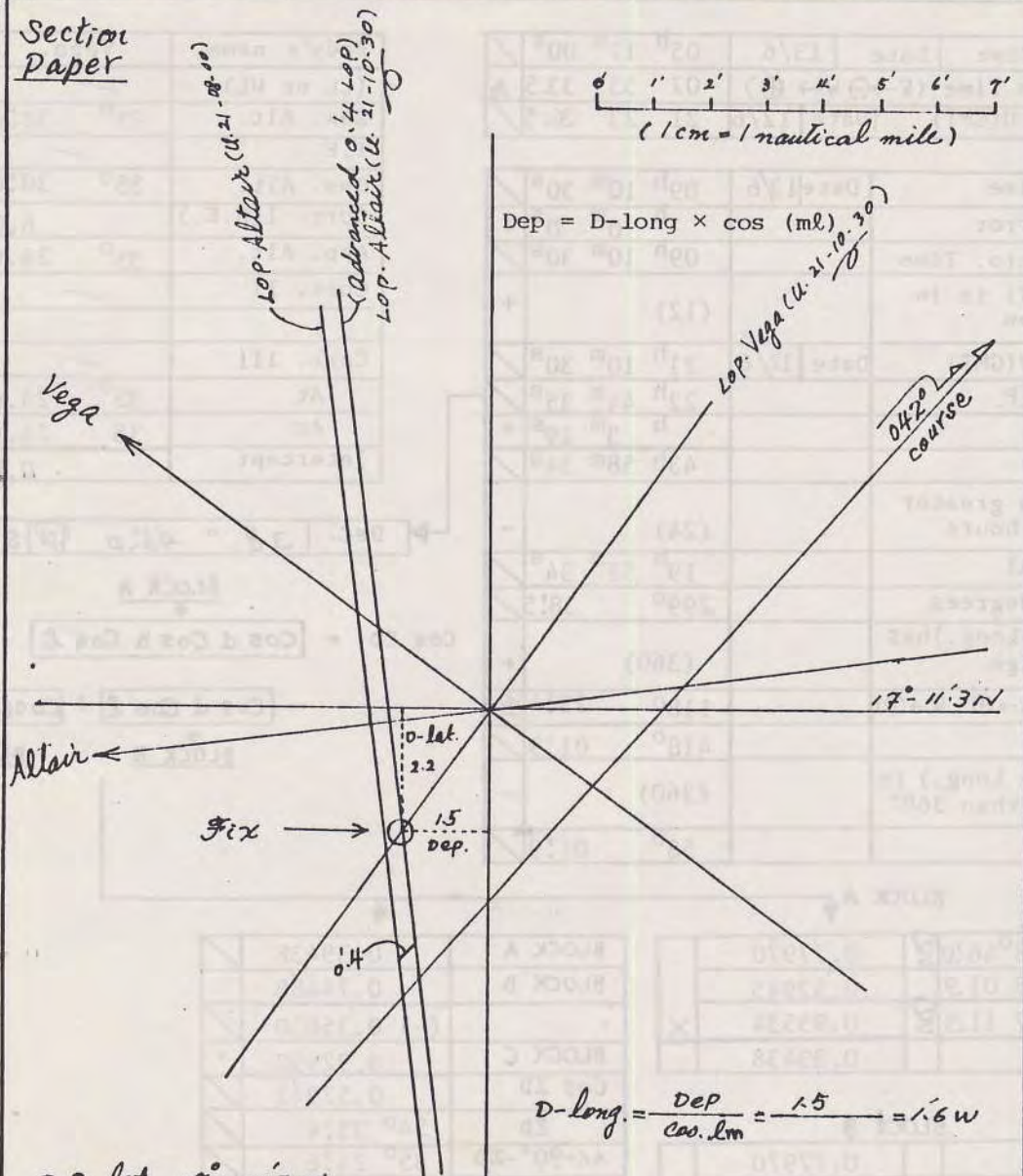
l & d same name l - d
l & d contrary name l + d

Formulae

Section Paper



$$\text{Dep} = D\text{-long} \times \cos (\text{ml})$$

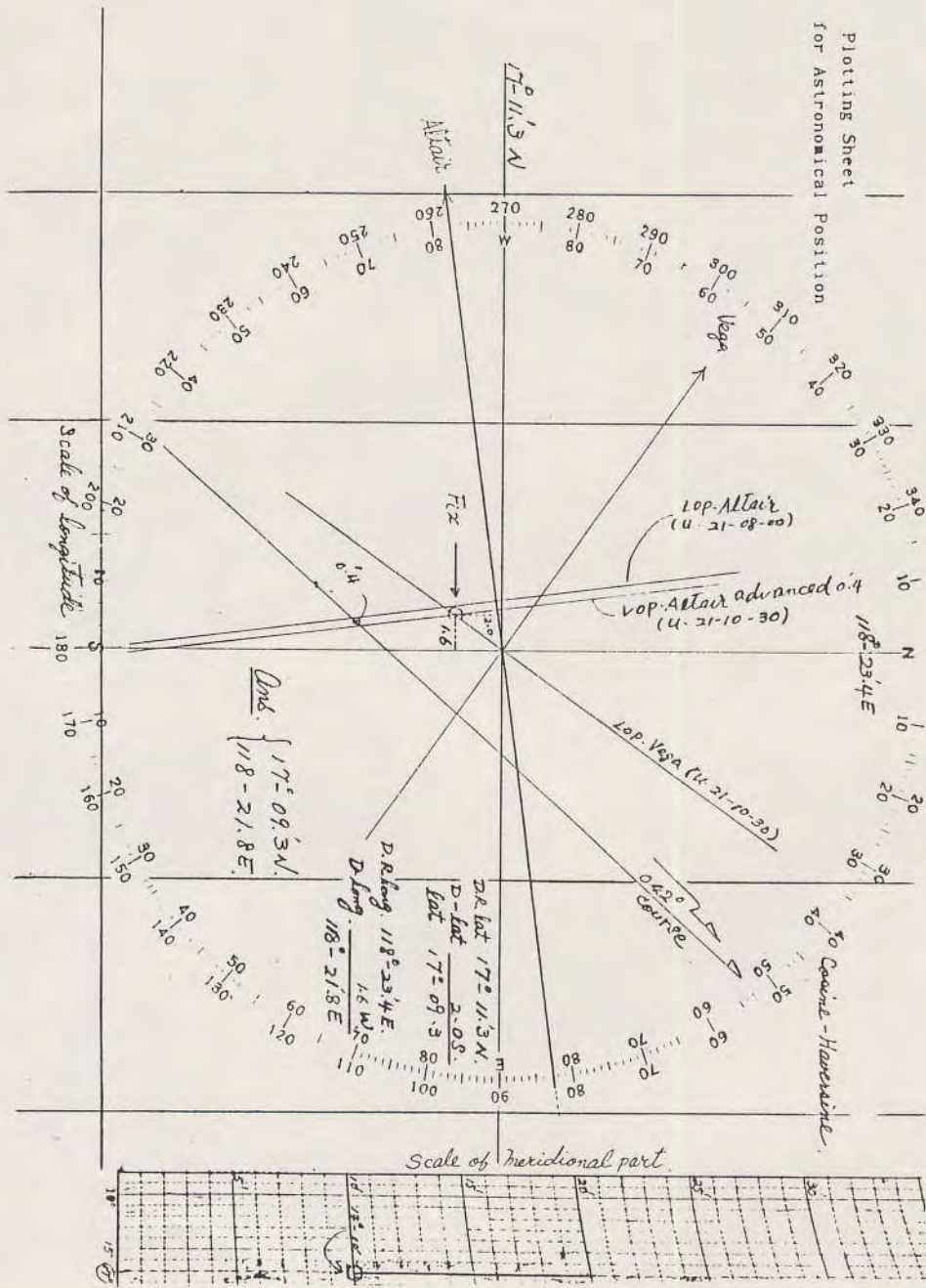


$$D\text{-long} = \frac{\text{Dep}}{\cos. \text{ml}} = \frac{1.5}{\cos. \text{ml}} = 1.6 \text{ W}$$

D.R. lat $17^{\circ} - 11.3' \text{ N}$
 D-lat $\frac{2.2 \text{ S}}{17 - 09.1 \text{ N}}$

D.R. long. $118^{\circ} - 23.4' \text{ E}$
 D-long. $\frac{1.6 \text{ W}}{118^{\circ} - 21.8' \text{ E}}$

Ans. $\left\{ \begin{array}{l} 17^{\circ} - 09.1' \text{ N.} \\ 118^{\circ} - 21.8' \text{ E.} \end{array} \right.$



NAUTICAL ALMANAC (1985)
&
INCREMENTS AND CORRECTIONS

EXTRACTED FROM THE NAUTICAL ALMANACE,
HER MAJESTY'S NAUTICAL ALMANAC OFFICE,
LONDON, U.K.

10^m

INCREMENTS AND CORRECTIONS

11^m

10	SUN PLANETS	ARIES	MOON	° or Corr ⁿ				
				°	'	"		
00	2 30-0	2 30-4	2 23-2	0-0	0-0	1-1	12-0	2-1
01	2 30-3	2 30-7	2 23-4	0-1	0-0	1-1	12-1	2-1
02	2 30-5	2 30-9	2 23-6	0-2	0-0	1-1	12-2	2-1
03	2 30-8	2 31-2	2 23-9	0-3	0-1	1-1	12-3	2-2
04	2 31-0	2 31-4	2 24-1	0-4	0-1	1-1	12-4	2-2
05	2 31-3	2 31-7	2 24-4	0-5	0-1	1-1	12-5	2-2
06	2 31-5	2 31-9	2 24-6	0-6	0-1	1-2	12-6	2-2
07	2 31-8	2 32-2	2 24-8	0-7	0-1	1-2	12-7	2-2
08	2 32-0	2 32-4	2 25-1	0-8	0-1	1-2	12-8	2-2
09	2 32-3	2 32-7	2 25-3	0-9	0-2	1-2	12-9	2-3
10	2 32-5	2 32-9	2 25-6	1-0	0-2	1-2	13-0	2-3
11	2 32-8	2 33-2	2 25-8	1-1	0-2	1-2	13-1	2-3
12	2 33-0	2 33-4	2 26-0	1-2	0-2	1-3	13-2	2-3
13	2 33-3	2 33-7	2 26-3	1-3	0-2	1-3	13-3	2-3
14	2 33-5	2 33-9	2 26-5	1-4	0-2	1-3	13-4	2-3
15	2 33-8	2 34-2	2 26-7	1-5	0-3	1-3	13-5	2-4
16	2 34-0	2 34-4	2 27-0	1-6	0-3	1-3	13-6	2-4
17	2 34-3	2 34-7	2 27-2	1-7	0-3	1-3	13-7	2-4
18	2 34-5	2 34-9	2 27-5	1-8	0-3	1-4	13-8	2-4
19	2 34-8	2 35-2	2 27-7	1-9	0-3	1-4	13-9	2-4
20	2 35-0	2 35-4	2 27-9	1-0	0-4	1-4	14-0	2-5
21	2 35-3	2 35-7	2 28-2	1-1	0-4	1-4	14-1	2-5
22	2 35-5	2 35-9	2 28-4	1-2	0-4	1-4	14-2	2-5
23	2 35-8	2 36-2	2 28-7	1-3	0-4	1-5	14-3	2-5
24	2 36-0	2 36-4	2 28-9	1-4	0-4	1-5	14-4	2-5
25	2 36-3	2 36-7	2 29-1	1-5	0-4	1-5	14-5	2-5
26	2 36-5	2 36-9	2 29-4	1-6	0-5	1-5	14-6	2-6
27	2 36-8	2 37-2	2 29-6	1-7	0-5	1-5	14-7	2-6
28	2 37-0	2 37-4	2 29-8	1-8	0-5	1-5	14-8	2-6
29	2 37-3	2 37-7	2 30-1	1-9	0-5	1-6	14-9	2-6
30	2 37-5	2 37-9	2 30-3	1-0	0-5	1-6	15-0	2-6
31	2 37-8	2 38-2	2 30-6	1-1	0-5	1-6	15-1	2-6
32	2 38-0	2 38-4	2 30-8	1-2	0-6	1-6	15-2	2-7
33	2 38-3	2 38-7	2 31-0	1-3	0-6	1-6	15-3	2-7
34	2 38-5	2 38-9	2 31-3	1-4	0-6	1-6	15-4	2-7
35	2 38-8	2 39-2	2 31-5	1-5	0-6	1-7	15-5	2-7
36	2 39-0	2 39-4	2 31-8	1-6	0-6	1-7	15-6	2-7
37	2 39-3	2 39-7	2 32-0	1-7	0-6	1-7	15-7	2-7
38	2 39-5	2 39-9	2 32-2	1-8	0-7	1-7	15-8	2-8
39	2 39-8	2 40-2	2 32-5	1-9	0-7	1-7	15-9	2-8
40	2 40-0	2 40-4	2 32-7	1-0	0-7	1-8	16-0	2-8
41	2 40-3	2 40-7	2 32-9	1-1	0-7	1-8	16-1	2-8
42	2 40-5	2 40-9	2 33-2	1-2	0-7	1-8	16-2	2-8
43	2 40-8	2 41-2	2 33-4	1-3	0-8	1-8	16-3	2-9
44	2 41-0	2 41-4	2 33-7	1-4	0-8	1-8	16-4	2-9
45	2 41-3	2 41-7	2 33-9	1-5	0-8	1-8	16-5	2-9
46	2 41-5	2 41-9	2 34-1	1-6	0-8	1-9	16-6	2-9
47	2 41-8	2 42-2	2 34-4	1-7	0-8	1-9	16-7	2-9
48	2 42-0	2 42-4	2 34-6	1-8	0-8	1-9	16-8	2-9
49	2 42-3	2 42-7	2 34-9	1-9	0-9	1-9	16-9	3-0
50	2 42-5	2 42-9	2 35-1	1-0	0-9	1-9	17-0	3-0
51	2 42-8	2 43-2	2 35-3	1-1	0-9	1-9	17-1	3-0
52	2 43-0	2 43-4	2 35-6	1-2	0-9	1-9	17-2	3-0
53	2 43-3	2 43-7	2 35-8	1-3	0-9	1-9	17-3	3-0
54	2 43-5	2 43-9	2 36-1	1-4	0-9	1-9	17-4	3-0
55	2 43-8	2 44-2	2 36-3	1-5	1-0	1-9	17-5	3-1
56	2 44-0	2 44-4	2 36-5	1-6	1-0	1-9	17-6	3-1
57	2 44-3	2 44-7	2 36-8	1-7	1-0	1-9	17-7	3-1
58	2 44-5	2 45-0	2 37-0	1-8	1-0	1-9	17-8	3-1
59	2 44-8	2 45-2	2 37-2	1-9	1-0	1-9	17-9	3-1
60	2 45-0	2 45-5	2 37-5	1-0	1-1	1-9	18-0	3-2

vii

11	SUN PLANETS	ARIES	MOON	° or Corr ⁿ				
				°	'	"		
00	2 45-0	2 45-5	2 37-5	0-0	0-0	1-2	12-0	2-3
01	2 45-3	2 45-7	2 37-7	0-1	0-0	1-2	12-1	2-3
02	2 45-5	2 46-0	2 38-0	0-2	0-0	1-2	12-2	2-3
03	2 45-8	2 46-2	2 38-2	0-3	0-1	1-2	12-3	2-4
04	2 46-0	2 46-5	2 38-4	0-4	0-1	1-2	12-4	2-4
05	2 46-3	2 46-7	2 38-7	0-5	0-1	1-2	12-5	2-4
06	2 46-5	2 47-0	2 38-9	0-6	0-1	1-3	12-6	2-4
07	2 46-8	2 47-2	2 39-2	0-7	0-1	1-3	12-7	2-4
08	2 47-0	2 47-5	2 39-4	0-8	0-2	1-3	12-8	2-5
09	2 47-3	2 47-7	2 39-6	0-9	0-2	1-3	12-9	2-5
10	2 47-5	2 48-0	2 39-9	1-0	0-2	1-3	13-0	2-5
11	2 47-8	2 48-2	2 40-1	1-1	0-2	1-3	13-1	2-5
12	2 48-0	2 48-5	2 40-3	1-2	0-2	1-4	13-2	2-5
13	2 48-3	2 48-7	2 40-6	1-3	0-2	1-4	13-3	2-5
14	2 48-5	2 49-0	2 40-8	1-4	0-3	1-4	13-4	2-6
15	2 48-8	2 49-2	2 41-1	1-5	0-3	1-4	13-5	2-6
16	2 49-0	2 49-5	2 41-3	1-6	0-3	1-4	13-6	2-6
17	2 49-3	2 49-7	2 41-5	1-7	0-3	1-5	13-7	2-6
18	2 49-5	2 50-0	2 41-8	1-8	0-3	1-5	13-8	2-6
19	2 49-8	2 50-2	2 42-0	1-9	0-4	1-5	13-9	2-7
20	2 50-0	2 50-5	2 42-3	1-0	0-4	1-5	14-0	2-7
21	2 50-3	2 50-7	2 42-5	1-1	0-4	1-5	14-1	2-7
22	2 50-5	2 51-0	2 42-7	1-2	0-4	1-6	14-2	2-7
23	2 50-8	2 51-2	2 43-0	1-3	0-4	1-6	14-3	2-7
24	2 51-0	2 51-5	2 43-2	1-4	0-5	1-6	14-4	2-8
25	2 51-3	2 51-7	2 43-4	1-5	0-5	1-6	14-5	2-8
26	2 51-5	2 52-0	2 43-7	1-6	0-5	1-6	14-6	2-8
27	2 51-8	2 52-2	2 43-9	1-7	0-5	1-7	14-7	2-8
28	2 52-0	2 52-5	2 44-2	1-8	0-5	1-7	14-8	2-8
29	2 52-3	2 52-7	2 44-4	1-9	0-6	1-7	14-9	2-9
30	2 52-5	2 53-0	2 44-6	1-0	0-6	1-7	15-0	2-9
31	2 52-8	2 53-2	2 44-9	1-1	0-6	1-7	15-1	2-9
32	2 53-0	2 53-5	2 45-1	1-2	0-6	1-8	15-2	2-9
33	2 53-3	2 53-7	2 45-4	1-3	0-6	1-8	15-3	2-9
34	2 53-5	2 54-0	2 45-6	1-4	0-7	1-8	15-4	3-0
35	2 53-8	2 54-2	2 45-8	1-5	0-7	1-8	15-5	3-0
36	2 54-0	2 54-5	2 46-1	1-6	0-7	1-8	15-6	3-0
37	2 54-3	2 54-7	2 46-3	1-7	0-7	1-9	15-7	3-0
38	2 54-5	2 55-0	2 46-6	1-8	0-7	1-9	15-8	3-0
39	2 54-8	2 55-2	2 46-8	1-9	0-7	1-9	15-9	3-0
40	2 55-0	2 55-5	2 47-0	1-0	0-8	1-9	16-0	3-1
41	2 55-3	2 55-7	2 47-3	1-1	0-8	1-9	16-1	3-1
42	2 55-5	2 56-0	2 47-5	1-2	0-8	1-9	16-2	3-1
43	2 55-8	2 56-2	2 47-7	1-3	0-8	1-9	16-3	3-1
44	2 56-0	2 56-5	2 48-0	1-4	0-8	1-9	16-4	3-1
45	2 56-3	2 56-7	2 48-2	1-5	0-9	1-9	16-5	3-2
46	2 56-5	2 57-0	2 48-5	1-6	0-9	1-9	16-6	3-2
47	2 56-8	2 57-2	2 48-7	1-7	0-9	1-9	16-7	3-2
48	2 57-0	2 57-5	2 48-9	1-8	0-9	1-9	16-8	3-2
49	2 57-3	2 57-7	2 49-2	1-9	0-9	1-9	16-9	3-2
50	2 57-5	2 58-0	2 49-4	1-0	1-0	1-9	17-0	3-3
51	2 57-8	2 58-2	2 49-7	1-1	1-0	1-9	17-1	3-3
52	2 58-0	2 58-5	2 49-9	1-2	1-0	1-9	17-2	3-3
53	2 58-3	2 58-7	2 50-1	1-3	1-0	1-9	17-3	3-3
54	2 58-5	2 59-0	2 50-4	1-4	1-0	1-9	17-4	3-3
55	2 58-8	2 59-2	2 50-6	1-5	1-1	1-9	17-5	3-4
56	2 59-0	2 59-5	2 50-8	1-6	1-1	1-9	17-6	3-4
57	2 59-3	2 59-7	2 51-1	1-7	1-1	1-9	17-7	3-4
58	2 59-5	3 00-0	2 51-3	1-8	1-1	1-9	17-8	3-4
59	2 59-8	3 00-2	2 51-6	1-9	1-1	1-9	17-9	3-4
60	3 00-0	3 00-5	2 51-8	1-0	1-2	1-9	18-0	3-5

8^m

INCREMENTS AND CORRECTIONS

9^m

8	SUN PLANETS	ARIES	MOON	v or Corr*			9	SUN PLANETS	ARIES	MOON	v or Corr*		
				v	or	Corr*					v	or	Corr*
00	2 00-0	2 00-3	1 54-5	0-0	0-0	6-0	0-0	2 15-0	2 15-4	2 08-9	0-0	0-0	6-0
01	2 00-3	2 00-6	1 54-8	0-1	0-0	6-1	0-0	2 15-3	2 15-6	2 09-1	0-1	0-0	6-1
02	2 00-5	2 00-8	1 55-0	0-2	0-0	6-2	0-0	2 15-5	2 15-9	2 09-3	0-2	0-0	6-2
03	2 00-8	2 01-1	1 55-2	0-3	0-0	6-3	0-0	2 15-8	2 16-1	2 09-5	0-3	0-0	6-3
04	2 01-0	2 01-3	1 55-5	0-4	0-1	6-4	0-0	2 16-0	2 16-4	2 09-8	0-4	0-1	6-4
05	2 01-3	2 01-6	1 55-7	0-5	0-1	6-5	0-0	2 16-3	2 16-6	2 10-0	0-5	0-1	6-5
06	2 01-5	2 01-8	1 56-0	0-6	0-1	6-6	0-0	2 16-5	2 16-9	2 10-3	0-6	0-1	6-6
07	2 01-8	2 02-1	1 56-2	0-7	0-1	6-7	0-0	2 16-8	2 17-1	2 10-5	0-7	0-1	6-7
08	2 02-0	2 02-3	1 56-4	0-8	0-1	6-8	0-0	2 17-0	2 17-4	2 10-8	0-8	0-1	6-8
09	2 02-3	2 02-6	1 56-7	0-9	0-1	6-9	0-0	2 17-3	2 17-6	2 11-0	0-9	0-1	6-9
10	2 02-5	2 02-8	1 56-9	1-0	0-1	7-0	0-0	2 17-5	2 17-9	2 11-2	1-0	0-2	7-0
11	2 02-8	2 03-1	1 57-2	1-1	0-2	7-1	0-0	2 17-8	2 18-1	2 11-5	1-1	0-2	7-1
12	2 03-0	2 03-3	1 57-4	1-2	0-2	7-2	0-0	2 18-0	2 18-4	2 11-7	1-2	0-2	7-2
13	2 03-3	2 03-6	1 57-6	1-3	0-2	7-3	0-0	2 18-3	2 18-6	2 12-0	1-3	0-2	7-3
14	2 03-5	2 03-8	1 57-9	1-4	0-2	7-4	0-0	2 18-5	2 18-9	2 12-2	1-4	0-2	7-4
15	2 03-8	2 04-1	1 58-1	1-5	0-2	7-5	0-0	2 18-8	2 19-1	2 12-4	1-5	0-2	7-5
16	2 04-0	2 04-3	1 58-4	1-6	0-2	7-6	0-0	2 19-0	2 19-4	2 12-7	1-6	0-3	7-6
17	2 04-3	2 04-6	1 58-6	1-7	0-2	7-7	0-0	2 19-3	2 19-6	2 12-9	1-7	0-3	7-7
18	2 04-5	2 04-8	1 58-8	1-8	0-3	7-8	0-0	2 19-5	2 19-9	2 13-1	1-8	0-3	7-8
19	2 04-8	2 05-1	1 59-1	1-9	0-3	7-9	0-0	2 19-8	2 20-1	2 13-4	1-9	0-3	7-9
20	2 05-0	2 05-3	1 59-3	2-0	0-3	8-0	0-0	2 20-0	2 20-4	2 13-6	2-0	0-3	8-0
21	2 05-3	2 05-6	1 59-5	2-1	0-3	8-1	0-0	2 20-3	2 20-6	2 13-9	2-1	0-3	8-1
22	2 05-5	2 05-8	1 59-8	2-2	0-3	8-2	0-0	2 20-5	2 20-9	2 14-1	2-2	0-3	8-2
23	2 05-8	2 06-1	2 00-0	2-3	0-3	8-3	0-0	2 20-8	2 21-1	2 14-3	2-3	0-4	8-3
24	2 06-0	2 06-3	2 00-3	2-4	0-3	8-4	0-0	2 21-0	2 21-4	2 14-6	2-4	0-4	8-4
25	2 06-3	2 06-6	2 00-5	2-5	0-4	8-5	0-0	2 21-3	2 21-6	2 14-8	2-5	0-4	8-5
26	2 06-5	2 06-8	2 00-7	2-6	0-4	8-6	0-0	2 21-5	2 21-9	2 15-1	2-6	0-4	8-6
27	2 06-8	2 07-1	2 01-0	2-7	0-4	8-7	0-0	2 21-8	2 22-1	2 15-3	2-7	0-4	8-7
28	2 07-0	2 07-3	2 01-2	2-8	0-4	8-8	0-0	2 22-0	2 22-4	2 15-5	2-8	0-4	8-8
29	2 07-3	2 07-6	2 01-5	2-9	0-4	8-9	0-0	2 22-3	2 22-6	2 15-8	2-9	0-5	8-9
30	2 07-5	2 07-8	2 01-7	3-0	0-4	9-0	0-0	2 22-5	2 22-9	2 16-0	3-0	0-5	9-0
31	2 07-8	2 08-1	2 01-9	3-1	0-4	9-1	0-0	2 22-8	2 23-1	2 16-2	3-1	0-5	9-1
32	2 08-0	2 08-4	2 02-2	3-2	0-5	9-2	0-0	2 23-0	2 23-4	2 16-5	3-2	0-5	9-2
33	2 08-3	2 08-6	2 02-4	3-3	0-5	9-3	0-0	2 23-3	2 23-6	2 16-7	3-3	0-5	9-3
34	2 08-5	2 08-9	2 02-6	3-4	0-5	9-4	0-0	2 23-5	2 23-9	2 17-0	3-4	0-5	9-4
35	2 08-8	2 09-1	2 02-9	3-5	0-5	9-5	0-0	2 23-8	2 24-1	2 17-2	3-5	0-6	9-5
36	2 09-0	2 09-4	2 03-1	3-6	0-5	9-6	0-0	2 24-0	2 24-4	2 17-4	3-6	0-6	9-6
37	2 09-3	2 09-6	2 03-4	3-7	0-5	9-7	0-0	2 24-3	2 24-6	2 17-7	3-7	0-6	9-7
38	2 09-5	2 09-9	2 03-6	3-8	0-5	9-8	0-0	2 24-5	2 24-9	2 17-9	3-8	0-6	9-8
39	2 09-8	2 10-1	2 03-8	3-9	0-6	9-9	0-0	2 24-8	2 25-1	2 18-2	3-9	0-6	9-9
40	2 10-0	2 10-4	2 04-1	4-0	0-6	10-0	0-0	2 25-0	2 25-4	2 18-4	4-0	0-6	10-0
41	2 10-3	2 10-6	2 04-3	4-1	0-6	10-1	0-0	2 25-3	2 25-6	2 18-6	4-1	0-6	10-1
42	2 10-5	2 10-9	2 04-6	4-2	0-6	10-2	0-0	2 25-5	2 25-9	2 18-9	4-2	0-7	10-2
43	2 10-8	2 11-1	2 04-8	4-3	0-6	10-3	0-0	2 25-8	2 26-1	2 19-1	4-3	0-7	10-3
44	2 11-0	2 11-4	2 05-0	4-4	0-6	10-4	0-0	2 26-0	2 26-4	2 19-3	4-4	0-7	10-4
45	2 11-3	2 11-6	2 05-3	4-5	0-6	10-5	0-0	2 26-3	2 26-6	2 19-6	4-5	0-7	10-5
46	2 11-5	2 11-9	2 05-5	4-6	0-7	10-6	0-0	2 26-5	2 26-9	2 19-8	4-6	0-7	10-6
47	2 11-8	2 12-1	2 05-7	4-7	0-7	10-7	0-0	2 26-8	2 27-2	2 20-1	4-7	0-7	10-7
48	2 12-0	2 12-4	2 06-0	4-8	0-7	10-8	0-0	2 27-0	2 27-4	2 20-3	4-8	0-8	10-8
49	2 12-3	2 12-6	2 06-2	4-9	0-7	10-9	0-0	2 27-3	2 27-7	2 20-5	4-9	0-8	10-9
50	2 12-5	2 12-9	2 06-5	5-0	0-7	11-0	0-0	2 27-5	2 27-9	2 20-8	5-0	0-8	11-0
51	2 12-8	2 13-1	2 06-7	5-1	0-7	11-1	0-0	2 27-8	2 28-2	2 21-0	5-1	0-8	11-1
52	2 13-0	2 13-4	2 06-9	5-2	0-7	11-2	0-0	2 28-0	2 28-4	2 21-3	5-2	0-8	11-2
53	2 13-3	2 13-6	2 07-2	5-3	0-8	11-3	0-0	2 28-3	2 28-7	2 21-5	5-3	0-8	11-3
54	2 13-5	2 13-9	2 07-4	5-4	0-8	11-4	0-0	2 28-5	2 28-9	2 21-7	5-4	0-9	11-4
55	2 13-8	2 14-1	2 07-7	5-5	0-8	11-5	0-0	2 28-8	2 29-2	2 22-0	5-5	0-9	11-5
56	2 14-0	2 14-4	2 07-9	5-6	0-8	11-6	0-0	2 29-0	2 29-4	2 22-2	5-6	0-9	11-6
57	2 14-3	2 14-6	2 08-1	5-7	0-8	11-7	0-0	2 29-3	2 29-7	2 22-5	5-7	0-9	11-7
58	2 14-5	2 14-9	2 08-4	5-8	0-8	11-8	0-0	2 29-5	2 29-9	2 22-7	5-8	0-9	11-8
59	2 14-8	2 15-1	2 08-6	5-9	0-8	11-9	0-0	2 29-8	2 30-2	2 22-9	5-9	0-9	11-9
60	2 15-0	2 15-4	2 08-9	6-0	0-9	12-0	0-0	2 30-0	2 30-4	2 23-2	6-0	1-0	12-0

SIGHT REDUCTION TABLE (1985)
&
ALTITUDE CORRECTION TABLES
Pub. No. 229, Vol. 2.
HER MAJESTY'S NAUTICAL ALMANAC OFFICE
LONDON, U.K.

A2 ALTITUDE CORRECTION TABLES 10°-90°—SUN, STARS, PLANETS

OCT.—MAR. SUN			APR.—SEPT.			STARS AND PLANETS				DIP				
App. Alt.	Lower Limb	Upper Limb	App. Alt.	Lower Limb	Upper Limb	App. Alt.	Corr ⁿ	App. Alt.	Additional Corr ⁿ	Ht. of Eye	Corr ⁿ	Ht. of Eye	Ht. of Eye	Corr ⁿ
9 34	10.8	-21.5	9 39	10.6	-21.2	9 56	-5.3	10 08	-5.2	1985				
9 45	10.9	-21.4	9 51	10.7	-21.1	10 08	-5.2	10 20	-5.1	VENUS				
9 56	11.0	-21.3	10 03	10.8	-21.0	10 33	-5.0	10 46	-4.9	Jan. 1-Feb. 4				
10 08	11.1	-21.2	10 15	10.9	-20.9	11 00	-4.8	11 14	-4.7	" 0 + 0.2				
10 21	11.2	-21.1	10 27	11.0	-20.8	11 29	-4.6	11 45	-4.5	41 + 0.1				
10 34	11.3	-21.0	10 40	11.1	-20.7	12 01	-4.4	12 18	-4.3	76 + 0.1				
10 47	11.4	-20.9	10 54	11.2	-20.6	12 35	-4.3	12 54	-4.1	Feb. 5-Feb. 28				
11 01	11.5	-20.8	11 08	11.3	-20.5	13 13	-4.0	13 33	-3.9	" 0 + 0.3				
11 15	11.6	-20.7	11 23	11.4	-20.4	13 54	-3.8	14 16	-3.7	34 + 0.2				
11 30	11.7	-20.6	11 38	11.5	-20.3	14 40	-3.7	15 04	-3.5	60 + 0.1				
11 46	11.8	-20.5	11 54	11.6	-20.2	15 30	-3.5	15 57	-3.4	80 + 0.1				
12 02	11.9	-20.4	12 10	11.7	-20.1	16 26	-3.2	16 56	-3.2	Mar. 1-Mar. 16				
12 19	12.0	-20.3	12 28	11.8	-20.0	17 28	-3.1	17 58	-2.6	" 0 + 0.4				
12 37	12.1	-20.2	12 46	11.9	-19.9	18 02	-2.9	18 38	-2.8	29 + 0.3				
12 55	12.2	-20.1	13 05	12.0	-19.8	18 38	-2.8	19 17	-2.7	51 + 0.2				
13 14	12.3	-20.0	13 24	12.1	-19.7	19 58	-2.6	20 42	-2.5	68 + 0.1				
13 35	12.4	-19.9	13 45	12.2	-19.6	20 42	-2.5	21 28	-2.5	83				
13 56	12.5	-19.8	14 07	12.3	-19.5	21 28	-2.5	22 19	-2.3	Mar. 17-Apr. 21				
14 18	12.6	-19.7	14 30	12.4	-19.4	22 19	-2.3	22 54	-2.2	" 0 + 0.5				
14 42	12.7	-19.6	14 54	12.5	-19.3	23 13	-2.2	24 11	-2.1	26 + 0.4				
15 06	12.8	-19.5	15 19	12.6	-19.2	24 11	-2.1	25 14	-2.0	46 + 0.3				
15 32	12.9	-19.4	15 46	12.7	-19.1	25 14	-2.0	26 22	-1.9	60 + 0.2				
15 59	13.0	-19.3	16 14	12.8	-19.0	26 22	-1.9	27 36	-1.8	73 + 0.1				
16 28	13.1	-19.2	16 44	12.9	-18.9	27 36	-1.8	28 56	-1.7	84 + 0.1				
16 59	13.2	-19.1	17 15	13.0	-18.8	28 56	-1.7	30 24	-1.6	Apr. 22-May 7				
17 32	13.3	-19.0	17 48	13.1	-18.7	30 24	-1.6	32 00	-1.5	" 0 + 0.6				
18 06	13.4	-18.9	18 24	13.2	-18.6	32 00	-1.5	33 45	-1.5	29 + 0.4				
18 42	13.5	-18.8	19 01	13.3	-18.5	33 45	-1.5	35 40	-1.4	51 + 0.3				
19 21	13.6	-18.7	19 42	13.4	-18.4	35 40	-1.4	37 48	-1.2	68 + 0.2				
20 03	13.7	-18.6	20 25	13.5	-18.3	37 48	-1.2	40 08	-1.1	83				
20 48	13.8	-18.5	21 11	13.6	-18.2	40 08	-1.1	42 44	-1.0	May 8-May 29				
21 35	13.9	-18.4	22 00	13.7	-18.1	42 44	-1.0	45 36	-0.9	" 0 + 0.7				
22 26	14.0	-18.3	22 54	13.8	-18.0	45 36	-0.9	48 47	-0.8	34 + 0.3				
23 22	14.1	-18.2	23 51	13.9	-17.9	48 47	-0.8	52 18	-0.7	60 + 0.2				
24 21	14.2	-18.1	24 53	14.0	-17.8	52 18	-0.7	56 11	-0.6	80 + 0.1				
25 26	14.3	-18.0	26 00	14.1	-17.7	56 11	-0.6	60 28	-0.5	May 30-July 18				
26 36	14.4	-17.9	27 13	14.2	-17.6	60 28	-0.5	65 08	-0.4	" 0 + 0.8				
27 52	14.5	-17.8	28 33	14.3	-17.5	65 08	-0.4	70 11	-0.3	41 + 0.2				
29 15	14.6	-17.7	30 00	14.4	-17.4	70 11	-0.3	75 34	-0.2	76 + 0.1				
30 46	14.7	-17.6	31 35	14.5	-17.3	75 34	-0.2	81 13	-0.1	July 19-Dec. 31				
32 26	14.8	-17.5	33 20	14.6	-17.2	81 13	-0.1	87 03	0.0	" 0 + 0.9				
34 17	14.9	-17.4	35 17	14.7	-17.1	87 03	0.0	90 00	0.0	60 + 0.1				
36 20	15.0	-17.3	37 26	14.8	-17.0	90 00	0.0			MARS				
38 36	15.1	-17.2	39 50	14.9	-16.9					Jan. 1-Dec. 31				
41 08	15.2	-17.1	42 31	15.0	-16.8					" 0 + 1.0				
43 59	15.3	-17.0	45 31	15.1	-16.7					" 0 + 1.1				
47 10	15.4	-16.9	48 55	15.2	-16.6					" 0 + 1.2				
50 46	15.5	-16.8	52 44	15.3	-16.5					" 0 + 1.3				
54 49	15.6	-16.7	57 02	15.4	-16.4					" 0 + 1.4				
59 23	15.7	-16.6	61 51	15.5	-16.3					" 0 + 1.5				
64 30	15.8	-16.5	67 17	15.6	-16.2					" 0 + 1.6				
70 12	15.9	-16.4	73 16	15.7	-16.1					" 0 + 1.7				
76 26	16.0	-16.3	79 43	15.8	-16.0					" 0 + 1.8				
83 05	16.1	-16.2	86 32	15.9	-15.9					" 0 + 1.9				
90 00			90 00							" 0 + 2.0				

App. Alt. = Apparent altitude = Sextant altitude corrected for index error and dip.

SIGHT REDUCTION TABLE

58°, 302° L.H.A.

LATITUDE SAME NAME AS DECLINATION

N. Lat. L.H.A. greater than 180° Z=360-Z
L.H.A. less than 180° Z=Z

Table with columns for Declination (Dec.) and Latitude (15° to 22°), and rows for Local Hour Angle (L.H.A.) from 0 to 90. Each cell contains three values representing sight reduction data.

58°, 302° L.H.A.

LATITUDE SAME NAME AS DECLINATION

SIGHT REDUCTION TABLE

39°, 321° L.H.A.

LATITUDE SAME NAME AS DECLINATION

N. Lat. { LHA greater than 180° Z = Z
LHA less than 180° Z = 360° - Z

Table with columns for Dec., 15°, 16°, 17°, 18°, 19°, 20°, 21°, 22°, and Dec. Each column contains numerical data for sight reduction.

39°, 321° L.H.A.

LATITUDE SAME NAME AS DECLINATION

INTERPOLATION TABLE

Dec Inc	Altitude Difference (d)										Double Second Diff and Corr.	Dec Inc	Altitude Difference (d)										Double Second Diff and Corr.				
	Tens			Decimals			Units						Tens			Decimals			Units								
	10'	20'	30'	0'	1'	2'	3'	4'	5'	6'			7'	8'	9'	10'	20'	30'	40'	50'	0'	1'		2'	3'	4'	5'
44.0	7.3	14.6	22.0	29.3	36.6	0	0007	1522	3037	4452	5967	7503	52.0	8.6	17.3	26.0	34.6	43.3	0	0009	1726	3544	5261	7079	18		
44.1	7.3	14.7	22.1	29.4	36.7	1	0108	1623	3138	4653	6168	7683	52.1	8.7	17.3	26.1	34.7	43.4	1	0110	1827	3645	5362	7180	19		
44.2	7.3	14.7	22.1	29.4	36.8	2	0210	1724	3239	4754	6269	7784	52.2	8.7	17.4	26.1	34.8	43.5	2	0210	1928	3745	5463	7280	20		
44.3	7.4	14.8	22.2	29.5	36.9	3	0310	1825	3340	4855	6370	7885	52.3	8.7	17.4	26.1	34.9	43.6	3	0311	2029	3846	5564	7381	21		
44.4	7.4	14.8	22.2	29.6	37.0	4	0310	1825	3340	4855	6370	7885	52.4	8.7	17.5	26.2	34.9	43.7	4	0312	2130	3947	5665	7482	22		
44.5	7.4	14.8	22.3	29.7	37.1	5	0411	1926	3441	4956	6471	7976	52.5	8.8	17.5	26.3	35.0	43.8	5	0413	2231	4048	5766	7583	23		
44.6	7.4	14.9	22.3	29.7	37.2	6	0412	1927	3442	4957	6472	7977	52.6	8.8	17.5	26.3	35.1	43.8	6	0514	2332	4149	5867	7684	24		
44.7	7.5	14.9	22.4	29.8	37.3	7	0513	2027	3542	5057	6572	8077	52.7	8.8	17.6	26.4	35.2	43.9	7	0615	2433	4250	5968	7785	25		
44.8	7.5	15.0	22.4	29.9	37.4	8	0613	2128	3643	5158	6673	8178	52.8	8.8	17.6	26.4	35.2	44.0	8	0716	2534	4351	6069	7886	26		
44.9	7.5	15.0	22.5	30.0	37.5	9	0714	2229	3744	5259	6774	8279	52.9	8.9	17.7	26.5	35.3	44.1	9	0817	2635	4452	6170	7987	27		
45.0	7.5	15.0	22.5	30.0	37.5	0	0008	1523	3038	4553	6068	7583	53.0	8.9	17.7	26.5	35.3	44.1	0	0009	1827	3645	5362	7180	28		
45.1	7.5	15.0	22.5	30.0	37.6	1	0108	1624	3139	4654	6169	7684	53.1	8.9	17.7	26.5	35.4	44.2	1	0110	1928	3746	5463	7281	29		
45.2	7.5	15.0	22.6	30.1	37.6	2	0209	1724	3239	4755	6270	7785	53.2	8.9	17.7	26.6	35.4	44.3	2	0211	2029	3847	5564	7382	30		
45.3	7.5	15.1	22.6	30.2	37.7	3	0210	1725	3240	4756	6271	7786	53.3	8.9	17.8	26.6	35.5	44.4	3	0312	2129	3948	5665	7483	31		
45.4	7.6	15.1	22.7	30.3	37.8	4	0311	1826	3341	4856	6371	7886	53.4	8.9	17.8	26.7	35.6	44.5	4	0413	2230	4049	5766	7584	32		
45.5	7.6	15.2	22.8	30.3	37.9	5	0411	1927	3442	4957	6472	7987	53.5	8.9	17.8	26.8	35.7	44.6	5	0413	2231	4049	5767	7585	33		
45.6	7.6	15.2	22.8	30.4	38.0	6	0512	2027	3542	5058	6573	8088	53.6	8.9	17.9	26.8	35.7	44.7	6	0514	2332	4150	5868	7686	34		
45.7	7.6	15.3	22.9	30.5	38.1	7	0513	2028	3543	5159	6674	8189	53.7	9.0	17.9	26.9	35.8	44.8	7	0615	2433	4251	6069	7787	35		
45.8	7.7	15.3	22.9	30.6	38.2	8	0614	2129	3644	5260	6775	8290	53.8	9.0	18.0	26.9	35.9	44.9	8	0716	2534	4352	6170	7888	36		
45.9	7.7	15.3	23.0	30.6	38.3	9	0714	2230	3745	5361	6876	8391	53.9	9.0	18.0	27.0	36.0	45.0	9	0817	2635	4453	6271	7989	37		
46.0	7.6	15.3	23.0	30.6	38.3	0	0008	1523	3139	4654	6169	7684	54.0	9.0	18.0	27.0	36.0	45.0	0	0009	1827	3645	5464	7382	38		
46.1	7.7	15.3	23.0	30.7	38.4	1	0109	1624	3240	4755	6270	7785	54.1	9.0	18.0	27.0	36.0	45.1	1	0110	1928	3746	5565	7483	39		
46.2	7.7	15.4	23.1	30.8	38.5	2	0209	1725	3341	4856	6371	7886	54.2	9.0	18.0	27.1	36.1	45.2	2	0211	2029	3847	5666	7584	40		
46.3	7.7	15.4	23.1	30.9	38.6	3	0210	1726	3342	4957	6472	7987	54.3	9.0	18.1	27.1	36.2	45.3	3	0312	2130	3948	5767	7685	41		
46.4	7.7	15.5	23.2	30.9	38.7	4	0311	1826	3442	5058	6573	8088	54.4	9.1	18.1	27.2	36.3	45.4	4	0413	2231	4049	5868	7786	42		
46.5	7.8	15.5	23.3	31.0	38.8	5	0412	1927	3543	5159	6674	8189	54.5	9.1	18.2	27.3	36.3	45.4	5	0514	2332	4150	5969	7887	43		
46.6	7.8	15.5	23.3	31.1	38.8	6	0512	2028	3544	5260	6775	8290	54.6	9.1	18.2	27.3	36.4	45.5	6	0615	2433	4251	6070	7988	44		
46.7	7.8	15.6	23.4	31.2	38.9	7	0513	2129	3645	5361	6876	8391	54.7	9.1	18.3	27.4	36.5	45.6	7	0716	2534	4352	6171	7989	45		
46.8	7.8	15.6	23.4	31.2	39.0	8	0614	2229	3746	5462	6977	8492	54.8	9.2	18.3	27.4	36.6	45.7	8	0817	2635	4453	6272	8090	46		
46.9	7.9	15.7	23.5	31.3	39.1	9	0715	2330	3846	5563	7078	8593	54.9	9.2	18.3	27.5	36.6	45.8	9	0918	2736	4554	6373	8191	47		
47.0	7.8	15.6	23.5	31.3	39.1	0	0008	1624	3240	4755	6271	7786	55.0	9.1	18.3	27.5	36.6	45.8	0	0009	1828	3746	5565	7483	48		
47.1	7.8	15.7	23.5	31.4	39.2	1	0109	1725	3341	4856	6372	7887	55.1	9.2	18.3	27.5	36.7	45.9	1	0110	1929	3847	5666	7584	49		
47.2	7.8	15.7	23.6	31.4	39.3	2	0209	1725	3341	4957	6473	7988	55.2	9.2	18.4	27.6	36.8	46.0	2	0211	2030	3948	5767	7685	50		
47.3	7.9	15.8	23.6	31.5	39.4	3	0210	1826	3442	5058	6574	8089	55.3	9.2	18.4	27.6	36.9	46.1	3	0312	2131	4049	5868	7786	51		
47.4	7.9	15.8	23.7	31.6	39.5	4	0311	1927	3543	5159	6675	8190	55.4	9.2	18.5	27.7	36.9	46.2	4	0413	2231	4150	5969	7887	52		
47.5	7.9	15.8	23.8	31.7	39.6	5	0412	2028	3644	5260	6776	8291	55.5	9.3	18.5	27.8	37.0	46.3	5	0514	2332	4251	6070	7988	53		
47.6	7.9	15.9	23.8	31.7	39.7	6	0513	2129	3745	5361	6877	8392	55.6	9.3	18.5	27.8	37.1	46.4	6	0615	2433	4352	6171	8089	54		
47.7	8.0	15.9	23.9	31.8	39.8	7	0614	2230	3846	5462	6978	8493	55.7	9.3	18.6	27.9	37.2	46.4	7	0716	2534	4453	6272	8090	55		
47.8	8.0	16.0	23.9	31.9	39.9	8	0715	2331	3947	5563	7079	8594	55.8	9.3	18.6	27.9	37.2	46.5	8	0817	2635	4554	6373	8191	56		
47.9	8.0	16.0	24.0	32.0	40.0	9	0715	2331	3947	5563	7079	8594	55.9	9.4	18.7	28.0	37.3	46.6	9	0918	2736	4655	6474	8292	57		
48.0	8.0	16.0	24.0	32.0	40.0	0	0008	1624	3240	4857	6373	7888	56.0	9.3	18.6	28.0	37.3	46.6	0	0009	1928	3847	5666	7685	58		
48.1	8.0	16.0	24.0	32.0	40.1	1	0109	1725	3341	4958	6474	7989	56.1	9.3	18.7	28.0	37.4	46.7	1	0110	2029	3948	5767	7786	59		
48.2	8.0	16.0	24.1	32.1	40.1	2	0210	1826	3442	5059	6575	8090	56.2	9.3	18.7	28.1	37.4	46.8	2	0211	2130	4049	5868	7887	60		
48.3	8.0	16.1	24.1	32.2	40.2	3	0211	1927	3543	5160	6676	8191	56.3	9.4	18.8	28.1	37.5	46.9	3	0312	2231	4150	5969	7988	61		
48.4	8.1	16.1	24.2	32.3	40.3	4	0311	1927	3543	5261	6777	8292	56.4	9.4	18.8	28.2	37.6	47.0	4	0413	2332	4251	6070	8089	62		
48.5	8.1	16.2	24.3	32.3	40.4	5	0412	2028	3644	5362	6878	8393	56.5	9.4	18.8	28.3	37.7	47.1	5	0514	2433	4352	6171	8190	63		
48.6	8.1	16.2	24.3	32.4	40.5	6	0513	2129	3745	5463	6979	8494	56.6	9.4	18.9	28.3	37.7	47.2	6	0615	2534	4453	6272	8191	64		
48.7	8.1	16.3	24.4	32.5	40.6	7	0614	2230	3846	5564	7080	8595	56.7	9.5	18.9	28.4	37.8	47.3	7	0716	2635	4554	6373	8292	65		
48.8	8.2	16.3	24.4	32.6	40.7	8	0715	2331	3947	5665	7181	8696	56.8	9.5	19.0	28.4	37.9	47.4	8	0817	2736	4655	6474	8393	66		
48.9	8.2	16.3	24.5	32.6	40.8	9	0715	2332	4048	5766	7282	8797	56.9	9.5	19.0	28.5	38.0	47.5	9	0918	2837	4756	6575	8494	67		
49.0	8.1	16.3	24.5	32.6	40.8	0	0008	1625	3341	4958	6474	7989	57.0	9.5	19.0	28.5	38.0	47.5	0	0010	1929	3948	5767	7786	68		
49.1	8.2	16.3	24.5	32.7	40.9	1	0109	1726	3442	5059	6575	8090	57.1	9.5	19.0	28.5	38.0	47.6	1	0111	2030	4049	5868				

4. How to Program the Formulae of Celestial Navigation

By CASIO fx-180P, fx-3600P, fx-4000P, fx-7000G and fx-8000G.

Electronic calculator "Casio fx-180P" can be programmed. It has a program memory of 38 steps and two programmed procedures of computation can be stored in the memory. To store a program in the calculator, execute ordinary calculation in the LRN mode (MODE 0).

Then the program has been memorized. Input data and press ENT Key and the calculator executes the program according to the data. So an expeditious solution will be available repeatedly.

As mentioned, "Casio fx-180P" has a memory of only 38 steps, so the basic formula : $Ac = 90^\circ - \cos^{-1} \{ (\cos Lat. \times \cos Dec. \times \cos LHA) - \cos L. \times \cos D + \cos (L+D) \}$ should be simplified and restated as follows:

$$Ac = 90^\circ - \cos^{-1} \left\{ (\cos Lat. \times \cos Dec. \times \cos LHA) - \frac{\cos Lat. \times \cos Dec. + (\cos Lat. \times \cos Dec. - \sin Lat. \times \sin Dec.)}{\sin Dec.} \right\}$$

$$\therefore \cos (\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta$$

$$= 90^\circ - \cos^{-1} \left\{ (\cos Lat. \times \cos Dec. \times \cos LHA) + \frac{\sin Lat. \times \sin Dec.}{\sin Dec.} \right\}$$

$$= \sin^{-1} \{ (\cos Lat. \times \cos Dec. \times \cos LHA) + \sin Lat. \times \sin Dec. \}$$

$$\therefore 90^\circ - \cos^{-1} (\theta) = \sin^{-1} (\theta)$$

Concerning the formula of azimuth of a celestial body:

$Z = \sin^{-1} (\sin LHA \times \cos Dec. \div \cos Ac)$ can be programmed as it is. Therefore,

$$\text{Program 1 (P}_1\text{)} = \sin^{-1} \left\{ (\cos Lat. \times \cos Dec. \times \cos LHA) + \sin Lat. \times \sin Dec. \right\}$$

$$\text{Program 2 (P}_2\text{)} = \sin^{-1} (\sin LHA \times \cos Dec. \div \cos \frac{Ac}{(P_1)})$$

Program Lat.(L) = 21°N, Dec.(D) = 19°N, and LHA = 315°

MODE	0	P ₁	MODE	4	ENT	2	1	0''	Kin	1	ENT	1	9	0''	Kin	2	ENT
	3	1	5	0''	Kin	3											
Kout	1	sin	x	Kout	2	sin)	+	Kout	1	cos	x	Kout	2	cos	x	
Kout	3	cos)	INV	sin ⁻¹	=	Kin	4	INV	HLT							

Ref: Ac (= Hc) = sin⁻¹ (cos L x cos D x cos LHA) + (sin L x sin D)

INV	P ₂	Kout	3	sin	x	Kout	2	cos	+	Kout	4	cos)	inv	sin ⁻¹
-----	----------------	------	---	-----	---	------	---	-----	---	------	---	-----	---	-----	-------------------

Ref: Z = Sin⁻¹ (sin LHA x cos D + cos Ac)

Run --- Computation by the program.

Attention!

when latitude (L) and declination (D) are of contrary name declination should be treated as a negative value.

Example 1 — From "Sight Reduction Table" Page 93, Vol.2. Pub. No.229

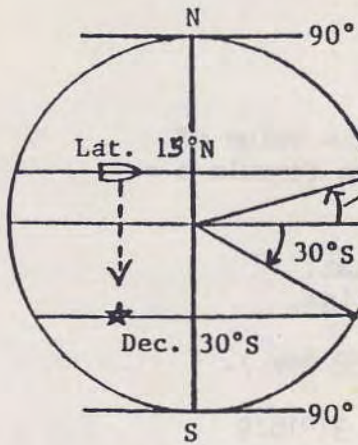
Required:- Ac and Z, when lat. = 15°N, dec. = 30°S and LHA = 315°

Solution

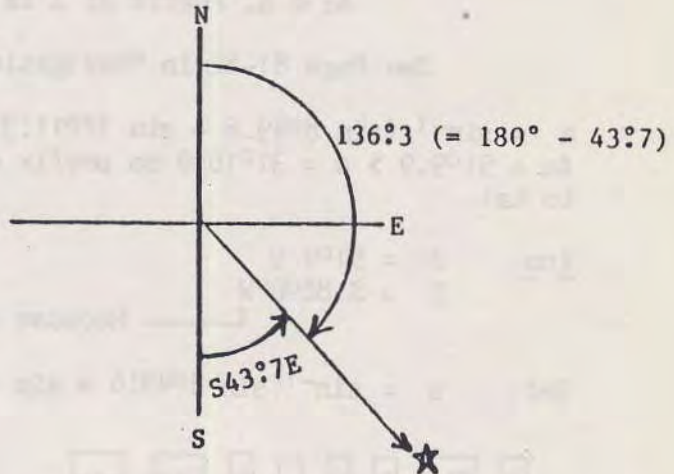
MODE	.	P ₁	1	5	0''	ENT	3	0	0''	+/-	ENT	3	1	5	0''	ENT
------	---	----------------	---	---	-----	-----	---	---	-----	-----	-----	---	---	---	-----	-----

→ 27.522495 INV 0'' → 27°31' 20.98 (= 27°31'.3 → 20.98/60 ÷ 0.3497 = 0.3)

INV P₂ → -43.6711912 (÷ 43°7) INV 0'' → -43°40' 16.2 (= -43°40'.3 → 16.2/60 = 0.27)



Prefix of Z = South.
 Suffix of Z = East (Because of $LHA > 270^\circ$)
 $\therefore Z = S 43.7^\circ E$ ($S 43^\circ 40' 3'' E$)
 or 136.3



Ans. $A_c = 27^\circ 31' 3''$
 $Z = S 43.7^\circ E$ or 136.3

Example 2 - From page

Required:- A_c and Z , when $Lat. = 17^\circ 11' 3'' N$, $Dec. = 08^\circ 49' 6'' N$, and $LHA = 39^\circ 00' 2''$.

Solution

P1 1 7 01" 1 1 . 3 01" ENT 8 01" 4 9 . 6 01" ENT

3 9 01" 0 . 2 01" ENT $\rightarrow 51.16505034$ INV 01" $\rightarrow 51^\circ 09' 54.18$

(= $51^\circ 09' 9'' \rightarrow 54.18/60 = 0.903 \div 0.9$) RUN $\rightarrow 82.63971254$ INV 01" \rightarrow
 ($\div 82^\circ 6'$)

$82^\circ 38' 22.97'' (= 82^\circ 38' 4'' \rightarrow 22.97/60 = 0.38 \div 0.4)$

Attention!

In a case when

Lat. and Dec. are the same names and the value of Lat. > value of Dec., the prefix of Z (= 82°) should be checked by the formula $a = \sin^{-1}(\sin D \div \sin L)$ of Altitude in Prime Vertical.

- when $A_c > a$, Prefix of Z is contrary name to Lat.
- when $A_c < a$, Prefix of Z is the same name as Lat.

See Page 81-82 in "Navigation Table" (TD/LN/52 Rev.).

$a = \sin^{-1}(\sin 80^{\circ}49.6 \div \sin 17^{\circ}11.3) = 31.28203863 = 31^{\circ}16.9$
 $A_c = 51^{\circ}09.9 > a = 31^{\circ}16.9$ so prefix of Z should be contrary name to Lat.

Ans. $A_c = 51^{\circ}09.9$
 $Z = S 82^{\circ}06' W$
 ↑ Because of LHA < 180°

Ref: $a = \sin^{-1}(\sin 80^{\circ}49.6 \div \sin 17^{\circ}11.3)$

8	01"	4	9	.	6	01"	sin	-	1	7	01"	1	1	.	3	01"															
sin =								→ 0.519251226								INV sin								→ 31.28203863							
INV 01"								→ 31°16'55.34								(= 31°16.9 → 55.34/60 = 0.922 ÷ 0.9)															

Example 3 - From page 247.

Required: - A_c and Z, when Lat. = $17^{\circ}11.3 N$, Dec. = $38^{\circ}46.0 N$, and
 $LHA = 58^{\circ}01.9$.

P1	1	7	01"	1	1	.	3	01"	ENT	3	8	01"	4	6	01"																
ENT 5 8 01"								. 9 01"								ENT → 35.40925418								INV 01"							
→ 35°24' 33.32								(= 35°24.6 → 33.32/60 ÷ 0.5553 = 0.6)																							

$$\boxed{\text{RUN}} \rightarrow 54.24913429 \quad \boxed{\text{INV}} \quad \boxed{0.9} \quad 54^{\circ}14'0'' \quad 56.88 \quad (= 54^{\circ}14'9'' \rightarrow Z)$$

$$56.88/60 = 0.948 \div 0.9$$

In this case the computation of $a = \sin^{-1}(\sin D + \sin L)$ to check the prefix of Z ($= 54^{\circ}14'9''$) is unnecessary. Because the value of Dec. ($38^{\circ}46'0''$) is greater than that of Lat. ($= 17^{\circ}11'3''$) although Lat. and Dec. are the same name.

Ans. $Ac = 35^{\circ}24'6''$
 $Z = N 54^{\circ}2' W$ or $N 54^{\circ}14'9'' W$

Example 4

when Lat. = $52^{\circ}28'2'' N$, Dec. = $11^{\circ}09'0'' S$ and LHA = $323^{\circ}30'7''$

Required:- Ac and Z (please be careful when L and D are of contrary name)

Ans. $Ac = 19.0967568 = 19^{\circ}05'48''.32 = 19^{\circ}05'8''$
 $Z = -38.127409 = -38^{\circ}07'38''.67 = S 38^{\circ}07'6'' E$

Example 5

when Lat. = $52^{\circ}28'2'' N$, Dec. = $20^{\circ}16'3'' N$, and LHA = $39^{\circ}44'0''$

Required:- Ac and Z

Ans. $Ac = 45.57938214 = 45^{\circ}34'05''.78 = 45^{\circ}34'8''$
 $Z = 58.94817626 = 58^{\circ}56'05''.43 = S 58^{\circ}56'9'' W$

Ref. : Lat. and Dec. are the same name and Lat. > Dec.

$$\text{Then } a = \sin^{-1}(\sin D + \sin L) = \sin^{-1}(\sin 20^{\circ}16'3'' + \sin 52^{\circ}28'2'')$$

$$= 25.90585778 = 25^{\circ}54'21''.09 = 25^{\circ}54'4''$$

$$Ac (= 45^{\circ}34'8'') > a (= 25^{\circ}54'4'')$$

So the prefix of Z ($= 58^{\circ}56'9''$) should be contrary to Lat. ($\rightarrow S$)

Example 6

when Lat. = $15^{\circ}08'0'' S$, Dec. = $56^{\circ}50'0'' S$ and LHA = $293^{\circ}27'5''$

Required:- Ac and Z

Ans. $Ac = 25.38906874 = 25^{\circ}23^{\circ}20.65 = 25^{\circ}23'3$
 $Z = -33.7460874 = -33^{\circ}44^{\circ}45.9 = S 33^{\circ}44'8 E$

In this case the computation of $a = \sin^{-1}(\sin D + \sin L)$ to check the prefix of Z is unnecessary. Because the value of Dec. is greater than that of Lat. although Lat. and Dec. are the same name.

Example 7

when Lat. = $15^{\circ}08'0 S$, Dec. = $38^{\circ}44'9 N$ and LHA = $321^{\circ}06'3$

Required:- Ac and Z

Ans. $Ac = 24.99537237 = 24^{\circ}59^{\circ}43.43 = 24^{\circ}59'7$
 $Z = -32.7041063 = -32^{\circ}42^{\circ}14.7 = N 32^{\circ}42'2 E$

Example 8

when Lat. = $28^{\circ}17'0 N$, Dec. = $15^{\circ}52'1 S$ and LHA = $60^{\circ}24'3$

Required:- Ac and Z

Ans. $Ac = 16.7845703 = 16^{\circ}47^{\circ}04.45 = 16^{\circ}47'1$
 $Z = 60.88216353 = 60^{\circ}52^{\circ}55.75 = S 60^{\circ}52'9 W$

Example 9

when Lat. = $28^{\circ}22'8 N$, Dec. = $16^{\circ}40'5 S$ and LHA = $307^{\circ}16'5$

Required:- Ac and Z

Ans. $Ac = 21.96595906 = 21^{\circ}57^{\circ}57.45 = 21^{\circ}57'9$
 $Z = -55.2797932 = -55^{\circ}16^{\circ}47.2 = S 55^{\circ}16'8 E$

Casio fx-3600 P

Program

MODE 0 P1 MODE 4
 ENT 2 1 0'' Kin 1 ENT 1 9 0'' Kin 2 ENT 3 1 5 0''
 Kin 3
 Kout 1 cos x Kout 2 cos x Kout 3 cos)] +
 Kout 1 sin x Kout 2 sin)] INV sin = Kin 4 INV HLT
 Ref.(1): $Ac(= Hc) = \sin^{-1}\{(\cos \text{ Lat. } \times \cos \text{ Dec. } \times \cos \text{ LHA}) + (\sin \text{ Lat. } \times \sin \text{ Dec.})\}$
 Kout 3 sin x Kout 2 cos + Kout 4 cos)] INV \sin^{-1}
 INV RTN
 Ref.(2): $Z = \sin^{-1}(\sin \text{ LHA } \times \cos \text{ Dec. } + \cos \text{ Ac})$

Ref.(3): To erase program P1 or P2 → MODE 0 (or INV P2)

INV PCL

To erase both P1 and P2 → MODE 0 INV PCL

Run --- The calculator executes the program with the data.

Example 1

MODE . P1 2 1 0' " ENT 1 9 0' " ENT 3 1 5 0' " ENT →

47.8037721 INV 0' " → 47°48'13.58 (= 47°48'2, 13.58/60 ≐ 0.226 ≐ 0.2)

ENT → -84.5026918 = -84°5 → See "Sight Reduction Table" page 92, Vol.2, Pub. No.229

Example 2

when Lat. = 15°N, Dec. = 30°S, and LHA = 315°

Required:- Ac and Z

Attention!: when latitude and declination are of contrary name, declination should be treated as a negative value.

Solution

MODE . P1 1 5 0' " ENT 3 0 0' " +/- ENT 3 1 5 0' "

ENT → 27.522495 INV 0' " → 27°31'20.98 (= 27°31'3 → 20.98/60

≐ 0.3497 ≐ 0.3 ENT → -43.6711912 ≐ -43°7 or 136°3 (= 180°-43°7)

See "Sight Reduction Tables" page 93, Vol.2, Pub. No.229

Example 3

when Lat. = 14°N, Dec. = 26°S, and LHA = 327°

Required:- Ac and Z

(MODE $\boxed{\cdot}$) $\boxed{P_1}$ $\boxed{1}$ $\boxed{4}$ $\boxed{0''}$ \boxed{ENT} $\boxed{2}$ $\boxed{6}$ $\boxed{0''}$ $\boxed{+/-}$ \boxed{ENT} $\boxed{3}$ $\boxed{2}$ $\boxed{7}$ $\boxed{0''}$

\boxed{ENT} $\rightarrow 38.70785818$ \boxed{INV} $\boxed{0''}$ $\rightarrow 38^{\circ}42'28.29$ ($=38^{\circ}42'5$ $\rightarrow 28.29/60$)

$\dot{=} 0.47 \dot{=} 0.5$) \boxed{ENT} $\rightarrow -38.8519671 \dot{=} 38^{\circ}9$ or $141^{\circ}1$ ($= 180^{\circ}-38^{\circ}9$)

See "Sight Reduction Tables" page 251, Vol.1, Pub. No.229

Example 4

when Lat. = $15^{\circ}08.0$ S

α Pavonis Dec. = $56^{\circ}50'0$ S, LHA = $293^{\circ}27'5$

Vega Dec. = $38^{\circ}44'9$ N, LHA = $321^{\circ}06'3$

Jupiter Dec. = $12^{\circ}08'6$ S, LHA = $27^{\circ}45'0$

Required:- Ac and Z of aforementioned celestial bodies.

Solution

1) α Pavonis

(MODE $\boxed{\cdot}$) $\boxed{P_1}$ $\boxed{1}$ $\boxed{5}$ $\boxed{0''}$ $\boxed{8}$ $\boxed{0''}$ \boxed{ENT} $\boxed{5}$ $\boxed{6}$ $\boxed{0''}$ $\boxed{5}$ $\boxed{0}$ $\boxed{0''}$ $\boxed{2}$ $\boxed{9}$ $\boxed{3}$

$\boxed{0''}$ $\boxed{2}$ $\boxed{7}$ $\boxed{\cdot}$ $\boxed{5}$ $\boxed{0''}$ \boxed{ENT} $\rightarrow 25.38906874$ \boxed{INV} $\boxed{0''}$ $\rightarrow 25^{\circ}23'20.65$

($= 25^{\circ}23'3$ $\rightarrow 20.65/60 = 0.3$) \boxed{ENT} $\rightarrow -33.7460874$ \boxed{INV} $\boxed{0''}$

$\rightarrow 33^{\circ}44'045.9$ ($= 33^{\circ}44'8$ $\rightarrow 45.9/60 = 0.765 \dot{=} 0.8$)

Ans. Ac = $25^{\circ}23'3$, Z = S $33^{\circ}44'8$ E.

2) Vega \rightarrow Be careful when Lat. and Dec. are of contrary name.

$\boxed{1}$ $\boxed{5}$ $\boxed{0''}$ $\boxed{8}$ $\boxed{0''}$ \boxed{ENT} $\boxed{3}$ $\boxed{8}$ $\boxed{0''}$ $\boxed{4}$ $\boxed{4}$ $\boxed{\cdot}$ $\boxed{9}$ $\boxed{0''}$ $\boxed{+/-}$ \boxed{ENT}

$\boxed{3}$ $\boxed{2}$ $\boxed{1}$ $\boxed{0''}$ $\boxed{6}$ $\boxed{\cdot}$ $\boxed{3}$ $\boxed{0''}$ \boxed{ENT} $\rightarrow 24.99537237$ \boxed{INV} $\boxed{0''}$ $\rightarrow 24^{\circ}59'$

43.34 ($= 24^{\circ}59'7$ $\rightarrow 43.34/60 \dot{=} 0.722 \dot{=} 0.7$) \boxed{ENT} $\rightarrow -32.7041063$

INV 01" → -32°42'14.7 (= -32°42'2 → 14.7/60 ÷ 0.245 ÷ 0.2)

Ans. Ac = 24°59'7, Z = N 32°42'2 E.

3) Jupiter

1 5 01" 8 01" ENT 1 2 01" 8 . 6 01" ENT 2 7 01"

4 5 01" ENT → 62.8856946 INV 01" → 62°53'08.5 (= 62 53'1 → 8.5/60 = 0.1416 --- ÷ 0.1)

ENT → 87.13158594 INV 01" → 87°7'53.71 (= 87°7'9 → 53.71/60 = 0.8951 --- ÷ 0.9)

Ans. Ac = 62°53'1, Z = N 87°7'9 W

See "Astronomical Navigation Tables" page XXIII - XXIV, Pub. No.601 Maritime Safety Agency, Japan.

•X: The most important Example is No.4.

Computation by programmable calculators: CASIO fx-4000 P. fx-7000 G and fx-8000 G.

1) Formulae

$$Ac(Hc) = \sin^{-1} \{(\cos Lat \times \cos Dec \times \cos LHA) + \sin Lat \times \sin Dec\}$$

$$Z = \sin^{-1} (\sin LHA \times \cos Dec + \cos Ac)$$

$$a = \sin^{-1} (\sin Dec + \sin L)$$

When Dec & Lat are of the same names and, Lat > Dec,

Ac(Hc) > a ... Prefix of Z is contrary name to Latitude,

Ac(Hc) < a ... Prefix of Z is the same name as Latitude.

Note: Ac(Hc) = Calculated Altitude (Degree & minute), Z = Azimuth (Degree) and, a = Altitude in Prime vertical (Degree and minute)

2) Program

Lb 0 : " LAT = " : ? → L

: " DEC = " : ? → D

: " LHA = " : ? → H

: $\sin^{-1} ((\cos L \times \cos D \times \cos H) + \sin L \times \sin D)$ ▲
? → A

: $\sin^{-1} (\sin H \times \cos D + \cos A)$

L > 0 ⇒ D > 0 ⇒ L > D ⇒ $\sin^{-1} (\sin D + \sin L)$ ▲
Goto 0

3) Keystrokes of Program

Switch on **MODE** **2** **EXE**

SHIFT **Lb%** **0** **:** **ALPHA** **"** **ALPHA** **L** **ALPHA** **A** **ALPHA** **T** **SHIFT** **=**

ALPHA **"** **:** **SHIFT** **?** **→** **ALPHA** **L**

: **ALPHA** **"** **ALPHA** **D** **ALPHA** **E** **ALPHA** **C** **SHIFT** **=**

ALPHA **"** **:** **SHIFT** **?** **→** **ALPHA** **D**

: **ALPHA** **"** **ALPHA** **L** **ALPHA** **H** **ALPHA** **A** **SHIFT** **=**

ALPHA **"** **:** **SHIFT** **?** **→** **ALPHA** **H**

: **SHIFT** **sin⁻¹** **(** **(** **cos** **ALPHA** **L** **x** **cos** **ALPHA** **D** **x**

cos **ALPHA** **H** **)** **+** **sin** **ALPHA** **L** **x** **sin** **ALPHA** **D** **)**

SHIFT **▲** **SHIFT** **?** **→** **ALPHA** **A**

: **SHIFT** **sin⁻¹** **(** **sin** **ALPHA** **H** **x** **cos** **ALPHA** **D** **+** **cos**

ALPHA **A** **)** **SHIFT** **▲**

ALPHA **L** **SHIFT** **>** **0** **SHIFT** **⇒** **ALPHA** **D** **SHIFT**

> **0** **SHIFT** **⇒** **ALPHA** **L** **SHIFT** **>** **ALPHA** **D**

SHIFT **⇒** **SHIFT** **sin⁻¹** **(** **sin** **ALPHA** **D** **+** **sin**

ALPHA **L** **)** **SHIFT** **▲** **SHIFT** **Goto** **0**

Example 1

when Lat. = 38°N, Dec. = 19°S, and LHA = 340°

Required:- Ac(=Hc) and Z

Solution

MODE 1 Prog 0 EXE 3 8 0" EXE (-) 1 9 0" EXE 3 4 0 0"

EXE → 29.98050372 SHIFT 0" → 29°58'49.81" (= 29°58'8

→ 49"81/60 = 0.830 --- ÷ 0'8) EXE ANS EXE → -21.92182127 ÷ -21°9

or 158°1 (= 180° - 21°9)

Ans Ac(=Hc) = 29°58'8, = S 21°9 E or 158°1

See "Sight Reduction Tables" page 225, Vol. 3, Pub. No. 229

Example 2

when Lat. = 45°S, Dec. = 40°N, LHA = 320°

Required:- Ac(= Hc) and Z

Solution

MODE 1 Prog 0 EXE 4 5 0" EXE (-) 4 0 0" EXE 3 2 0 0"

EXE — -2.267911364 SHIFT 0" — -2°16'4.48" (= -2°16.1

— 4.48"/60 = 0.074 --- ÷ 0.1) EXE ANS EXE — -29.52411728 ÷ 29°5

Ans. Ac(= Hc) = 2°16'1, Z = N 29°5 E or 29°5

See "Sight Reduction Tables" page 265, Vol.3, Pub. No. 229

Example 3

when Lat. = $52^{\circ}28'2''$ N.

Sun : Dec. = $11^{\circ}09'0''$ S, LHA = $323^{\circ}30'7''$

Moon : Dec. = $20^{\circ}16'3''$ N, LHA = $39^{\circ}44'0''$

Required:- Ac and Z

Solution

1) Sun

MODE 1 Prog 0 EXE 5 2 0'' 2 8 . 2 0'' EXE (-) 1 1 0'' 9

0'' EXE 2 0 0'' 1 6 . 3 0'' EXE → 19.09675689

SHIFT 0'' → $19^{\circ}05'48.32''$ (= $19^{\circ}05'8''$ → $48.32''/60 = 0.805 \approx \underline{0.8}$)

EXE ANS EXE → -38.12740902 SHIFT 0'' → $38^{\circ}07'38.67''$

(= $-38^{\circ}07'6''$ → $38.67''/60 = 0.6445 \approx \underline{0.6}$)

2) Moon

EXE 5 2 0'' 2 8 . 2 0'' EXE 2 0 0'' 1 6 . 3 0''

EXE 3 9 0'' 4 4 0'' EXE → 45.57938213

SHIFT 0'' → $45^{\circ}34'45.78''$ (= $45^{\circ}34'8''$ → $45.78/60 = 0.763 \approx \underline{0.8}$)

EXE ANS EXE → 58.94817624 SHIFT 0'' → $58^{\circ}56'53.43''$ (= 58°)

$56'9''$ → $53.43/60 = 0.8905 \approx \underline{0.9}$ EXE → 25.90585779

SHIFT 0'' → $25^{\circ}54'21.09''$ ($\approx 25^{\circ}54.3$), Ac(Hc) > a

Ans. 1) Sun : Ac = $19^{\circ}05'8''$ = S $38^{\circ}07'6''$ E

2) Moon: Ac = $45^{\circ}34'8''$ = S $58^{\circ}56'9''$ W

Be careful of prefix South!

See "Astronomical Navigation Tables" page XXI, Pub. No.601,
Maritime Safety Agency, Japan.

Example 4

Required: Ac(= Hc) and Z

when

- 1) Lat. = 15°N, Dec. = 30°S and LHA = 315°. (L & D, contrary names)
- 2) Lat. = 15°N, Dec. = 9°S and LHA = 315°. (L & D, contrary names)
- 3) Lat. = 21°N, Dec. = 19°N and LHA = 315°. (L & D, same names)

Solution

1) MODE 1 Prog 0 EXE
1 5 0'' EXE (-) 3 0 0'' EXE 3 1 5 0''
EXE → 27.52249499 SHIFT 0'' → 27°31'20.98" (= 27°31'!3)
 → 20.98/60 = 0.34 --- ÷ 0.3)
EXE Ans EXE → -43.67119127 ÷ -43°07

2) EXE 1 5 0'' EXE (-) 9 0'' EXE 3 1 5 0''
EXE → 39.35441086 SHIFT 0'' → 39°21'05.88"
 (= 39°21'!3 → 15.88/60 = 0.26 --- ÷ 0.3)
EXE Ans EXE → -64.58404476 ÷ -64°06

3) EXE 2 1 0'' EXE 1 9 0'' EXE 3 1 5 0''
EXE → 47.80377208 SHIFT 0'' → 47°48'13.58"
 (= 47°48'!2 → 13.58/60 = 0.22 --- ÷ 0.2)
EXE Ans EXE → -84.5026916 ÷ -84°05 EXE → 65.2953868
SHIFT 0'' → 65°17'43.39" (÷ 65°17'!7) --- Ac(Hc) < a.

Ans. See "Sight Reduction Tables" page 92, 93 Vol. 2, Pub. No. 229

1) $Ac(Hc) = 27^{\circ}31'.3$, $Z = S 43^{\circ}.7 E$ or $136^{\circ}.3 (= 180^{\circ} - 43^{\circ}.7)$

Note: Ship's latitude \rightarrow North, Declination \rightarrow South
So prefix of Z is South.

$360^{\circ} > LHA (315^{\circ}) > 180^{\circ}$ so suffix of Z is East.

2) $Ac(Hc) = 39^{\circ}21'.3$, $Z = S 64^{\circ}.6 E$ or $115^{\circ}.4$

3) $Ac(Hc) = 47^{\circ}48'.2$, $Z = \underline{N} 84^{\circ}.5 E$ or $84^{\circ}.5$

Note: When Latitude and Declination are of the same names and, the value of Latitude is greater than that of Declination, there is some probability that the celestial body is located in the Prime Vertical. So to name prefix of Z (Azimuth) should be carefully considered by following procedures.

$a = \sin^{-1} (\sin D \div \sin L)$ $a =$ Altitude in Prime Vertical

when, $Ac(Hc) > a$, Prefix of Z is contrary name to Latitude.

$Ac(Hc) < a$, Prefix of Z is the same name as Latitude.

See "Navigation Tables"

In the case of calculation 3),

$a = \sin^{-1} (\sin 19^{\circ}N \div \sin 21^{\circ}N) = 65^{\circ}17'.7$ is greater than the value of $Ac(Hc) = 47^{\circ}48'.2$, so prefix of Z is the same name as Latitude $21^{\circ}N$

Example 5

when Lat. = $21^{\circ}N$, Dec. = $13^{\circ}N$ and LHA = 300°

Required:- $Ac(Hc)$ and Z

Solution

MODE | 1 | Prog | 0 | EXE

2 | 1 | 0' " | EXE | 1 | 3 | 0' " | EXE | 3 | 0 | 0 | 0' "

EXE \rightarrow 32.37386856 SHIFT | 0' " \rightarrow $32^{\circ}22'25.93'' (= 32^{\circ}22'.4)$

EXE Ans EXE → -87.59651094 ÷ -87.6 Z = N 87°6 E

Lat. and Dec. → same names and value of Lat. > value of Dec., so check the Altitude in Prime Vertical by making use of the formula

$$a = \sin^{-1} (\sin D + \sin L)$$

EXE → 38.8813531 SHIFT 0" → 38°52'52.87" ≐ 38°52'9

$$Ac(Hc) = 32°22'4 < a = 38°52'9$$

so prefix of Z is the same name as Latitude (N)

See "Sight Reduction Tables" page 122, Vol. 2, Pub. No.229

Example 6

when Lat. = 22°N, Dec. = 8°N and LHA = 14°

Required:- Ac(Hc) and Z

Solution

MODE 1 Prog 0 EXE

2 2 0" EXE 8 0" EXE 1 4 0" EXE

→ 70.56549201 SHIFT 0" → 70°33'55.77" ≐ 70°33'9

EXE Ans EXE → 46.05511009 = 46°1

Lat. and Dec. are of the same name and value of Lat. > value of Dec. so Altitude in Prime Vertical should be computed to decide the prefix of Z.

EXE → 21.80926819

SHIFT 0" → 21°48'33.37" = 21°48'6

$$AC(Hc) = 70°33'9 > a = 21°48'6$$

So prefix of Z is contrary name to Lat.

$$Z = S 46^{\circ}.1 W \text{ or } \underline{226^{\circ}.1}$$

↑
Because of LHA < 180°

In the case of "Sight Reduction Tables" page 30, Vol.2, Pub. No. 229

$$Z = 133^{\circ}.9, Z_n = 360^{\circ} - Z = 360^{\circ} - 133^{\circ}.9 = \underline{226^{\circ}.1}$$

Because of N. Lat. $\left\{ \begin{array}{l} \text{LHA greater than } 180^{\circ} \text{ --- } Z_n = Z \\ \text{LHA less than } 180^{\circ} \text{ --- } Z_n = 360^{\circ} - Z \end{array} \right\}$

Example 7

Required:- Ac(Hc) and Z

- when 1. Sun : Lat. = $52^{\circ}28'.2 N$, Dec. = $11^{\circ}09'.0 S$, LHA = $323^{\circ}30'.7$
 2. Moon: Lat. = $52^{\circ}28'.2 N$, Dec. = $20^{\circ}16'.3 N$, LHA = $39^{\circ}44'.0$

Solution

In this case, each Ac(Hc) and Z can be computed continuously by the calculator.

MODE 1 Prog 0 EXE 5 2 0" 2 8 . 2 0" EXE (-) 1 1

0" 9 0" EXE 3 2 3 0" 3 0 . 7 0" EXE

→ 19.09675691 SHIFT 0" → $19^{\circ}05'48.32'' = \underline{19^{\circ}05'.8}$ EXE Ans EXE

→ $-38.12740902 = \underline{-38^{\circ}.1}$

EXE 5 2 0" 2 8 . 2 0" EXE 2 0 0" 1 6 . 3 0"

EXE 3 9 0" 4 4 0" EXE → 45.57938213 SHIFT 0"

→ $45^{\circ}34'45.78'' = \underline{45^{\circ}34'.8}$ EXE Ans EXE → $58.94817624 \div \underline{58^{\circ}.9}$

EXE → 25.90585779 SHIFT 0" → $25^{\circ}54'21.09''$ --- Ac(Hc) > a.

Ans. Sun Ac(Hc) = $19^{\circ}05'.8$, Z = S $38^{\circ}.1$ E.
 Moon Ac(Hc) = $45^{\circ}34'.8$, Z = S $58^{\circ}.9$ W.

Example 8

Required:- Ac(Hc) and Z

- when 1. α Pavonis : Lat. = $15^{\circ}08'0''$ S, Dec. = $56^{\circ}50'0''$ S, LHA = $293^{\circ}27'5''$
- 2. Vega : Lat. = $15^{\circ}08'0''$ S, Dec. = $38^{\circ}44'9''$ N, LHA = $321^{\circ}06'3''$
- 3. Jupiter : Lat. = $15^{\circ}08'0''$ S, Dec. = $12^{\circ}08'6''$ S, LHA = $27^{\circ}45'0''$

Solution

By continuous keystrokes

MODE 1 Prog 0 EXE

(α Pavonis)

1 5 01" 8 01" EXE 5 6 01" 5 0 01" EXE 2 9 3 01"

2 7 . 5 01" EXE \rightarrow 25.38906872 SHIFT 01"

$\rightarrow 25^{\circ}23'20.65'' \div 25^{\circ}23'3''$ EXE Ans EXE $\rightarrow -33.74608747 \div -33^{\circ}7'$

(Vega)

EXE 1 5 01" 8 01" EXE (-) 3 8 01" 4 4 . 9 01" EXE

3 2 1 01" 6 . 3 01" EXE \rightarrow 24.99537237 SHIFT

01" $\rightarrow 24^{\circ}59'43.34'' = 24^{\circ}59'7''$ EXE Ans EXE $\rightarrow -32.70410639 \div -32^{\circ}7'$

(Jupiter)

EXE 1 5 01" 8 01" EXE 1 2 01" 8 . 6 01" EXE 2 7 01"

4 5 01" EXE \rightarrow 62.88569458

SHIFT 01" $\rightarrow 62^{\circ}53'08.5'' \div 62^{\circ}53'1''$

EXE Ans EXE $\rightarrow 87.13158511 = 87^{\circ}1'$

EXE → 53.68421517 SHIFT 0" → 53°41'3.17" --- Ac(Hc) > a.

- Ans. 1. α Pavonis Ac(Hc) = 25°23'3, Z = S 33°7 E.
 2. Vega Ac(Hc) = 24°59'7, Z = N 32°7 E.
 3. Jupiter Ac(Hc) = 62°53'1, Z = N 87°1 W.

Example 8

Required:- Ac(Hc) and Z

- when 1. Sun : Lat. = 29°57'5 N, Dec. = 10°59'3 S, LHA = 66°33'2
 2. Moon : Lat. = 29°57'5 N, Dec. = 24°16'1 N, LHA = 347°59'2

- Ans. 1. Sun : Ac(Hc) = 14°04'6, Z = S 68°2 W
 2. Moon : Ac(Hc) = 77°53'9, Z = S 64°8 E ---
 Ac(Hc) 77°53'9 > a 55°23'5

Example 9

Required:- Ac(Hc) and Z

1. Antares : Lat. = 13°42'0 N, Dec. = 26°20'0 S,
 LHA = 16°46'8
 2. Arcturus: Lat. = 13°42'0 N, Dec. = 19°25'4 N,
 LHA = 50°37'0

- Ans. 1. Antares : Ac(Hc) = 46°46'1, Z = S 22°2 W
 2. Arcturus: Ac(Hc) = 41°18'6, Z = N 76°0 W

The important review of Prefix and Suffix of Z

1) Prefix

1. Dec. and Lat. are of contrary names, Prefix of Z is contrary name to Lat.
 2. Dec. and Lat. are of the same names and, Lat. < Dec., Prefix of Z is the same name as Lat.

- 3. Dec. and Lat. are of the same names and, Lat. > Dec.,
when Ac(Hc) > Altitude in Prime Vertical

$$\{a = \sin^{-1}(\sin D \div \sin L)\}$$

Prefix of Z is contrary name to Lat.

Ac(Hc) < Altitude in Prime Vertical

$$\{a = \sin^{-1}(\sin D \div \sin L)\}$$

Prefix of Z is the same name as Lat.

- 4. when $180^\circ < LHA < 360^\circ$, Suffix is E.
 $0^\circ < LHA < 180^\circ$, Suffix is W.



1) Formula

$$\text{Advancing distance} = D \div T \times A$$

Note: D = Distance travelled (nautical mile), T = Time elapsed (minute) and, A = Advancing time (minute)

2) Program

```
Lbl 1 : " DST = " : ? → D
      : " ETM = " : ? → T
      : " ATM = " : ? → A
      : D ÷ T x A ▲ Goto 1
```

3) Keystrokes of Program

Switch on MODE 2 ⇒ EXE

SHIFT Lbl 1 : SHIFT ALPHA " D S T ALPHA SHIFT = ALPHA
" : SHIFT ? → ALPHA D : SHIFT ALPHA
" E T M ALPHA SHIFT = ALPHA " : SHIFT
? → ALPHA T : SHIFT ALPHA " A T M
ALPHA SHIFT = ALPHA " : SHIFT ? →
ALPHA A : ALPHA D ÷ ALPHA T SHIFT ▲
SHIFT Goto 1

1) Formula

$$\text{Amplitude} = \sin^{-1} \left(\frac{\sin D - \sin L \times \sin C}{\cos L \times \cos C} \right)$$

Note: D = Declination, L = Latitude and, C = Constant (0° or 0.7°)
 when the centre of the sun is on the celestial horizon, C = 0°
 when the centre of the sun is on the visible horizon, C = 0.7°

2) Program

Lbl 2 : " DEC = " : ? → D
 : " LAT = " : ? → L
 : " [0°] or [0.7°] = " : ? → C

$$: \sin^{-1} \left(\frac{\sin D - \sin L \times \sin C}{\cos L \times \cos C} \right) \blacktriangle \text{Goto 2}$$

3) Keystrokes of Program

Switch on **MODE** **2** **⇒** **⇒** **EXE**

SHIFT **Lbl** **2** **:** **SHIFT** **ALPHA** **"** **D** **E** **C** **ALPHA**

SHIFT **=** **ALPHA** **"** **:** **SHIFT** **?** **→** **ALPHA** **D** **:**

SHIFT **ALPHA** **"** **L** **A** **T** **ALPHA** **SHIFT** **=** **ALPHA**

" **:** **SHIFT** **?** **→** **ALPHA** **L** **:** **ALPHA** **"** **ALPHA**

' **0** **'** **"** **ALPHA** **.** **SHIFT** **ALPHA** **O** **R** **'** **ALPHA**

0 **.** **7** **'** **"** **ALPHA** **.** **SHIFT** **=** **ALPHA** **"** **:**

SHIFT **?** **→** **ALPHA** **C** **:** **SHIFT** **sin⁻¹** **(** **(** **sin**

ALPHA **D** **-** **sin** **ALPHA** **L** **x** **sin** **ALPHA** **C** **)**

+ **cos** **ALPHA** **L** **x** **cos** **ALPHA** **C** **)** **SHIFT** **▲**

SHIFT **Goto** **2**

Assumptions to observe true amplitude are;

1. Sun's lower limb is about two-thirds of a diameter above the visible horizon, its center is on the celestial horizon.
2. Moon's upper limb is on the visible horizon, its center is on the celestial horizon.
3. When planets or stars are on the celestial horizon, they are about one sun diameter, or some 32'.0 above the visible horizon.

* To check compass error, true amplitude of the sun is most desirable

Example 1

when GMT is 20h 03m 13s (Local apparent time 05h 08m, 20 June '79), 19 June 1979 in D.R.P. 27°30'N, 136°30'E, and the sun, when its lower limb is 1/2 of its diameter above the horizon, bears 068° by gyro.

Required:- The gyro error

Solution

From Nautical Almanac Dec. of the sun = N 23°25'.4 and by D.R.P., Lat. = 27°30'N

MODE 1 Prog 2 EXE 2 3 01" 2 5 . 4 01" EXE 2 7 01"

3 0 01" EXE 0 EXE → 26.62560823

Amplitude E 26°6 N = N 63°4 E or 63°4

True Azimuth = N 63°4 E	(Prefix & Suffix See "Celestial Navigation" text - TD/TRB/37, page 114-115)
Gyro Azimuth = N 68°0 E 0	
Gyro error = 4°6 W	Ans. 4°6 W

(From "Celestial Navigation", Prof. K. HASEGAWA 1983, Tokyo)

Example 2

Required:- True Amplitude

- when
- 1) Dec. = 18° Lat. = 25°
 - 2) Dec. = 19°5 Lat. = 30°
 - 3) Dec. = 21°0 Lat. = 38°
 - 4) Dec. = 23°5 Lat. = 42°

Solution

MODE 1 Prog 2 EXE

1) 1 8 0' " EXE 2 5 0' " EXE 0 EXE → 19.93552733 ≐ 19°9

2) EXE 1 9 . 5 0' " EXE 3 0 0' " EXE 0 EXE → 22.67149089 ≐ 22°7

3) EXE 2 1 0' " EXE 3 8 0' " EXE 0 EXE

4) EXE 2 3 . 5 0' " EXE 4 2 0' " EXE 0 EXE → 32.45043401 ≐ 32°5

See Figure 2805 a. Table 27, Amplitudes, from Bowditch. Vol. II.

Altitude and Azimuth

The altitude (H_C) and Azimuth (A_Z) of a celestial body can be computed by the following formula:

$$(1) \sin H = \sin \phi \sin S + \cos \phi \cos S \cos LHA$$

$$(2) x = \tan A = \sin LHA + (\cos LHA \sin \phi - \tan S \cdot \cos \phi)$$

Since computers and calculators normally give the arc tangent in the range -90° to $+90^\circ$, the correct Azimuth of body measured eastward from north over the range 0° to 360° can be selected according to the following rules:

If $0^\circ \leq LHA \leq 180^\circ$

$$A = 180^\circ + \tan^{-1} x, \text{ if } x \text{ is positive}$$

$$A = 360^\circ + \tan^{-1} x, \text{ if } x \text{ is negative}$$

If $180^\circ \leq LHA \leq 360^\circ$

$$A = \tan^{-1} x, \text{ if } x \text{ is positive}$$

$$A = 180^\circ + \tan^{-1} x, \text{ if } x \text{ is negative}$$

Standard navigational notation

H_C = H computed altitude of the body above (if $\sin H > 0$) or below (if $\sin H < 0$) the horizon;

Z_n = True Azimuth of the body measured eastward from north over the range 0° to 360°

O = Latitude of observer (+ north, - south)

S = Declination of the body (+ north, - south)

LHA = Local hour angle of the body

The equation (1) and (2) are basic formulae used in preparing sight reduction tables; they do not include the effect of refraction.

Example 3 On 25 April 1978, the 1056 DR position of a ship is Lat. $32^{\circ}41.6' N$, Long. $62^{\circ}14.5' W$. At watch time $10^h - 56^m - 27^s$ the navigator observed the lower limb of the Sun with a marine sextant having an IC (+) 1.6, height of eye 42 ft., the observed sextant altitude is $64^{\circ} 10.2'$, watch error is 10^s faster than Zone time.

Required: a. True azimuth (Z_n) b. Intercept (a) c. Assume position (AP.) Solution.

	Sun \odot		d(+) 0.8		\odot
W	10 -56 -27 April 25	14 ^h	$13^{\circ}08.2' N$	h_s	$64^{\circ}10.2'$
WE (F)	10 \ominus	corr.	+ 0.8	I_c	+ 1.6
ZT	10 -56 -17	dec.	$13^{\circ}09.0' N$	D	- 6.3
ZD (+)	4	See page		\odot	+ 15.5
GMT	14 -56 -17 April 25			H_o	$64^{\circ}21.0'$
14 ^h	$30^{\circ} 29.6'$) By the table or calculation			
$56^m 17^s$	$14^{\circ} 04.3'$				
GHA \odot	$44^{\circ} 33.9'$				<u>By Computer</u>
a	$62^{\circ} 33.9' W$	Ap aL $33^{\circ} N$	Z_n $136^{\circ} 2'$ (136.18277...)		
LHA \odot	342°	aλ $62^{\circ} 33.9' W$	a $6.7' T.$ (-6.6688..)		

Explanation of Solution

1. Converting the time of observation to Greenwich mean time (GMT).
2. At GMT find LHA, and dec, by using nautical Almanac.
3. Correct the observed sextant altitude to get H_o (True altitude).
4. Assume position should be within 30.0 of the DR position.
5. Compute the result by using Prg. ϕ .

PROGRAM SHEET

Program for	Compute azimuth and intercept		No	Prg	Ø
<p>Description Input Lat = Assume latitude of Observer (+N, -S) Dec.= Corrected declination of body (+N,-S) LHA = local hour angle of body HO = Corrected sextant altitude of body Output ZN = true azimuth of the body in degrees INCEPT+A-T = Intercept (a) in minutes when result is positive (+A) = away result is negative (-T) = toward</p>					
<p>Example 1. a lat 33° N Dec 13°12.7 N LHA 20 HO 63°02.5 2. " 33° S " 7°36.3 N " 301 " 20°32.5 3. " 17° N " 22°54.7 S " 334 " 42°51.2 4. " 21° S " 18°40.9 S " 323 " 54°57.4</p> <p>Answer 1. ZN 227°36 a 2. 84 (A) 3. ZN 146.68 a -10.48 (T) 4. ZN 092.80 a 14.28 (A)</p>					
<p>Preparation and operation 4. ZN 092.80 a 14.28 (A)</p> <ul style="list-style-type: none"> ● Store the program written on the next page. ● Execute the program as shown below in the RUN mode (MODE II). 					

Step	Key operation	Display	Step	Key operation	Display
1	Prg Ø <input type="checkbox"/> EXE	INCEPT	11	<input type="checkbox"/>	
2	<input type="checkbox"/> EXE	LAT+N-S?	12	<input type="checkbox"/>	
3	(-) 3300.0 <input type="checkbox"/> EXE	DEG+N-S?	13	<input type="checkbox"/>	
4	736.3 <input type="checkbox"/> EXE	LHA?	14	<input type="checkbox"/>	
5	30100 <input type="checkbox"/> EXE	HO?	15	<input type="checkbox"/>	
6	2032.5 <input type="checkbox"/> EXE	ZN	16	<input type="checkbox"/>	
7	<input type="checkbox"/> EXE	65.39751078	17	<input type="checkbox"/>	
8	<input type="checkbox"/> EXE	INCEPT+A-T	18	<input type="checkbox"/>	
9	<input type="checkbox"/> EXE	19.037628	19	<input type="checkbox"/>	
10	EXE <input type="checkbox"/> EXE	INCEPT	20	<input type="checkbox"/>	

(repeat again)

	No	Prg	Ø
--	----	-----	---

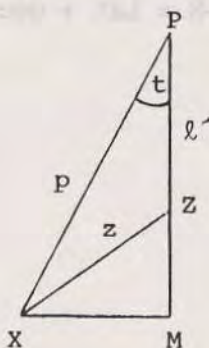
Line	MODE [2]	Program	Notes	Number of steps
1	"	I N C E P T " ▲ Prg 7 : Prg 8 :		
2	Prg 9 :	SIN (SIN L x SIN D + COS L x COS		
3	D x COS H) → R :	Prg 6 : (R - S		
4) x 6 Ø → I :	" I N C E P T +		
5	A - T " ▲ I ▲			
6				
7				

Ex-Meridian (Reduction formula)

=====

The meridian zenith distance of the body is the least zenith distance and is smaller than the zenith distance obtained from an observation taken a few minutes before or after the body has crossed the meridian by a small quantity called "Reduction".

Derivation of reduction formula:



- P = Pole
- Z = Zenith
- X = The body a few minutes before or after crossing the meridian
- M = The body on the meridian
- Z = ZX, observed zenith distance
- ZM = Mer. zenith distance
- ρ = Co-declination of the body = 90-Dec. (d)
- l' = Co-latitude of observer = 90-Lat. (l)
- t = Meridian angle

From spherical triangle P x z

$$\begin{aligned} \cos t &= (\cos z - \cos p \cos l') / \sin p \sin l' \\ &= (\cos z - \sin d \sin l) / \cos d \cos l \quad \dots \text{Eq 1} \end{aligned}$$

When body is on meridian $t = 0^\circ$, $\cos t = 1$ if R = reduction,

$$1 = (\cos (z-R) - \sin d \sin l) / \cos d \cos l \quad \dots \text{Eq 2}$$

$$2-1 \text{ then } 1 - \cos t = \{ \cos (z-R) - \cos z \} / \cos d \cos l \quad \dots \text{Eq 3}$$

$$\therefore \cos A = 1 - 2 \sin^2 \frac{A}{2} \text{ and } \cos B - \cos A = 2 \sin \frac{1}{2} (A+B)$$

$\sin \frac{1}{2} (A-B)$: then Eq 3 becomes

$$2 \sin^2 \frac{t}{2} = 2 \sin \frac{1}{2} \{(z + z + R) \sin \frac{1}{2} (z + z + R)\} / \cos d \cos \ell$$

$$\sin^2 \frac{t}{2} = \left\{ \sin (z + \frac{B}{2}) \cdot \sin \frac{R}{2} \right\} / \cos d \cos \ell \quad \dots \text{Eq 4}$$

Since R is very small so $z - \frac{R}{2} = z - R$

$$\therefore \sin \frac{R}{2} = \cos d \cos \ell \sin^2 \frac{t}{2} / \sin (z - R) \quad \dots \text{Eq 5}$$

When the body is nearly crossing the meridian, t is small, the chord and the subtended arc of the circle are nearly equal then:

$$\sin \theta'' = \theta'' \sin 1'', \quad \sin^2 \frac{t}{2} = \frac{\sin^2 t}{4}, \quad z - R = \text{Lat} + \text{dec.}$$

So Eq5 may be written

$$\frac{R''}{2} \sin 1'' = \frac{\cos d \cos \ell}{\sin (\ell \pm d)} \times \frac{\sin^2 t}{4}$$

$$R'' = \frac{\cos d \cos \ell}{\sin (\ell \pm d)} \times \frac{2 \sin^2 t}{4 \sin 1''}$$



Converting t° to t in minutes of time $\sin^2 t = t^2 \sin^2 15'$

$$\therefore R'' = \frac{\cos d \cos \ell}{\sin (\ell \pm d)} \times \frac{\sin^2 15'}{2 \sin 1''} \times t^2$$

$\frac{\sin^2 15'}{2 \sin 1''}$ is constant = 1.9635 then

$$R'' = \frac{1.9635 \times \cos d \times \cos L \times \text{cosec} (\ell \pm d) \times t^2}{A}$$

Let C = Reduction in minutes

$$\therefore C' = \frac{A \times t^2}{60}$$

These are the formula used in the computation of Ex-meridian tables:

A for table I of Nories or table 29 of Bowditch

C' for table II of Nories or table 30 of Bowditch

by using an electronic calculator or computer, in order to get correct reduction for both upper and lower transit, the formula and condition may be written as follows:

$$R = \frac{.008726 \times \cos D \cos L \times t^2 \times I}{\sin \text{ abs } (L - D \times I)} \quad \dots \text{Eq6}$$

where R = reduction in degrees I is for setting condition
L = Lat (+N, -s) I = -1 for lower transit
D = dec (+N, -s) I = 1 for upper transit
t = meridian angle in degrees

if we know the reduction then we can find the latitude of observer by the following procedure:

1. True Meridian altitude = Corrected Sextant altitude ± Reduction

$$\text{T. Mer. Alt.} = H_0 \pm R$$

2. True Meridional zenith distance = 90 - True meridian altitude

$$\text{T. MZD} = 90 - \text{T. Mer. Alt.}$$

3. By the same procedure as latitude by meridian transit, the latitude of observer at the time of Ex-meridian observation can be obtained.
-

Example : At DR. Lat. $48^{\circ}12'$ N, Long. $24^{\circ}32'$ W, the true altitude of Antares was $21^{\circ}28'$ Hour angle $357^{\circ}00'$ Dec. $26^{\circ}18'0$ S, Determine the Lat. and position line.

<u>By table</u>	Table I	Table II	T. Alt.	$21^{\circ}28'0$
	Lat. $42^{\circ}12'$ N	LHA $357^{\circ}00'$	Reduction	<u>3.4</u>
	Dec. $26^{\circ}18'$ S	A = $1''4$		
	A = $1''4$	Red. for $1'' = 2.4$	T. Mer. Alt.	$21^{\circ}31'4$
		" for $4 = 0.96$	T. MZD.	$18^{\circ}28'6$
		Reduction = 3.36	Dec.	<u>$26^{\circ}18'0$ S</u>
			Lat.	<u>$42^{\circ}10'6$ N</u>
			True Azimuth	177° (from AZ table)

Position line passes 087° and 267° through Lat. $42^{\circ}10'6$ N Long. 2432 W.

<u>By program</u>	Lat. $42^{\circ}12'$ N		using Prg. 1→T. MZD	$68^{\circ}47727667$
	Dec. $26^{\circ}18'$ S		= $68^{\circ}28'63$	
	LHA $357^{\circ}00'$		Dec. = $26^{\circ}18'5$	
	Ho $21^{\circ}28.0$		Lat. = $42^{\circ}10'63$ N	
			using Prg. 2→ZN	$177^{\circ}1106136$
			= $177^{\circ}1106136$	
			= 177°	
			direction of position line = $ZN \pm 90$	
			= <u>$177^{\circ} \pm 90^{\circ} = 267^{\circ}$ or 087°</u>	

PROGRAM SHEET

Program for Compute true meridional zenith distance by EX-MERIDIAN (Reduction formula) No Prg. 1

Description Input Lat = DR. Latitude of observer (+N, -S)
 Dec = Corrected declination of body (+N, -S)
 LHA = Local hour angle of body
 HO = Corrected sextant altitude of body
 Output T.MZD = True meridional zenith distance (degrees)

Example

1. DR. Lat 48°13'N Dec 21°39'S LHA 356°00' HO 19°52'0
2. " 42°10'N " 62°01'N " 176°30' HO 14°20'0
3. " 50°02'S " 57°29'S " 184°20' HO 17°20'

Anwer 2. T.MZD 75°70501092, 3. T.MZD 72.72599481

Preparation and operation

• Execute the program as shown below in the RUN mode (MODE II).

Step	Key operation	Display	Step	Key operation	Display
1	Prg 1 [EXE]	X-MER	11	[]	
2	[EXE]	LAT+N-S?	12	[]	
3	4813.0 [EXE]	DEC+N-S?	13	[]	
4	(-) 2139 [EXE]	LHA?	14	[]	
5	35600 [EXE]	HO?	15	[]	
6	1952 [EXE]	T. MZD	16	[]	
7	[EXE]	70.04124028	17	[]	
8	[EXE]	X-MER	18	[]	
9	[EXE]	(repeat again)	19	[]	
10	[EXE]		20	[]	

No. Prg. 1

Line	MODE [2]	Program	Notes	Number of steps
1	" X - M E R	if ▲ Prg 7 : Prg 8 : Prg		
2	9 : Abs (H - I 8 0)	→ T : (-) 1		
3	→ I : T < 9 0	⇒ Goto 2 : 1 8 0 -		
4	T → T : 1 → I : Lbl 2 : . 0 0 8			
5	7 2 6 x COS D x COS L ÷ SIN Abs (L -			
6	D x I) x T x ² x I + S → M : "			
7	T • M Z D " ▲ 9 0 - M → N ▲			
8				
9				

Compass error by time azimuth

The azimuth of the body can be obtained by the equation (2) as explained in the problem of altitude and azimuth. The accuracy of computed azimuth depends on the accuracy of the time of observation and the accuracy of the ship's position or the observer's position.

Example: On 24 April 1970, DR Lat. $33^{\circ}25.2$ S Long. $139^{\circ}22.8$ W at ZT 16-26-32. Observed bearing of the sun GB 297.5 CB 290.5 variation at that area is 5° E. Require GE and deviation of magnetic compass.

Solution

	<u>Sun 0</u>		<u>d(+) 0.8</u>	
ZT	16 26 32	24 April	01 ^h	$12^{\circ}59'7''$ N Computed Zn 296 ^o 6
ZD	+ 9		corr(+)	$.4$ GR 297 ^o 5
GMT	01 26 32	25 April	dec.	$13^{\circ} 0'1''$ N GE 0.9 W
01 ^h	<u>$195^{\circ}29'1''$</u>		=====	=====
$26^m32^s(+)$	<u>$6^{\circ}38'0''$</u>			Computed Zn 296 ^o 6
GHAO	$202^{\circ}07'1''$			Var 5° E
DR λ	<u>$139^{\circ}22'8''$</u>			MB 291.6
LHA	$62^{\circ}44'3''$			CB 290.5
	=====	DR Lat $33^{\circ} 25'2''$ S		Dev. 1.1 E
		=====		=====

Explanation of Solution

1. Converting observed zone time (ZT) to GMT.
2. From date and GMT, find true LHA and declination, using nautical almanac.
3. Using DR Lat., and declination as input of Prg. 2 to obtain Zn.

PROGRAM SHEET

4. Compass the computed Zn with Gyro bearing to obtain Gyro error.
5. Apply variation to Zn to obtain true magnetic bearing (MB).
6. Compare MB with compass bearing to get deviation (Dev.).

Example 1. Lat 33°24'0" N Dec 50°13'8" W LHA 316°41'3"
 2. Lat 33°24'0" S Dec 50°13'8" W LHA 316°41'3"
 Answer 5. Zn = 44°08'22.50"

* Execute the program as shown below in the RUN mode (F5) (F6)

Step	Key operation	Display	Key operation	Display
1	<input type="checkbox"/> [F5] Prg 5	T-VZ	<input type="checkbox"/>	
2	<input type="checkbox"/> [F5] LAT+N-S1	LAT+N-S1	<input type="checkbox"/>	
3	<input type="checkbox"/> [F5] 2324	Dec+N-S2	<input type="checkbox"/>	
4	<input type="checkbox"/> [F5] 5013.8	LHA?	<input type="checkbox"/>	
5	<input type="checkbox"/> [F5] 31641.3	Zn	<input type="checkbox"/>	
6	<input type="checkbox"/> [F5] 07.71043681		<input type="checkbox"/>	
7	<input type="checkbox"/> [F5] T-VZ		<input type="checkbox"/>	
8	<input type="checkbox"/> [F5] (Report)		<input type="checkbox"/>	
9	<input type="checkbox"/> [F5]		<input type="checkbox"/>	
10	<input type="checkbox"/> [F5]		<input type="checkbox"/>	

1/3

Program	Notes	Number of tests
1 " T - A 2 " A Prg 5 : Prg 6		
2		

no. Prg. 5

PROGRAM SHEET

Program for Compute true azimuth from Lat, dec, LHA	No. Prg. 2
<p><u>Description</u></p> <p>Input Lat = Latitude of observer Dec = Declination of the body LHA = Local hour angle of the body</p> <p>Output ZN. = True azimuth of the body</p> <p><u>Example</u> 1. Lat 33°24'0 N Dec 20°13'8 N LHA 316°41'2 2. Lat 33°24'0 S Dec 20°13'8 N LHA 316°41'2</p> <p>Answer 2. ZN = 44°08'733264</p> <p><u>Preparation and operation</u></p> <p>● Execute the program as shown below in the RUN mode (MODE II).</p>	

Step	Key operation	Display	Step	Key operation	Display
1	Prg 2 <input type="checkbox"/> EXE	T-AZ	11	<input type="checkbox"/>	
2	<input type="checkbox"/> EXE	LAT+N-S?	12	<input type="checkbox"/>	
3	3324 <input type="checkbox"/> EXE	Dec+N-S?	13	<input type="checkbox"/>	
4	2013.8 <input type="checkbox"/> EXE	LHA?	14	<input type="checkbox"/>	
5	31641.2 <input type="checkbox"/> EXE	ZN	15	<input type="checkbox"/>	
6	<input type="checkbox"/> EXE	97.71043681	16	<input type="checkbox"/>	
7	<input type="checkbox"/> EXE	T-AZ	17	<input type="checkbox"/>	
8	<input type="checkbox"/> EXE	(repeat again)	18	<input type="checkbox"/>	
9	<input type="checkbox"/> EXE		19	<input type="checkbox"/>	
10	<input type="checkbox"/> EXE		20	<input type="checkbox"/>	

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No. Prg. 2

Line	MODE: Z	Program	Notes	Number of steps
1	" T - A Z "	▲ Prg 7 : Prg 8 : Prg 6		
2				

Compass error by Amplitude

True azimuth of a celestial body can be obtained by amplitude observation, and being used to compare with the compass in order to get compass error.

Formula $\sin A = \frac{\sin d - \sin L \cdot \sin h}{\cos L \cdot \cos h}$

Notation A = Amplitude
 d = Declination of a celestial (+N, -S, $d < 24^\circ$)
 L = Latitude of observer (+N, -S)
 h = True altitude of center of the body from celestial horizon

Condition:

1. If the body is observed when its center is on the celestial horizon, that means $h = 0^\circ$ under the following assumption:

The Sun's lower limb is about 2/3 of its diameter above visible horizon.

The Moon's upper limb is on the visible horizon.

The Star or planet is slightly more than one Sun's diameter or about $32'0$ above the visible horizon.

2. If the body is observed when it is on the visible horizon, that means $h \neq 0$ and corrections must be applied in order to get the correct observed amplitude when the center of the body is on the celestial horizon.

For the Sun, when observation is made at height of eye 41 ft, standard condition temp. 50°F, Atmos. pressure 29.83 inches of mercury the value of h may be computed as follows:

Dip	- 6!2	Dip. - 6!2	Dip. - 6!2		
Refraction	- 35!3	R - 33!2	R - 33!2	(A-P)	
Irradiation of Hor.	- 0!6	SD + 15!8	SD - 15!8	(daily page)	
Parallax	+ 0!1	P + 0!7	P + 0!1		
h	(-)42!0	h - 23!5	h - 55!1		
	=====	=====	=====		

(This h is used for determining the corrections in table 28 of Bowditch, Vol. II.)

(For explanation)

By using computer or programmable calculator, the true azimuth (Zn) of the observed body can be computed according to the following rules:

For rising sun when $h = 0$ $Zn = 90 - \text{Sun}^{-1} A$
 $h = 0$ Lat.= dec. same name, h is positive
 Lat.= dec. contrary name, h is negative
 $Zn = 90 + \text{Sin}^{-1} A$

For setting sun when $h = 0$ $Zn = 270 + \text{Sin}^{-1} A$
 $h = 0$ Lat.= dec. same name, h is negative
 Lat.= dec. contrary name, h is positive
 $Zn = 270 + \text{sin}^{-1} A$

Example of amplitude

1. The DR Lat. of a ship is $51^{\circ}24'6''$ N. The navigator observes the setting Sun when the center is on the visible horizon, at that time declination of the Sun is $19^{\circ}40'4''$ N.

Required: 1. Observed amplitude

2. Zn on visible horizon (data from Dutton 12th edition P. 508)

by Table 27, 28

by computer

T 27	Amp. W	32.6 N		
T 28	Corr.	(+) 1.1		
	Obs. Amp. W	33.7 N	Obs. Amp.	33.716
	Zn	303.7	Zn	303.716

2. DR Lat. $41^{\circ}03'8''$ N Observe rising sun when center is on visible horizon GB $059^{\circ}05'$, declination of Sun is $22^{\circ}31'9''$ N.

Required: Gyro error (Dutton 13th ed.)

by Table

by computer

T 27	True Amp. E	30.5 N	Obs. Amp.	29.84 = 29.8
T 28	Corr.	- .7	Zn	60.15 = 60.2
	Obs. Amp. E	29.8 N	GB	59.5
	Zn	60.2	GE	.7 E
	GB	59.5		
	GE	.7 E		

Program for Compute true azimuth by amplitude of the Sun No. Prg 3
PROGRAM SHEET

Description Input
 "LAT+N-S" Input Latitude of observer (+N, -S)
 "Dec+N-S" " Declination of the Sun (+N, -S)
 "R1-S2" Input 1 for rising observation
 " 2 for setting observation
 "V1-C2" Input 1 Sun's center on visible horizon
 2 Sun's center on celestial horizon
 Output True azimuth of the Sun at time of observation

Example

1. DR Lat 51°24'6 N Dec 19°40'4 N Set θ on visible horizon
 2. DR Lat 16°03'6 S Dec 20°09'1 N Rise θ on visible horizon
- Answer 2. ZN 69.20611918

Preparation and operation

• Execute the program as shown below in the RUN mode (MODE II).

Step	Key operation	Display	Step	Key operation	Display
1	Prg 3 [EXE]	AMP.S	11	[]	
2	[EXE]	LAT+N-S?	12	[]	
3	5124.6 [EXE]	DEC+N-S?	13	[]	
4	1940.4 [EXE]	R1-S2?	14	[]	
5	2 [EXE]	V1-C2?	15	[]	
6	1 [EXE]	ZN.	16	[]	
7	[EXE]	303.716742	17	[]	
8	[EXE]	AMP.S	18	[]	
9	[EXE]	(repeat again)	19	[]	
10	[EXE]		20	[]	

Line	MODE: [2]	Program 3	Notes	Number of steps
1	" A M P . S "	" ▲ Prg 7 ; "	" R 1 -	
2	S 2 " ; ? → I :	" V 1 - C 2 "		
3	: ? → J : L ÷ Abs:	L → E : D ÷ Abs:		
4	D → F ; Ø → H :	J = 2 → Goto 5 :		
5	I = 2 → Goto 2 :	E = F → Goto 3 : Goto		
6	4 : Lbl 2 : E = F → Goto 4 :	Lbl 3 :		
7	. 7 → H : Goto 5 : Lbl 4 :	- . 7 →		
8	H : Lbl 5 : SIN ¹ ((SIN D - SIN L X SIN			
9	H)) ÷ COS L ÷ COS H) → P :	I = 1		
10	→ Goto 7 : 2 7 Ø + P → Z :	Goto 8 :		
11	Lbl 7 : 9 Ø - P → Z : Lbl 8 :	" Z :		
12	N . " ▲ Z ▲			
13				

PROGRAM SHEET

Program for	Sub. Routine	No.
Description		
Prg 5 converting Deg Min (1530.0) to Deg. 15°5		
Prg 6 Compute true azimuth (ZN) from Lat, dec and LHA		
Prg 7 Input Latitude (L) and declination (D)		
Prg 8 Input Local hour angle		
Prg 9 Input Corrected observed altitude (HO)		

Line	MOE: [2]	Program	Notes	Number of steps
Prg 5	1	Int : (A ÷ 1 0 0) → B : B + (A		
	2	- B X 1 0 0) ÷ 6 0 → C		
	3			
Prg 6	4	SIN: H ÷ (COS H X SIN L - tan D X COS L		
	5) → X : tan ⁻¹ X → Y : H > 1 8 0 →		
	6	Goto 2 : X ≥ 0 ⇒ Goto 3 : 3 6 0 + Y		
	7	→ Z : Goto 4 : Lbl 2 : X < 0 ⇒ Goto 3		
	8	: Y → Z : Goto 4 : Lbl 3 : 1 8 0 +		
	9	Y → Z : Lbl 4 : " Z N . " Δ Z Δ		
	10			
Prg 7	11	Md : " L A T + N - S " ; ? → A		
	12	: Prg 5 : C → L : " D E C + N -		
	13	S " : ? → A : Prg 5 : C → D		
	14			
Prg 8	15	" L H A " : ? → A : Prg 5 : C →		
	16	H		
	17			
Prg 9	18	" H O " : ? → A : Prg 5 : C → S		
	19			

BY NC-88, TAMAYA CO., LTD
 Formulae of Celestial Navigation, Piloting, Dead Reckoning and the
 Nautical Almanac are programmed and stored.

STAR FINDER:

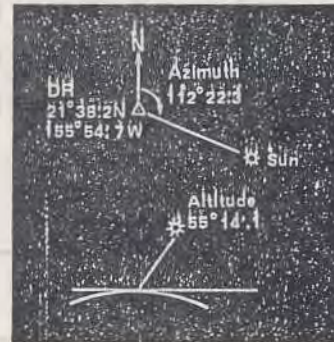
NAUTICAL ALMANAC [ALM] / ALTITUDE AND AZIMUTH [AZ]

NC-88 Nautical Almanac [ALM] is good with accuracy better than 0.2 through the year 2100. Followed by [AZ] It computes the altitude and azimuth of any navigational body from any point on the earth. Almanac includes the Sun, Moon, Venus, Mars, Jupiter, Saturn and 63 navigational stars.

[SUN]

Find the GHA and DEC of the Sun at GMT 20^h18^m36^s on April 4, 1982. Then compute its Altitude and Azimuth from the DR position 21°38'2N, 155°54'7W.

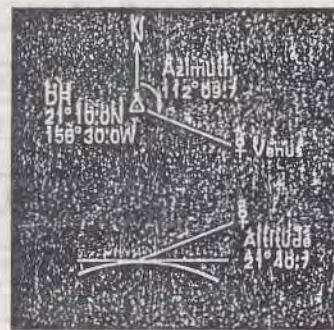
Input Key	Display	Description
[ALM]	[ALM]	Almanac
[0] 20 1836	HMS 20 1836	GMT
[0] 1982 0404	YMD 1982 0404	Date
[0] 0	CB 0	Celestial Body Number
[0]	CB Sun	Body Name
[0]	CB Sun (Blinks)	
[0]	SD 0.160	Semidiameter
[0]	DEC 5.483N	Declination
[0]	GHA 123.543	Greenwich Hour Angle
[0]	EOT -0.0259	Equation of Time
[AZ]	[ALT-AZ]	Altitude-Azimuth
[0] 21 382 [5]	LAT 21.382N	DR Lat.
[0] 155 547 [5]	LON 155.547W	DR Long.
[0]	-PROCESS-	
[0]	ALTc 55.141	Altitude
[0]	AZ 112.223	Azimuth



[VENUS]

Find the GHA and DEC of Venus at GMT 15^h30^m00^s on April 4, 1982. Then compute its Altitude and Azimuth from the DR position 21°10'0N, 156°30'0W.

Input Key	Display	Description
[ALM]	[ALM]	Almanac
[0] 15 3000	HMS 15 3000	GMT
[0] 1982 0404	YMD 1982 0404	Date
[0] 70	CB 70	Celestial Body Number
[0]	CB Venus	Body Name
[0]	CB Venus (Blinks)	
[0]	HP 0.002	Horizontal Parallax
[0]	DEC 11.095S	Declination
[0]	GHA 95.116	Greenwich Hour Angle
[AZ]	[ALT-AZ]	Altitude-Azimuth
[0] 21 100 [5]	LAT 21.100N	DR Lat.
[0] 156 300 [5]	LON 156.300W	DR Long.
[0]	-PROCESS-	
[0]	ALTc 21.407	Altitude
[0]	AZ 112.097	Azimuth



[SPICA]

Find the GHA and DEC of Spica at GMT 8^h30^m00^s on April 30, 1982. Then compute its Altitude and Azimuth from the DR position 31°20'0N, 138°14'5W.

Input Key	Display	Description
[ALM]	[ALM]	Almanac
[0] 8 3000	HMS 8 3000	GMT
[0] 1982 0430	YMD 1982 0430	Date
[0] 60	CB 60	Celestial Body Number
[0]	CB Spica	Body Name
[0]	CB Spica (Blinks)	
[0]	DEC 11.042S	Declination
[0]	CHAA 345.275	GHA Aries
[0]	SHA 158.561	SHA
[0]	GHA 144.236	Greenwich Hour Angle
[AZ]	[ALT-AZ]	Altitude-Azimuth
[0] 31 200 [5]	LAT 31.200N	DR Lat.
[0] 138 145 [5]	LON 138.145W	DR Long.
[0]	-PROCESS-	
[0]	ALTc 47.113	Altitude
[0]	AZ 188.541	Azimuth



Applications: Other than the strict Astro-Navigation practice, the true Azimuth of the celestial body may be used effectively in compass adjustment. The computed Sun's altitude is useful in knowing the twilight time in advance.

LINE OF POSITION (LOP) AND POSITION FIX (FIX)

FIX BY TWO SIGHTS

The DR position of a vessel is 21° 10' 00" N, 156° 30' 00" W around 15 o'clock GMT on April 4, 1982. It is steering the true course 67° at speed 8 knots when the following sights are taken. The height of eye is 3 meters. Compute the fix at the time of the sights and at 15 o'clock.

Date	GAIT	Body	Sextant Altitude (after index correction)
April 4, 1982	15 ^h 25 ^m 43 ^s	Vega (62)	70° 00' 3"
April 4, 1982	15 ^h 28 ^m 11 ^s	Venus (70)	21° 16' 3"

Input key	Display	Description
[LOP]	[LOP1]	Line of Position No.1
[6]	15.2543	Sight Time (Hour, Minutes, Second - GMT)
[6]	1982.0404	Sight Date (Year, Month, Day)
[6]	62	Celestial Body Number
[6]	CB	Body Name
[6]	70.003	Sextant Altitude (After Index Correction)
[3]	HGT	Height of Eye
[3]	TMP	Temperature
[3]	PR3	Pressure
[3]	LA1	DR Lat
[3]	LO1	DR Long
[6]	156.3000	DR Lat
[6]	156.3000	DR Long
[6]	CHECK?	
[6]	-PROCESS (Blinks)-	
[6]	AZ	26.514
[6]	IN1	8.6
[LOP]	[LOP2]	Line of Position No.2
[6]	15.2811	Sight Time
[6]	YVD	1982.0404
[6]	70	Celestial Body Number
[6]	CB	Body Name
[6]	21.163	Sextant Altitude (After Index Correction)
[6]	CC	67
[6]	SP3	8
[6]	CHECK?	
[6]	-PROCESS-	
[6]	AZ	111.564
[6]	IN1	-6.4
[FIX]	[FIX]	Position Fix
[6]	-PROCESS-	
[6]	LA1	21.209 N
[6]	LO1	156.327 W
[6]	HMSI	15.2543
[6]	YVDI	1982.0404
[6]	[FIX SERIES]	
[6]	HMSI	15.2811
[6]	YVDI	1982.0404
[6]	-PROCESS-	
[6]	LA1	21.210 N
[6]	LO1	156.324 W
[6]	[FIX SERIES]	
[6]	HMSI	15
[6]	YVDI	1982.0404
[6]	-PROCESS-	
[6]	LA1	21.195 N
[6]	LO1	156.361 W

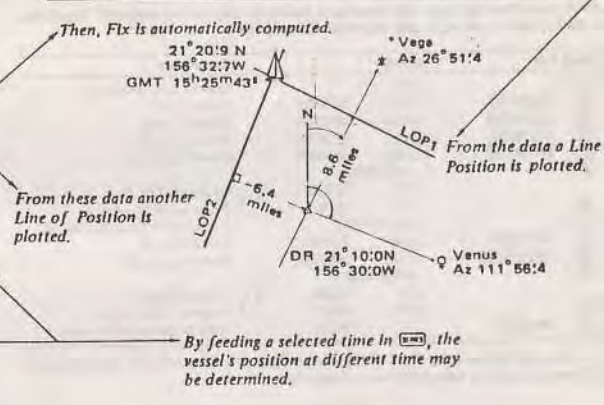
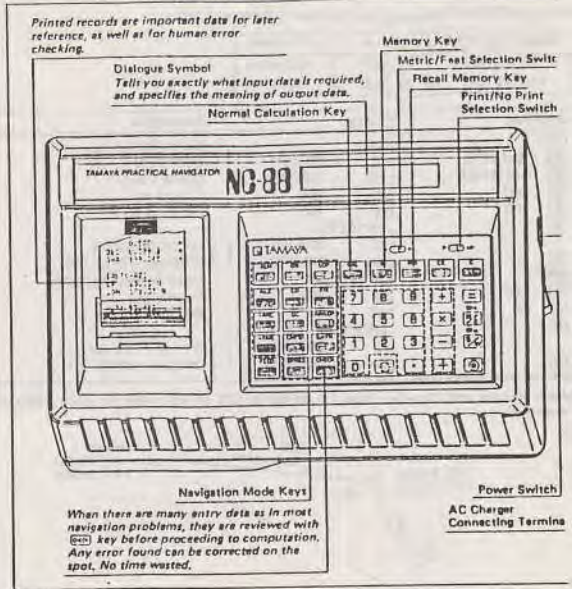
() Azimuth 26° 51' 4" Intercept 8' 6" (miles)

() Azimuth 111° 56' 4" Intercept -6' 4" (miles)

() Fix Lat. 21° 20' 9" N Fix Long. 156° 32' 7" W Fix Time 15h 25m 43s Fix Date 1982.0404 Fix Series Selected Time 15h 28m 11s

() Fix Lat. 21° 21' 0" N Fix Long. 156° 32' 4" W Fix Series Selected Time 15h 00m 00s

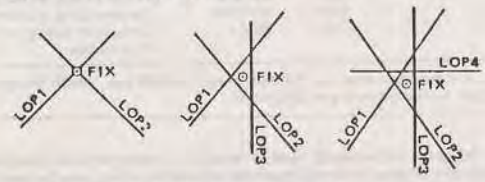
() Fix Lat. 21° 19' 5" N Fix Long. 156° 36' 1" W



FIX BY MULTIPLE SIGHTS

Fix by multiple sights is also possible by repeating [LOP] with more celestial bodies. Any celestial body in the NC-88 may be used.

In the theory of Astro-Navigation, a ship's position can be determined only after at least two Lines of Position (LOP) are obtained. The intersection of the two LOP's called "Fix" is the ship's position. If three LOP's are given, the centroid of the triangle is computed as the fix. We may also take the fourth and fifth LOP and so forth to refine the fix.

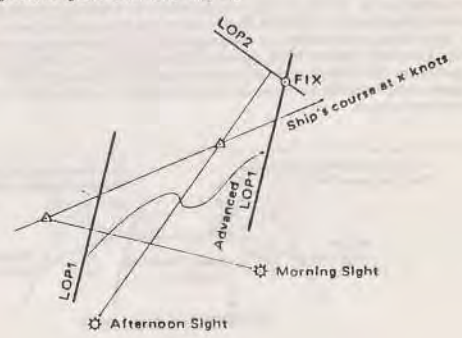


EXTRA FIX [RECALL] and ADD LOP FIX [ADD LOP]

When pre-computed Azimuths and Intercepts are externally available for two lines of Position the fix is directly computed by [RECALL]. The third and more number of LOP's are added by [ADD LOP] to determine the centroid.

RUNNING FIX BY SUN SIGHTS

If it is desired to fix the ship's position by the Sun sights only, RUNNING is made similarly in [LOP] by feeding ship's course and speed between the sights (e.g. morning and afternoon sights).



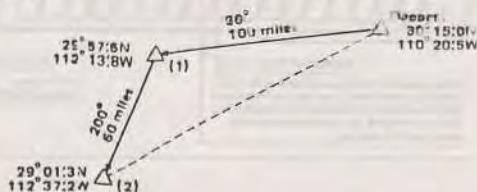
DEAD RECKONING (DR) BY MERCATOR SAILING

Find the DR position after the first and the second run.

Departure Point	Course	Distance
30° 15' 0N 110° 20' 5W	1) 260°	100 miles
	2) 200°	60 miles

Input Key	Display	Description
[DR]	[DR]	Dead Reckoning
[30] [15] [0]	LAT 30 150N	Depart Lat
[110] [20] [5]	LON 110.205W	Depart Long
[260]	CO 260	Course (1)
[100]	DST 100	Distance (1)
	-PROCESS-	
	LAT 29.576N	() DR Lat 29° 57' 6N
	LON 112.138W	() DR Long 112° 13' 8W
[DR SERIES]	[DR SERIES]	Dead Reckoning Series
[200]	CO 200	Course (2)
[60]	DST 60	Distance (2)
	-PROCESS-	
	LAT 29.013N	() DR Lat 29° 01' 3N
	LON 112.372W	() DR Long 112° 37' 2W

More courses and distances may be added in DR series mode by using [DR] key repeatedly.

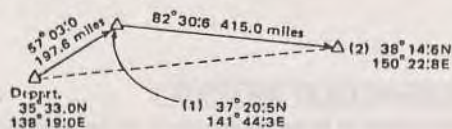


COURSE AND DISTANCE (CD) BY MERCATOR SAILING

Find the distance from the departure point to the arrival point (1) from the point (1) to the point (2), and the total distance run.

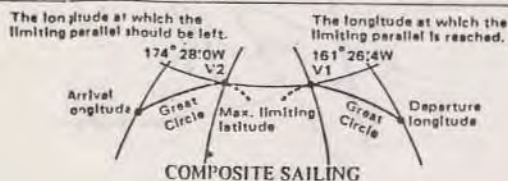
Input Key	Display	Description
[CD]	[CD]	Course and Distance
[35] [33] [0]	LATd 33.330N	Depart Lat
[138] [19] [0]	LONd 138.190E	Depart Long
[37] [20] [5]	LATs 37.205N	Arrival Lat (1)
[141] [44] [3]	LONs 141.443E	Arrival Long (1)
	-PROCESS-	
	CO 57.030	() Course 57° 03' 0
	DST 197.6	() Distance 197.6 miles
[CD SERIES]	[CD SERIES]	Course and Distance Series
[38] [14] [6]	LATa 38.146N	Arrival Lat. (2)
[150] [22] [8]	LONa 150.228E	Arrival Long. (2)
	-PROCESS-	
	CO 82.306	() Course 82° 30' 6
	DST 415.0	() Distance 415.0 miles
[4]	[197.6]	Total Distance 612.6 miles

Courses and distances to more continuing points of arrival may be determined in CD series mode by using [CD] key repeatedly.



Note on Accuracy:

The principle of [DR] and [CD] computation is Mercator Sailing. The oblate spheroid characteristics of earth (flattened at the poles and bulged at the equator) are taken into consideration in the programming. The most up-to-date WGS-72, World Geodetic System 1972 spheroid (Eccentricity = 0.08182), is being used to guarantee the utmost accuracy. When the course is exactly 090° or 270° the program automatically switches to Parallel Sailing. In this case the earth is considered as a sphere.



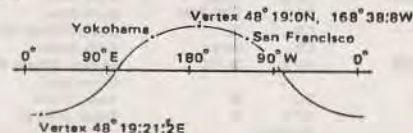
GREAT CIRCLE SAILING (GC)

	Depart. Point (San Francisco)	Arrival Point (Yokohama)
Lat.	37° 50' 8 N	34° 52' 0 N
Long.	122° 25' 5 W	139° 42' 0 E

Find the great circle distance, initial great circle course, vertex latitude and longitude, and latitude at 145° W and 150° W.

Input Key	Display	Description
[GC]	[GC]	Great Circle Sailing
[37] [50] [8]	LATd 37.508N	Depart Lat
[122] [25] [5]	LONd 122.255W	Depart Long
[34] [52] [0]	LATa 34.520N	Arrival Lat
[139] [42] [0]	LONa 139.420E	Arrival Long
	-PROCESS-	
	CO 302.379	Initial Great Circle Course 302° 37' 9
	DST 4488.8	Great Circle Distance 4488.8 miles
	LATv 48.190N	Vertex Lat 48° 19' 0N
	LONv 168.388W	Vertex Long 168° 38' 8W
[LATI SERIES]	[LATI SERIES]	Intermediate Latitude Series
[145]	LONI 145W	Intermediate Long
	-PROCESS-	
	LATI 46.467N	Intermediate Lat. 46° 46' 7N
[150]	LONI 150W	(change to 150° W)
	-PROCESS-	
	LATI 46.467N	Intermediate Lat. 46° 46' 7N

More Intermediate Longitudes may be entered by [LATI] key for Latitude determination.



Point to point planning:

Since a great circle, except the equator and any meridian line, is continuous changing direction as one proceeds along it, no attempt is customarily made to follow it exactly. Rather, a number of points are selected along the great circle and rhumb lines are followed from point to point, taking advantage of the fact that for short distances a great circle and a rhumb line almost coincide. The points usually are selected every 5° of longitude for convenience (the number of points to use is a matter of personal preference), and the corresponding latitudes are computed by NC-88.

COMPOSITE SAILING (COMP)

Find the composite track with the maximum limiting latitude of 45° N.

Input Key	Display	Description
[GC]	[GC]	Great Circle Sailing
[37] [50] [8]	LATd 37.508N	Depart Lat
[122] [25] [5]	LONd 122.255W	Depart Long
[34] [52] [0]	LATa 34.520N	Arrival Lat
[139] [42] [0]	LONa 139.420E	Arrival Long
	-PROCESS-	
	CO 302.379	Initial Great Circle Course 302° 37' 9
	DST 4488.8	Great Circle Distance 4488.8 miles
	LATv 48.190N	Vertex Lat 48° 19' 0N
	LONv 168.388W	Vertex Long 168° 38' 8W
[COMPOSITE]	[COMPOSITE]	Composite Sailing
[45]	LAT L 45N	Limiting Latitude
	-PROCESS-	
	CO 296.259	Initial GC Course to V1 296
	LONI 161.264W	Tangent Long V1 161° 26' 4
	LONI 174.290W	Tangent Long V2 174° 28' 4
	DST 4504.4	Composite Sailing Distance 4504.4 miles

More Limiting Latitudes may be determined by [COM] key, which brings the gram back to the beginning of [GC] mode.

When the great circle would carry a vessel to a higher latitude than desired, modification of great circle sailing called composite sailing, may be used to advantage. The composite track consists of a great circle from the point of departure tangent to the limiting parallel, a course line along the parallel a great circle tangent to the limiting parallel and through the destination.

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